

10	Gl 244		06 42 57	-16 38.8	DA2	8.44	-0.03	380.4	11.34	a = 7.500" P = 50.090 yr
11	Gl 729		18 46 45	-23 53.5	dM4.5e	10.46	1.72	341.1	13.12	AC-24:2833-183
12	Gl 905		23 39 26	+43 55.2	dM6 e	12.29	1.90	315.6	14.79	Ross 248
13	Gl 144		03 30 34	-09 37.6	K2 V	3.73	0.88	305.6	6.16	EPS Eri
14	Gl 447		11 45 09	+01 06.0	dM4.5	11.12	1.75	301.1	13.51	Ross 128
15	Gl 866	AB	22 35 45	-15 35.6	M5 e	12.66	1.98	294.3	15.00	L 789-006 V (AB) = 12.30 d(m) = 1.0 ; a = 0.36" P = 2.2 yr
16	Gl 15	A	00 15 31	+43 44.4	M2 V	8.08	1.56	289.5	10.39	GX And
17	Gl 15	B	00 15 31	+43 44.4	M6 Ve	11.06	1.79	289.5	13.37	GQ And
18	Gl 845		21 59 33	-56 59.6	K5 Ve	4.69	1.06	288.9	6.99	EPS Ind
19	Gl 820	A	21 04 40	+38 30.0	K5 Ve	5.21	1.18	288.7	7.51	61 Cyg
20	Gl 820	B	21 04 40	+38 30.0	K7 Ve	6.03	1.37	288.7	8.33	
21	Gl 725	A	18 42 12	+59 33.3	dM4	8.90	1.52	286.1	11.18	
22	Gl 725	B	18 42 13	+59 33.0	dM5	9.71	1.59	286.1	11.99	sep 17" 155d
23	Gl 71		01 41 45	-16 12.0	G8 Vp	3.49	0.72	286.0	5.77	TAU Cet
24	Gl 280	A	07 36 41	+05 21.3	F5 IV-V	0.38	0.42	285.8	2.66	ALF Cmi
25	Gl 280	B	07 36 41	+05 21.3	DA	10.70		285.8	13.00	
26	Gl 887		23 02 39	-36 08.5	M2 Ve	7.34	1.49	284.3	9.61	
27	GJ 1111		08 26 53	+26 57.2	M6.5	14.81	2.06	275.8	17.01	
28	Gl 54.1		01 09 59	-17 16.4	dM5 e	12.05	1.84	267.4	14.19	LTT 670 L 725-32
29	Gl 273		07 24 43	+05 22.7	M3.5	9.85	1.56	264.4	11.96	
30	Gl 825		21 14 20	-39 03.7	M0 Ve	6.67	1.41	258.6	8.73	
31	Gl 191		05 09 41	-44 59.9	M0 V	8.85	1.55	258.3	10.91	
32	Gl 860	A	22 26 13	+57 26.8	M2 V	9.85	1.62	251.9	11.86	ADS 15972 Kr 60 V(AB) = 9.59 d(m) = 1.67
33	Gl 860	B	22 26 13	+57 26.8	M6 V	11.30	1.80	251.9	13.30	DO Cep a = 2.412" P = 44.6 yr

34	Gl 628	wissenschaft in die schulen	16 27 31	-12 32.3	M3.5	10.08	1.58	244.7	12.02	
35	Gl 234	A	06 26 51	-02 46.2	M4.5 J	11.13	1.71	242.1	13.05	Ross 614 V (AB) = 10.10 d(m) = 3.5 ?
36	Gl 234	B	06 26 51	-02 46.2		14.60		242.1	16.50	V 577 Mon a = 0.932" 16.60 yr
37	GJ 1061		03 34 16	-44 40.3	M4.5	13.03	1.90	233.0	14.90	LFT 295 LTT 1702
38	Gl 473	A	12 30 51	+09 17.6	dM5.5eJ	13.04	1.83	232.2	14.87	Wolf 424 V (AB) = 12.43 d(m) = 0.3
39	Gl 473	B	12 30 51	+09 17.6	M7	13.30		232.2	15.10	FL Vir a = 0.76" P = 16.2 yr
40	Gl 35		00 46 31	+05 09.2	DZ7	12.38	0.55	230.9	14.20	van Maanen 2
41	NN 3522		08 56 14	+08 40.4	k	10.89	1.67	224.0	12.64	LTT 12352
42	Gl 83.1		01 57 28	+12 50.1	dM8 e	12.28	1.80	223.8	14.03	L 1159-016
43	NN 3618		10 42 40	-60 57.2	m	13.92	1.82	222.8	15.66	LTT 3946 L 143-23
44	Gl 1		00 02 28	-37 36.2	M4 V	8.54	1.46	221.8	10.27	
45	NN 3622		10 45 41	-11 03.1	M6.5	15.60	2.10	221.0	17.32	LP 731-58
46	Gl 674		17 24 53	-46 50.6	M3	9.37	1.53	219.7	11.08	
47	Gl 440		11 42 58	-64 33.5	DQ6	11.50	0.19	218.5	13.20	L 145-141
48	Gl 832		21 30 14	-49 13.2	M1 V	8.67	1.47	215.0	10.33	L 354-89 CD- 49:13515 Sm 83
49	Gl 380		10 08 19	+49 42.5	K2 Ve	6.59	1.36	213.2	8.23	
50	GJ 1002		00 04 13	-07 47.5	M5-5.5	13.75	1.98	212.8	15.39	
51	Gl 687		17 36 42	+68 23.1	M3.5 V	9.18	1.50	212.7	10.82	
52	GJ 1245	A	19 52 16	+44 17.5	M5.5 V e	13.41	1.90	212.0	15.04	V1581 Cyg orbit in Harrington AJ 100, p 559 (1990)

53	GJ 1245	B	19 52 17	+44 17.5	m	14.01	1.98	212.0	15.64	sep 7" 103d (LHS)
54	GJ 682		17 33 28	-44 16.6	M3.5	10.95	1.65	211.6	12.58	
55	GJ 876		22 50 35	-14 31.2	dM5	10.17	1.58	211.3	11.79	
56	GJ 166	A	04 12 58	-07 43.8	K1 Ve	4.43	0.82	207.1	6.01	LTT 1907 OMI(2) Eri
57	GJ 166	B	04 13 04	-07 44.1	DA4	9.52	0.03	207.1	11.10	LTT 1908 40 Eri B
58	GJ 166	C	04 13 04	-07 44.1	dM4.5e	11.17	1.67	207.1	12.75	LTT 1909 DY Eri
59	GJ 388		10 16 54	+20 07.3	M4.5Ve	9.40	1.54	203.9	10.95	AD Leo
60	GJ 768		19 48 21	+08 44.1	A7 IV-V	0.77	0.22	201.0	2.29	ALF Aql
61	GJ 702	A	18 02 56	+02 30.6	K0 Ve	4.21	0.86	199.0	5.70	ADS 11046 V(AB) = 4.02 d(m) = 1.80
62	GJ 702	B	18 02 56	+02 30.6	K5 Ve	6.00	1.15	199.0	7.49	a = 4.545" P = 88.13 yr
63	GJ 873		22 44 40	+44 04.6	dM4.5e	10.26	1.61	197.0	11.73	EV Lac opt. comp. sep 5"
64	GJ 445		11 44 35	+78 57.7	sdM4	10.80	1.60	191.5	12.21	AC+79:3888
65	GJ 1116	A	08 55 27	+19 57.4	m	14.06	1.84	191.3	15.47	
66	GJ 1116	B	08 55 27	+19 57.5	m	14.92	1.93	191.3	16.33	LP 426-40 sep 4.5" 333d angles increasing 1d /yr (LHS)
67	GJ 412	A	11 03 00	+43 47.0	M2 Ve	8.74	1.54	188.8	10.12	LTT 12976
68	GJ 412	B	11 03 02	+43 46.7	M6 e	14.40	2.09	188.8	15.78	LTT 12977 WX Uma
69	GJ 1005	AB	00 12 53	-16 24.3	M4	12.03	1.72	188.7	13.41	L 722-22 Hei 299 sep 0.14" V(AB) = 11.50 d(m) = 0.5 :
70	GJ 663	A	17 12 16	-26 31.8	K1 Ve	5.07	0.85	187.6	6.44	ADS 10417AB V (AB) = 4.32 d (m) = 0.04

71	Gl 663	B	17 12 16	-26 31.9	K1 Ve	5.11	0.86	187.6	6.48	a = 13.91" P = 548.7 yr
72	NN 3379		05 57 26	+02 42.3	M4	11.33	1.68	186.3	12.68	LTT 17897
73	Gl 526		13 43 12	+15 09.7	M4 Ve	8.46	1.44	184.0	9.78	
74	Gl 664		17 13 09	-26 28.6	K5 Ve	6.33	1.16	182.0	7.63	ADS 10417C cpm to Gl 663, sep 732"
75	Gl 169.1	A	04 26 47	+58 53.9	dM4	11.08	1.65	181.9	12.38	AC +58:25001 Stein 2051
76	Gl 169.1	B	04 26 47	+58 53.9	DC5	12.44	0.31	181.9	13.74	AC +58:25002 sep 7" 89d (NLTT)
77	Gl 764		19 32 28	+69 34.6	K0 V	4.68	0.79	178.2	5.93	SIG Dra
78	Gl 908		23 46 36	+02 08.2	M2 Ve	8.98	1.48	177.9	10.23	
79	Gl 783	A	20 07 55	-36 13.7	K3 V	5.32	0.87	177.1	6.56	
80	Gl 783	B	20 07 55	-36 13.7	M3.5	11.50		177.1	12.70	
81	Gl 752	A	19 14 29	+05 05.8	M3.5Ve	9.11	1.50	176.7	10.35	
82	Gl 752	B	19 14 32	+05 04.7	dM5 e	17.52	2.20	176.7	18.76	VB 10
83	Gl 754		19 17 07	-45 36.7	M4.5	12.23	1.68	175.7	13.45	L 347-014
84	Gl 780		20 03 50	-66 18.7	G8 V	3.56	0.76	175.2	4.78	DEL Pav
85	Gl 229		06 08 28	-21 50.6	M1 Ve	8.14	1.50	174.9	9.35	
86	Gl 570	A	14 54 32	-21 11.5	K5 Ve	5.75	1.10	174.2	6.96	
87	Gl 570	B	14 54 31	-21 11.3	M2 V	8.00	1.50	174.2	9.21	
88	Gl 251		06 51 35	+33 20.3	dM4	10.01	1.57	173.6	11.21	AC +33:25644
89	Gl 205		05 28 55	-03 41.1	M1.5 V	7.96	1.47	172.3	9.14	
90	Gl 643		16 52 45	-08 13.9	sdM4	11.80	1.69	171.9	12.98	Wolf 629 cpm with Gl 644 sep 72" 315d
91	Gl 300		08 10 29	-21 23.5	M4	12.10	1.60	170.0	13.25	L 674-015
92	Gl 34	A	00 46 03	+57 33.1	G3 V	3.45	0.57	168.4	4.58	ETA Cas
93	Gl 34	B	00 46 03	+57 33.1	K7 V	7.51	1.39	168.4	8.64	

94	Gl 213		05 39 14	+12 29.3	M4	11.53	1.62	166.5	12.64	AC+12:1800-213
95	Gl 693		17 42 24	-57 16.9	M3.5	10.75	1.65	165.5	11.84	L 205-128 Sm 3
96	Gl 588		15 28 58	-41 05.6	M3	9.31	1.52	165.1	10.40	CP -40:7021 LTT 6210 comp. B is optical
97	Gl 268		07 06 39	+38 37.5	M4.5 Ve	11.49	1.71	164.6	12.57	Ross 986 AC +38:23616
98	Gl 784		20 10 19	-45 18.8	M0 V	7.97	1.43	163.9	9.04	Sm 50
99	NN 3323		04 59 33	-07 00.6	m	12.10		163.0	13.20	LP 656-38
100	GJ 1221		17 48 58	+70 52.4	DXP9	14.15	0.40	162.8	15.21	LP 44-113
101	Gl 338	A	09 10 59	+52 54.1	M0 Ve	7.62	1.39	162.5	8.67	LFT 634
102	Gl 338	B	09 11 01	+52 54.2	M0 Ve	7.71	1.42	162.5	8.76	LFT 635
103	NN 3454		07 33 43	+07 11.7	m	13.22		162.0	14.27	LTT 17993
104	Gl 285		07 42 04	+03 40.8	dM4.5e	11.20	1.60	161.1	12.24	YZ CMi Ross 882 LFT 547
105	GJ 1128		09 41 57	-68 40.3	m	12.78	1.73	161.0	13.81	
106	NN 3877		14 53 42	-27 57.1	dM8	17.05	1.34	161.0	18.08	LP 914-54 see in Ruiz et al AJ 100, p 1270
107	Gl 139		03 17 56	-43 15.6	G5 V	4.26	0.71	159.6	5.28	82 Eri LTT 1583
108	Gl 661	A	17 10 40	+45 44.8	M3 J	9.96	1.49	159.5	10.97	Kui 79 V (AB) = 9.38 d (m) = 0.48
109	Gl 661	B	17 10 40	+45 44.8	M3.5	10.40		159.5	11.40	a = 0.71" P = 12.98 yr
110	Gl 625		16 24 14	+54 25.1	dM2	10.12	1.61	159.3	11.13	AC+54:1646- 56 AC +55:41703
111	Gl 555		14 31 35	-12 18.6	M3	11.31	1.64	159.0	12.32	
112	Gl 581		15 16 50	-07 32.4	dM5	10.56	1.60	157.9	11.55	

113	GJ 2097		13 04 36	+21 05.0	m	12.58	1.62	156.0	13.55	LP 378-541 San 215
114	G1 19		00 23 09	-77 32.1	G2 IV	2.80	0.62	155.4	3.76	BET Hyi
115	G1 223.2		05 52 39	-04 08.8	DZ9	14.45	1.05	154.8	15.40	LP 658-002
116	G1 644	A	16 52 48	-08 14.7	M3 J	9.69	1.57	153.9	10.63	Wolf 630 V1054 Oph V (AB) = 9.02 d (m) = 0.18
117	G1 644	B	16 52 48	-08 14.7		9.90		153.9	10.80	a = 0.218" P = 1.715 yr
118	G1 644	C	16 52 55	-08 18.2	M7	16.78	1.99	153.9	17.72	VB 8 sep (AC) 221"
119	G1 881		22 54 54	-29 53.3	A3 V	1.16	0.09	153.7	2.09	ALF Psa
120	GJ 1156		12 16 32	+11 24.0	dM e	13.81	1.88	152.9	14.73	
121	G1 896	A	23 29 20	+19 39.7	dM4 e	10.38	1.54	151.9	11.29	EQ Peg
122	G1 896	B	23 29 20	+19 39.7	dM6 e	12.40	1.65	151.9	13.30	
123	G1 566	A	14 49 05	+19 18.4	G8 Ve	4.70	0.73	149.1	5.57	XI Boo
124	G1 566	B	14 49 05	+19 18.4	K4 Ve	6.97	1.16	149.1	7.84	
125	G1 66	A	01 37 54	-56 26.9	K2 V	5.80	0.86	148.9	6.66	P Eri CD- 56:329
126	G1 66	B	01 37 54	-56 26.9	K3 V	5.90	0.80	148.9	6.76	not in CpD
127	G1 880		22 54 10	+16 17.4	dM2 e	8.67	1.50	148.2	9.52	
128	G1 299		08 09 11	+08 59.7	dM5	12.83	1.77	148.0	13.68	Ross 619
129	G1 829		21 27 12	+17 25.1	dM4 e	10.30	1.63	147.8	11.15	AC+17:534- 105
130	NN 3716		12 10 53	+10 32.4	A2 m	5.85	0.27	147.5	6.70	FK 2978
131	NN 4285		22 34 27	-66 04.6	m	11.45		147.0	12.29	LTT 9108 L 119-44
132	G1 892		23 10 52	+56 53.5	K3 V	5.56	1.01	146.4	6.39	
133	G1 402		10 48 19	+07 05.1	dM5	11.65	1.67	145.1	12.46	Wolf 358
134	G1 293		07 52 52	-67 38.4	DQ9	14.08	0.66	144.7	14.88	L 97-12
135	G1 408		10 57 25	+23 06.3	M3	10.02	1.54	144.6	10.82	LTT 12942 AC+23:468- 46

136	NN 3322	S	wissenschaft in die schulen	04 59 14	+09 54.8	dM3	11.47	1.52	142.0	12.23	LP 476-207 Rob 285 Steph 538
137	G1 667	A		17 15 33	-34 56.2	K3 V	6.29	1.04	140.0	7.02	V(AB) = 5.91 d(m) = 0.95
138	G1 667	B		17 15 33	-34 56.2	K5 V	7.20		140.0	7.90	AB: a = 1.82" P = 42.09 yr
139	G1 667	C		17 15 34	-34 56.5	M2.5	10.24	1.57	140.0	10.97	sep(AC) 30.5" 129d - 30.8" 136d (1889-1948)
140	G1 17			00 17 29	-65 10.1	F9 V	4.22	0.58	139.0	4.94	ZET Tuc
141	NN 3737			12 36 10	-38 04.9	M4	12.74	1.69	139.0	13.46	LTT 4818 L 471-42
142	G1 514			13 27 27	+10 39.0	M1 V	9.05	1.50	138.7	9.76	
143	GJ 1286			23 32 34	-02 39.3	M5	14.69	1.96	138.6	15.40	
144	NN 4053			18 18 51	+66 10.5	m	13.48	1.83	137.3	14.17	LP 71-165
145	G1 393			10 26 23	+01 06.4	dM2.5	9.64	1.52	136.2	10.31	
146	GJ 1230	A		18 39 04	+24 44.2	k-m	12.40	1.71	136.0	13.10	
147	GJ 1230	B		18 39 04	+24 44.3	m	14.00		136.0	15.00	
148	G1 33			00 45 45	+05 01.4	K2 V	5.74	0.88	135.9	6.41	
149	G1 53	A		01 04 56	+54 40.5	G5 VI	5.17	0.69	134.5	5.81	MU Cas LTT 10400
150	G1 53	B		01 04 56	+54 40.5		11.00		134.5	12.00	
151	NN 4274			22 20 23	-17 51.0	M4	13.25	1.84	134.1	13.89	LTT 9001 L 788-34 LP 820-12
152	G1 809			20 52 18	+61 58.5	M2 Ve	8.55	1.48	133.5	9.18	
153	G1 178			04 47 07	+06 52.5	F6 V	3.19	0.45	133.1	3.81	1 PI(3) Ori
154	GJ 2005			00 22 12	-27 26.0	M5.5	15.42		132.8	16.04	pi(trig) in PASP 98,658 (86)
155	GJ 1224			18 04 42	-15 58.0	m	13.63	1.79	132.7	14.24	
156	G1 713	AB		18 21 57	+72 42.7	F7 V	3.57	0.49	132.6	4.18	CHI Dra

157	NN 3378	S	wissenschaft in die schulen	05 56 43	+59 36.5	m	11.71	1.60	132.2	12.32	LTT 11755 L 1813-21 LP 86-137
158	Gl 666	A		17 15 15	-46 35.1	G8 V	5.53	0.77	131.9	6.13	
159	Gl 666	B		17 15 15	-46 35.1	M0 V	8.69	1.41	131.9	9.29	
160	Gl 623			16 22 39	+48 28.4	dM3	10.28	1.48	131.7	10.88	AC+48:1595- 89 SBO in ApJ 344, 441
161	NN 3192	A		02 59 32	-16 47.0	M3	10.96	1.69	131.0	11.55	LTT 1445 L 730-18 LP 771-95 V (AB) = 10.54 d(m) = 0.8
162	NN 3193	B		02 59 32	-16 47.0	M3	11.80		131.0	12.40	LP 771-96 sep 4.5" 121d d(R) = 0.7, d(pg) = 0.8 (NLTT)
163	Gl 618	A		16 16 47	-37 25.4	M3	10.60	1.57	130.0	11.17	
164	Gl 618	B		16 16 47	-37 25.4	M5 :	14.15	1.79	130.0	14.72	
165	Gl 185	A		05 00 20	-21 19.4	M0 V J	8.46	1.41	129.6	9.02	V(AB) = 8.31 d(m) = 2.1 , dM1 J (Wilson)
166	Gl 185	B		05 00 20	-21 19.4		10.50		129.6	11.10	a = 1.40" P = 42.7 yr
167	Gl 721			18 35 15	+38 44.2	A0 V	0.03	0.00	129.6	0.59	ALF Lyr
168	Gl 105	A		02 33 20	+06 39.0	K3 V	5.82	0.98	129.4	6.38	LTT 10858 USNOP
169	Gl 105	B		02 33 31	+06 38.0	dM4.5	11.66	1.60	129.4	12.22	LTT 10859 USNOP
170	NN 3417			06 53 17	+62 23.7	m	13.65		129.0	14.20	
171	GJ 1093			06 56 29	+19 25.8	m	14.83	1.93	128.9	15.38	
172	Gl 673			17 23 16	+02 10.2	K7 V	7.53	1.36	128.9	8.08	
173	Gl 686			17 35 39	+18 36.4	dM1	9.62	1.53	128.9	10.17	AC+18:1453- 48
174	Gl 884			22 57 38	-22 47.6	K5/M0 V	7.88	1.39	128.4	8.42	dM1 Wil

175	GI 915	wissenschaft in die schulen	23 59 34	-43 26.1	DA5	13.05	0.07	128.2	13.59	LTT 9857 LP 988-88 L 362-081 BPM 45338
176	GI 879		22 53 37	-31 49.8	K5 Ve	6.48	1.10	128.1	7.02	TW Psa
177	GI 68		01 39 47	+20 01.6	K1 V	5.22	0.84	126.5	5.73	
178	GI 268.3		07 13 14	+27 14.0	dM0	10.85	1.54	126.0	11.35	
179	NN 3789		13 29 28	+29 32.0	M4 e	11.95	1.57	126.0	12.45	
180	GI 701		18 02 28	-03 01.9	dM2	9.38	1.52	125.9	9.88	
181	GI 109		02 41 18	+25 19.0	dM3.5	10.57	1.56	125.6	11.06	AC+25:7918
182	GI 831	A	21 28 34	-10 00.6	dM4.5e	12.05	1.67	125.6	12.54	Wolf 922 V (AB) = 11.97 d(m) = 2.83:
183	GI 831	B	21 28 34	-10 00.6		14.90		125.6	15.40	Wolf 922 sep 0.218" 157d A&AS 71, p 57
184	GJ 1087		05 53 47	+05 22.2	DAP9	14.10	0.60	125.1	14.59	
185	NN 3991		17 07 56	+43 45.3	M3	11.80	1.48	125.0	12.30	USNO 752 pos?
186	GI 216	A	05 42 23	-22 27.8	F6 V	3.58	0.47	124.9	4.06	GAM Lep
187	GI 216	B	05 42 21	-22 26.2	K2 V	6.13	0.94	124.9	6.61	
188	GJ 1276		22 51 09	-07 02.3	DZ9+	15.65	1.90	124.2	16.12	LP 701-29
189	NN 4063		18 32 58	+40 05.1	M3 p	11.42	1.42	124.0	11.90	LP 229-17
190	GJ 1105		07 54 47	+41 26.9	k	12.00	1.63	123.5	12.46	
191	GI 450		11 48 33	+35 32.8	M1 Ve	9.73	1.51	123.5	10.19	SB? in ApJ 314, 272
192	GJ 2034		04 19 36	-48 46.1	DA8	14.36	0.52	123.0	14.81	LTT 1951 LFT 349 L302-89 BPM 31852
193	GJ 1123		09 17 32	-77 37.0	m	13.10	1.64	123.0	13.55	
194	GJ 1289		23 40 33	+36 15.7	k	12.57	1.60	123.0	13.02	
195	GI 493.1		12 58 05	+05 57.1	dM5 e	13.40	1.75	122.8	13.85	LTT 13750 Wolf 461

196	GI 799	A	20 38 44	-32 36.6	dM4.5e	10.99	1.57	122.8	11.44	AT Mic V (AB) = 10.24 d(m) = 0.0
197	GI 799	B	20 38 44	-32 36.6	dM4.5e	11.00		122.8	11.40	sep 3.9" (1962)
198	GI 747	A	19 05 45	+32 27.0	M3.5 J	11.86	1.70	122.6	12.30	AC +32:54804 ADS 12061C V(AB) = 11.25 d(m) = 0.3
199	GI 747	B	19 05 45	+32 27.0	M5 K	12.16		122.6	12.60	sep < 0.35"
200	GI 518		13 34 13	+03 57.0	DZ9	14.65	0.95	122.2	15.09	Wolf 489
201	GJ 1151		11 48 29	+48 40.1	m	13.25	1.84	121.8	13.68	
202	GJ 1227		18 22 05	+62 02.3	m	13.41	1.76	121.3	13.83	
203	GI 479		12 35 11	-51 43.6	M3	10.67	1.54	121.1	11.09	CP -51: 5356
204	GI 54		01 08 34	-67 43.1	k	9.80	1.54	120.9	10.21	
205	GI 117		02 50 07	-12 58.3	K2 V	6.03	0.87	120.4	6.43	
206	GI 793		20 29 50	+65 16.6	dM3	10.56	1.56	120.4	10.96	AC+65:6955 mu(GSC- AC) 0.522" 57.5d opt. comp. 33." 149d (1983.68)
207	GI 232		06 21 37	+23 28.1	M4.5	13.06	1.76	120.0	13.46	Ross 64
208	GI 877		22 52 12	-75 42.7	k	10.40	1.49	119.9	10.79	L 049-019
209	GI 502		13 09 32	+28 07.9	G0 V	4.26	0.57	119.8	4.65	BET Com
210	GI 438		11 40 49	-51 33.3	K0	10.36	1.53	119.0	10.74	
211	NN 3146		02 13 47	+13 22.1	m	15.79	1.98	118.2	16.15	USNO 694 LP 469-206
212	GJ 1154	AB	12 11 46	+00 54.2	m	13.73	1.77	118.2	14.09	LTT 13408 V (AB) = 13.42 d(m) = 1.2 , sep 5" optical
213	GJ 1057		03 10 39	+04 35.2	m	13.80	1.82	118.1	14.16	
214	NN 3076		01 08 46	+15 10.5	m	14.36		118.0	14.72	LP 467-16 L 1157-47 LTT 10436

215	Gl 84		02 02 37	-17 51.1	M3	10.19	1.51	118.0	10.55	L 727-32
216	Gl 381		10 09 31	-02 25.8	dM0	10.63	1.57	117.3	10.98	L 968-022 LP 609-71 comp.(?) at 25" d(m) = 2. (Worley), no cpm
217	Gl 257	A	06 56 21	-44 13.3	M3	11.50	1.66	116.9	11.80	V(AB) = 10.84 d(m) = 0.2
218	Gl 257	B	06 56 21	-44 13.3	M3	11.70		116.9	12.00	
219	NN 3517		08 51 07	-03 17.9	m	18.80		116.8	19.14	LP 666-9
220	Gl 382		10 09 46	-03 29.7	dM2	9.27	1.48	116.7	9.61	uncertain comp. 25" d (m) = 1. (Worley)
221	Gl 487		12 47 04	+66 23.0	M3	10.90	1.64	116.2	11.23	AC+66:3955 LTT 13665 (= LTT 13669?)
222	Gl 434		11 38 25	+34 29.0	G8 Ve	5.33	0.72	116.0	5.65	
223	Gl 451	A	11 50 06	+38 04.7	G8 VI	6.45	0.75	116.0	6.77	
224	Gl 451	B	11 50 06	+38 04.7		12.00		116.0	12.00	CF Uma sep 2" 175d; but speckle obs. sep < 0.03" 1979.80
225	Gl 486		12 45 29	+10 01.9	dM4	11.38	1.57	115.6	11.69	Wolf 437
226	Gl 48		00 58 48	+71 25.0	dM3.5e	10.04	1.46	115.5	10.35	AC+71:532
227	Gl 827		21 22 20	-65 35.6	F8 V	4.22	0.49	115.5	4.53	GAM Pav
228	Gl 867	A	22 36 01	-20 52.8	dM2 e	9.10	1.51	115.4	9.41	FK Aqr MOVEP Mich
229	Gl 867	B	22 36 01	-20 52.8	dM4 e	11.45	1.60	115.4	11.76	L 717-022
230	Gl 695	A	17 44 30	+27 44.9	G5 IV	3.42	0.75	115.1	3.73	MU Her ADS 10786 sep(AB) 29.9" 241d - 34.0" 247d (1831-1955)

231	Gl 695	B	17 44 28	+27 44.7	M3 J	10.35	1.49	115.1	10.66	V(BC) = 9.80 d(m) = 0.45 , a = 1.360" 43.20 yr
232	Gl 695	C	17 44 28	+27 44.7	M4 K	10.80		115.1	11.10	
233	NN 3839		14 14 55	+31 56.7	m	13.10		115.0	13.40	LFT 1085 LTT 14193 LP 325-15 L 1484-43
234	Gl 475		12 31 22	+41 37.7	G0 V	4.27	0.59	114.7	4.57	BET Cvn
235	Gl 849		22 07 00	-04 53.2	dM3.5	10.37	1.51	114.4	10.66	
236	Gl 791.2		20 27 21	+09 31.2	dM6 e	13.05	1.65	114.2	13.34	LTT 15983 HU Del
237	Gl 231		06 11 44	-74 44.2	G5 V	5.08	0.72	114.1	5.37	ALF Men
238	GJ 2066		08 13 34	+01 27.4	m	10.10	1.53	114.0	10.38	
239	GJ 2069	A	08 28 46	+19 34.0	M5 e	11.89		114.0	12.17	G040-025
240	GJ 2069	B	08 28 46	+19 34.2		13.32		114.0	13.60	
241	Gl 424		11 17 29	+66 07.0	M1 V	9.31	1.41	114.0	9.59	SZ Uma
242	NN 3667		11 26 42	+18 33.2	DC8	13.79		114.0	14.07	WD1126 +185 PG
243	Gl 70		01 40 46	+04 04.9	dM2	10.93	1.54	113.8	11.21	AC+03:2259- 31
244	GJ 1103	A	07 49 20	+00 08.1	m	13.50	1.68	113.8	13.78	LP 603-1 L 961-1 V(AB) = 13.26 d(m) = 1.5
245	GJ 1103	B	07 49 21	+00 08.2	m	15.00		113.8	15.30	LP 603-2 sep 3" 78d d(R) = 1.3, d(pg) = 1.0 (LHS)
246	Gl 49		00 59 27	+62 04.5	K5 V	9.56	1.50	112.6	9.82	LFT 94 Wolf 46
247	Gl 318		08 39 36	-32 46.9	DA6	11.88	0.22	112.3	12.13	
248	Gl 745	A	19 04 58	+20 48.8	sdM2	10.76	1.58	112.2	11.01	AC+20:1463- 148
249	Gl 745	B	19 05 05	+20 48.1	sdM2	10.75	1.58	112.2	11.00	AC+20:1463- 154
250	Gl 465		12 22 13	-17 56.0	dM4	11.28	1.60	112.1	11.53	Ross 695

251	GI 506	wissenschaft in die schulen	13 15 47	-18 02.0	G6 V	4.74	0.71	112.1	4.99	
252	NN 3128		01 59 37	+10 06.0	m	15.61	2.02	112.0	15.86	LP 469-67 USNO 693
253	GI 283	A	07 38 02	-17 17.4	DZQ6	13.00	0.24	112.0	13.25	L 745-046
254	GI 283	B	07 38 02	-17 17.4	m	16.42	1.83	112.0	16.67	
255	NN 3707		12 07 31	-14 47.0	m	12.06	1.58	112.0	12.31	LP 734-32
256	GI 512.1		13 25 59	+14 02.7	G2.5 Va	4.98	0.71	112.0	5.23	BS 5072
257	NN 3820		13 56 27	-19 35.4	K2 :	13.00		112.0	13.20	LTT 5455 L 763-63 LP 799-7
258	NN 4247		21 58 56	+28 03.9	m+	12.01	1.63	112.0	12.26	
259	GI 357		09 33 43	-21 25.4	M3 V	10.92	1.57	111.6	11.16	L 678-039
260	GI 595		15 39 20	-19 18.6	M3.5	11.87	1.60	111.0	12.10	L 768-119
261	NN 4360		23 42 58	-16 26.5	m	14.50		111.0	14.70	LP 823-4
262	GI 51		01 00 08	+62 05.8	M5	13.66	1.68	110.9	13.88	Wolf 47 cpm with GI 49 ?
263	GI 183		04 58 20	-05 48.6	K3 V	6.22	1.06	110.7	6.44	
264	NN 3421		06 59 54	+52 47.5	M4.5	13.30	1.84	109.1	13.49	LTT 11965 LFT 506 LP 122-59 L 1750-5
265	GI 250	A	06 49 52	-05 06.7	K3 V	6.59	1.05	108.9	6.78	
266	GI 250	B	06 49 52	-05 07.7	M2	10.09	1.50	108.9	10.28	
267	GI 367		09 42 37	-45 32.3	M3	10.11	1.53	108.8	10.29	CP-45:3978 LTT 3579
268	GI 785		20 12 10	-27 11.0	K0 V	5.73	0.88	108.8	5.91	
269	GI 91		02 11 40	-32 16.0	M2.5	10.32	1.50	108.5	10.50	
270	GI 352	A	09 28 53	-13 16.1	M3 J	10.81	1.53	107.9	10.98	Kui 41 V (AB) = 10.06 d(m) = 0.0
271	GI 352	B	09 28 53	-13 16.1		10.80		107.9	11.00	a = 0.551" P = 18.3 yr
272	NN 3380		05 58 36	+49 52.4	m	14.47	1.87	107.8	14.63	
273	GJ 1253		20 24 58	+58 24.0	M5	14.04	1.79	107.6	14.20	Wolf 1069

274	GI 176	wissenschaft in die schulen	04 39 58	+18 52.8	dM2.5e	9.98	1.52	107.4	10.14	
275	GI 902		23 36 41	-72 59.3	K3 V	7.07	0.99	107.4	7.23	
276	GI 803		20 42 04	-31 31.1	M0 Ve	8.81	1.42	106.9	8.95	AU Mic
277	GJ 2033		04 14 22	-12 41.0	k-m	10.87	1.55	106.0	11.00	LTT 1919 L 806-34
278	NN 3988		17 02 11	+51 28.0	k-m	13.56	1.75	105.2	13.67	
279	NN 3306		04 35 24	-08 53.9	DQ7	13.77	0.33	105.1	13.88	L 879-014 LTT 2049 L 879-14 LP 655-42
280	GI 226		05 59 42	+82 07.9	M2.5	10.50	1.51	105.0	10.61	AC+82:1111
281	GI 649		16 56 07	+25 49.6	dM2	9.65	1.50	105.0	9.76	
282	GJ 1065		03 48 18	-06 13.6	dM4	12.79	1.70	104.9	12.89	
283	GI 542		14 15 30	-59 08.3	K3 V	6.66	1.03	104.9	6.76	
284	GI 534		13 52 18	+18 38.9	G0 IV	2.68	0.58	104.7	2.78	ETA Boo
285	GI 654		17 02 37	-05 00.7	M3.5V	10.08	1.44	104.7	10.18	Wolf 636 LFT 1317 comp. to GI 653 sep 18.5" 146d
286	GI 633		16 37 09	-45 54.2	M3	12.68	1.61	104.6	12.78	L 339-019 LTT 6662
287	GI 137		03 16 44	+03 11.3	G5 Ve	4.82	0.68	104.5	4.92	KAP Cet
288	GJ 1207		16 54 26	-04 16.0	dM3.5	12.28	1.60	104.4	12.37	
289	GJ 1001		00 02 05	-40 57.8	M3.5	12.84	1.63	104.2	12.93	LTT 20
290	NN 3253		03 49 49	+16 52.7	M4.5	13.70		104.0	13.80	LTT 11284 Wolf 227
291	NN 3275		04 19 13	+19 08.5	dM4.5e	12.90	1.70	104.0	13.00	LP 415-636 BPM 85717
292	GI 150		03 40 51	-09 55.9	K0 IVe	3.53	0.92	103.5	3.60	DEL Eri
293	NN 3855		14 29 21	+59 56.2	M6.5	17.88		103.3	17.95	LP 98-79
294	GI 370		09 49 05	-43 15.7	K5 V	7.64	1.18	103.2	7.71	
295	GI 638		16 43 15	+33 35.7	K7 V	8.11	1.37	103.2	8.18	

296	G1 222	AB	05 51 25	+20 16.1	G0 V	4.40	0.59	103.1	4.47	BS 2047 CHI (1) Ori sep 0.6" d(m) = ? comp see AJ 72,910
297	G1 508	A	13 17 36	+48 02.4	dM1.5eJ	8.94	1.48	103.0	9.00	ADS 8862 V (AB) = 8.54 d (m) = 0.86
298	G1 508	B	13 17 36	+48 02.4		9.80		103.0	9.90	a = 1.465" P = 48.85 yr
299	G1 691		17 40 10	-51 48.6	G5 V	5.14	0.70	103.0	5.20	MU Ara
300	G1 102		02 30 44	+24 42.9	M4	12.96	1.70	102.4	13.01	L 1305-010
301	GJ 1138		10 47 00	+35 49.5	m	13.02	1.66	102.4	13.07	
302	G1 413.1		11 07 07	-24 19.3	M3	10.44	1.53	102.1	10.49	LTT 4108
303	NN 3978		16 49 11	+38 14.0	dK8	10.55	1.59	102.0	10.59	AG+38:1528
304	G1 453		11 55 27	-27 25.2	K5 V	6.98	1.15	101.9	7.02	
305	G1 519		13 35 13	+35 58.4	dM1	9.04	1.42	101.9	9.08	
306	G1 432	A	11 32 03	-32 34.0	K0 V	5.98	0.81	101.7	6.02	
307	G1 432	B	11 32 04	-32 34.1	m	15.00		101.7	15.00	VB 4
308	G1 694		17 42 25	+43 24.4	dM3.5	10.47	1.53	101.7	10.51	
309	GJ 1256		20 38 10	+15 18.7	dM4-5	13.43	1.72	101.6	13.46	
310	NN 3049		00 41 05	-41 33.6	M4	13.10		101.0	13.10	LFT 69 LTT 400 L 363-38 LP 989-140
311	NN 3992		17 09 52	+38 30.1	m	11.61		101.0	11.63	LTT 15087 Wolf 654
312	GJ 2012		00 38 58	-22 37.2	DQ9	14.53	0.62	100.8	14.55	
313	G1 228	A	06 08 09	+10 20.6	dM2.5 J	10.58	1.46	100.8	10.60	V(AB) = 10.41 d(m) = 1.9
314	G1 228	B	06 08 09	+10 20.6		12.50		100.8	12.50	sep 0.9" to 2.4" (1945- 61)

315	Gl 22	AC	00 29 20	+66 57.8	dM2.5e	10.38	1.54	100.6	10.39	V547 Cas V (AB) = 10.34 d(m) = 3.7 sep (AC) 0.4" d(K) = 1.94
316	Gl 22	B	00 29 20	+66 57.8	dM3.5	12.40		100.6	12.40	sep(AC-B) 4" d(K)(AC- B) = 1.35
317	Gl 286		07 42 16	+28 08.9	K0 IIIb	1.14	1.00	100.3	1.15	BET Gem
318	NN 3512		08 37 21	+59 41.6	m	15.05	1.93	100.2	15.05	LP 90-18
319	GJ 1028		01 02 21	-18 23.9	m	14.46	1.87	100.0	14.46	
320	NN 3119		01 48 32	-06 21.8	m	14.60		100.0	14.60	
321	NN 3126		01 57 56	+63 31.8	M4	11.03	1.54	100.0	11.03	
322	NN 3304		04 35 04	+28 07.1	m	12.53	1.65	100.0	12.53	LTT 11472
323	NN 3959		16 29 39	+40 58.0	m+	14.79	1.72	100.0	14.80	
324	NN 3976		16 48 50	+22 31.8	m	14.08	1.75	100.0	14.08	
325	Gl 678.1	A	17 27 55	+05 35.4	M1 V	9.30	1.49	100.0	9.30	comp B optical
326	NN 4248		21 59 27	-37 19.2	M3.5	11.80	1.65	100.0	11.80	LTT 8811 L 499-56 LP 983-71
327	Gl 203		05 25 16	+09 36.8	M3.5	12.48	1.64	99.7	12.47	Ross 41
328	Gl 341		09 20 24	-60 04.2	M0 V	9.50	1.48	99.4	9.50	CD-59:2351 LTT 3453 L 140-9
329	Gl 609		16 00 43	+20 44.6	M3	12.56	1.63	99.4	12.55	L 1346-53
330	Gl 748		19 09 38	+02 48.6	dM4	11.10	1.51	99.4	11.09	AC+02:2155- 242
331	Gl 239		06 34 19	+17 36.2	dM1	9.63	1.49	99.1	9.61	
332	NN 3079		01 09 55	-02 07.3	DAwk	14.09		99.0	14.07	GD 806

333	Gl 635	A	16 39 24	+31 41.5	G0 IV	2.91	0.65	99.0	2.89	ZET Her ADS 10157 V(AB) = 2.81 d(m) = 2.52
334	Gl 635	B	16 39 24	+31 41.5	K0 V	5.40		99.0	5.40	a = 1.355" P = 34.487 yr
335	Gl 846		21 59 39	+01 09.7	M0.5 V	9.18	1.48	98.9	9.16	
336	Gl 436		11 39 31	+26 59.8	dM3.5	10.67	1.52	98.8	10.64	AC +27:28217
337	Gl 449		11 48 05	+02 02.8	F9 V	3.61	0.55	98.8	3.58	BET Vir
338	Gl 754.1	A	19 17 53	-07 45.6	DQ5	12.28	0.06	98.8	12.25	LTT 7658 L 923-21 LDS 678A AC- 07:342-402
339	Gl 754.1	B	19 17 51	-07 45.3	dM5	12.12	1.63	98.8	12.09	AC-07:342- 397 L 923-22
340	Gl 482	A	12 39 07	-01 10.5	F0 V	3.46	0.36	98.7	3.43	GAM Vir ADS 8630 V (AB) = 2.74 d (m) = 0.06
341	Gl 482	B	12 39 07	-01 10.5	F0 V	3.52		98.7	3.49	
342	Gl 172		04 33 43	+52 48.0	K8 Ve	8.61	1.40	98.5	8.58	
343	GJ 1125		09 28 12	+00 33.0	M3.5	11.71	1.59	98.4	11.67	
344	GJ 1235		19 19 32	+20 47.5	k-m	13.38	1.71	98.4	13.34	
345	NN 3526		08 58 19	+68 15.2	m	12.65		98.3	12.61	LP 60-179
346	Gl 373		09 52 29	+63 02.0	dM1	9.00	1.43	98.3	8.96	
347	Gl 92		02 14 00	+33 59.8	G0 Ve	4.87	0.61	98.1	4.83	BS 660 DEL Tri SBO (A&A 195, 129)
348	Gl 606		15 57 11	-08 06.8	dM0	10.50	1.51	98.1	10.46	
349	Gl 852	A	22 14 42	-09 03.0	dM4.5e	13.40	1.70	98.1	13.40	Wolf 1561
350	Gl 852	B	22 14 42	-09 03.0	dM5 e	14.40	1.90	98.1	14.40	
351	GJ 1129		09 42 32	-17 58.8	m	12.60	1.59	98.0	12.56	
352	Gl 372		09 50 41	-03 26.9	dM0	10.54	1.52	98.0	10.50	

353	NN 3571	S	wissenschaft in die schulen	09 51 09	+21 10.6	m	14.05		98.0	14.01	
354	GJ 1264			21 44 34	-72 19.9	M2 Ve	9.80	1.46	98.0	9.80	CP-72:2640 LTT 8698 AY Ind
355	GJ 358			09 37 49	-40 50.7	M3	10.75	1.53	97.6	10.70	L 390-5
356	GJ 75			01 44 06	+63 36.4	K0 V	5.63	0.81	97.2	5.57	
357	GJ 442	A		11 44 08	-40 13.7	G5 V	4.90	0.66	97.1	4.84	
358	GJ 442	B		11 44 09	-40 13.4		15.00		97.1	15.00	VB 5
359	NN 3182			02 45 03	+54 11.1	DC9	15.32	0.93	97.0	15.25	
360	GJ 1083	AB		05 37 21	+24 46.9	m	14.85	1.88	96.7	14.78	Riepe's double sep 0.6" 315d
361	GJ 339.1			09 12 29	+53 38.9	DXP7	13.85	0.34	96.7	13.78	
362	NN 3147			02 14 08	+35 12.9	m+	15.99		96.6	15.91	LP 245-10
363	GJ 1119			08 57 11	+46 47.3	m	13.32	1.72	96.6	13.24	
364	GJ 909	A		23 49 57	+75 15.9	K3 V	6.40	0.98	96.5	6.32	
365	GJ 909	B		23 49 57	+75 15.9	M2	11.70		96.5	11.60	
366	GJ 1134			10 38 53	+37 52.6	m	12.98	1.68	96.2	12.90	
367	GJ 452.1			11 51 34	+10 05.7	M3.5	12.77	1.69	96.1	12.68	Ross 119
368	GJ 423	A		11 15 31	+31 48.6	G0 Ve	4.33	0.59	96.0	4.24	XI Uma ADS 8119 V (AB) = 3.79 d (m) = 0.47
369	GJ 423	B		11 15 31	+31 48.6	G0 Ve	4.80		96.0	4.70	s = 2.530" P = 59.840 yr, Aa-P: a = 0.05" P = 1.832 yr
370	NN 3804			13 43 09	-17 42.6	M3.5	11.86	1.56	96.0	11.80	LTT 5346 L 762-51 LP 798-34
371	NN 4071			18 40 27	+13 51.0	m	12.81		96.0	12.72	LTT 15516 L 1209-6 LP 510-15
372	GJ 170			04 26 59	+39 44.9	M4.5	13.91	1.73	95.9	13.82	Ross 594

373	GI 320	wissenschaft in die schulen	08 41 26	-38 42.4	K1 V	6.56	0.93	95.9	6.47	
374	GJ 1265		22 10 56	-17 55.8	m	13.57	1.73	95.8	13.48	
375	GI 569	AB	14 52 08	+16 18.3	dM0 e	10.20	1.48	95.6	10.10	CE Boo comp 5.1" 17.5d
376	GI 218		05 45 53	-36 20.6	M3	10.73	1.48	95.5	10.63	
377	GI 27		00 36 45	+20 58.9	K0+ V	5.85	0.85	95.1	5.74	
378	GI 536		13 58 31	-02 25.3	M1	9.70	1.46	95.1	9.59	
379	GI 631		16 33 44	-02 13.2	K0 Ve	5.75	0.82	95.1	5.64	
380	NN 3125		01 57 25	+73 18.1	m	14.12	1.90	95.0	14.01	LP 30-55
381	NN 3270		04 14 35	+08 42.3	dM4 e	13.82		95.0	13.71	LTT 11392 Rob 270
382	GJ 2036	A	04 52 30	-55 56.0	M2 Ve	11.13	1.57	95.0	11.00	LDS 131A BPM 17964
383	GJ 2036	B	04 52 30	-55 56.0		12.15	1.60	95.0	12.00	LDS 131B BPM 17965 sep 9" Eggen
384	NN 3849		14 26 37	+33 24.6	dM9	19.74		95.0	19.63	LP 271-25
385	GI 740		18 55 34	+05 51.4	M2 V	9.22	1.46	94.6	9.10	
386	GI 431		11 29 23	-40 46.3	M3.5	11.52	1.54	94.3	11.39	L 396-007
387	NN 3010		00 06 20	+20 33.9	m	13.54		94.0	13.41	LTT 10045
388	GI 173		04 35 21	-11 08.1	dM1	10.36	1.50	94.0	10.23	
389	NN 3801		13 40 29	+33 33.1	M3	11.97	1.64	94.0	11.80	LTT 13999 Ross 1015
390	GI 568	A	14 51 41	+23 45.5	M3.5 J	12.19	1.61	93.9	12.05	Ross 52 V (AB) = 11.66 d(m) = 0.5
391	GI 568	B	14 51 41	+23 45.5		12.70		93.9	12.60	a = 0.69" P = 34.1 yr Heintz AJ 99, 420 (1990)
392	GI 136		03 16 41	-62 46.0	G2 V	5.54	0.64	93.6	5.40	ZET(1) Ret
393	GJ 1232		19 07 40	+17 35.5	k-m	13.52	1.85	93.6	13.38	
394	GI 669	A	17 17 54	+26 32.8	dM4 e	11.42	1.55	93.3	11.27	Ross 868

395	Gl 669	B	17 17 53	+26 32.8	dM5 e	12.97	1.64	93.3	12.82	Ross 867
396	Gl 766	A	19 43 43	+27 01.2	dM4.5 J	12.91	1.72	93.1	12.75	Ross 165 V (AB) = 12.38 d(m) = 0.5
397	Gl 766	B	19 43 43	+27 01.2		13.40		93.1	13.20	a = 1.10" P = 81 yr Heintz AJ 101, 1071
398	GJ 1041	A	01 56 36	+03 16.5	k-m	10.98	1.52	93.0	10.82	V(AB) = 10.91 d(m) = 3.
399	GJ 1041	B	01 56 36	+03 16.5	m	14.00		93.0	13.80	LP 589-9 sep 4" 75d d(R) = 2.6 d(pg) = 3.1 (NLTT)
400	NN 4333		23 19 09	+17 02.1	m	11.72	1.51	92.8	11.56	LTT 16862 LFT 1785 L 1295-31 LP 462-27
401	Gl 47		00 58 13	+61 06.5	dM2.5e	10.83	1.57	92.4	10.66	AC+60:3496
402	Gl 124		03 05 27	+49 25.4	G0 V	4.05	0.60	92.4	3.88	IOT Per Heintz AJ 96 : double?
403	Gl 624		16 23 04	-69 58.5	G0 V	4.91	0.55	92.4	4.74	ZET Tra
404	NN 3928		15 53 39	+35 20.6	m	13.68		92.0	13.50	
405	GJ 1284		23 27 35	-20 39.8	M2 Ve	11.16	1.51	92.0	11.00	
406	NN 4281		22 26 15	-13 39.8	M6.5	17.14	2.16	91.9	16.96	LP 760-3 Mv = 17.03 +- .14 G&L ApJ 305, 784
407	Gl 821		21 06 30	-13 28.7	M3	10.87	1.50	91.7	10.68	Wolf 918
408	Wo 9520		15 19 38	+21 09.3	dM0 e	10.11	1.51	91.6	9.92	BPM 90688
409	NN 3412	AB	06 49 29	+60 56.8	M3.5	11.06	1.54	91.5	10.87	LTT 11937 LP 87-237 L 1815-5 Hei 334 d(m) = 0.5 V(AB) = 10.52
410	GJ 1236		19 19 39	+06 57.2	m	12.35	1.69	91.5	12.16	

411	Gl 541	wissenschaft in die schulen	14 13 23	+19 26.5	K2 III ep	-0.10	1.20	91.2	-0.30	ALF Boo
412	Gl 545		14 17 29	-09 22.8	M4	12.90	1.59	91.1	12.70	Ross 848
413	NN 3210		03 11 18	-54 18.0	DZ7	14.75	0.52	91.0	14.55	BPM 17113 L 227-140
414	Gl 856	A	22 21 12	+32 12.5	dM0 eJ	11.41	1.57	91.0	11.21	AC +31:68884 V (AB) = 10.75 d(m) = 0.2
415	Gl 856	B	22 21 12	+32 12.5		11.60		91.0	11.40	sep 1.4" 145d (1964)
416	Gl 410		10 59 57	+22 14.2	dM2 e	9.60	1.48	90.9	9.39	
417	Gl 428	A	11 22 29	-61 22.4	K7 V	7.50	1.26	90.9	7.29	V(AB) = 7.21 d(m) = 1.31
418	Gl 428	B	11 22 29	-61 22.4	M0 Ve	8.30		90.9	8.10	a = 5.760" P = 421.5 yr
419	GJ 1097		07 26 14	-03 11.2	M3	11.43	1.50	90.8	11.22	
420	GJ 1004		00 09 40	+50 09.2	DA8	14.36	0.42	90.7	14.15	
421	GJ 1238		19 25 40	+75 26.7	m+	15.37	1.94	90.7	15.16	
422	Gl 190		05 06 21	-18 12.9	M4	10.30	1.50	90.6	10.09	L 737-009
423	GJ 1086		05 48 46	-00 11.3	DQP8	14.55	0.48	90.5	14.33	LTT 17876
424	Gl 433		11 32 58	-32 15.1	M2 V	9.83	1.51	90.5	9.61	
425	Gl 63		01 35 07	+56 58.9	dM3	11.19	1.39	90.3	10.97	AC +56:13511
426	NN 3140		02 07 33	+11 18.0	dM4	12.72		90.0	12.50	Rob 115
427	NN 3396		06 28 18	+41 32.1	m	14.83		90.0	14.60	LP 205-49
428	Gl 362		09 38 39	+70 16.3	M3	11.22	1.52	90.0	10.99	AC+70:4337
429	NN 3592		10 13 12	-55 55.0	DZ9	15.10	0.68	90.0	14.87	BPM 19929 L 190-21
430	NN 4078		18 45 22	-57 29.0	m	12.70		90.0	12.50	LTT 7454 L 207-41
431	GJ 1277		22 53 25	-60 18.3	M4	14.08	1.79	90.0	13.85	
432	Gl 494		12 58 19	+12 38.7	dM1.5e	9.75	1.47	89.9	9.52	DT Vir

433	Gl 865		22 34 57	-65 38.2	k-m	11.48	1.61	89.9	11.25	L 119-021 Sm 113 LHS: may have a comp. 13" 189d
434	Gl 386		10 14 20	-11 42.2	dM0	10.98	1.47	89.7	10.74	L 824-28
435	Gl 86		02 08 25	-51 04.1	K0 V	6.12	0.82	89.4	5.88	LTT 1130
436	GJ 1187		14 56 29	+56 51.8	m	15.53	1.95	89.4	15.29	
437	NN 3967		16 37 32	+00 48.3	m	13.69	1.70	89.3	13.44	LP 625-34
438	GJ 1148		11 39 09	+43 01.8	M3.5	11.90	1.52	89.1	11.65	Ross 1003
439	Gl 537	A	14 00 32	+46 34.9	dM3 e	9.85	1.48	89.1	9.60	
440	Gl 537	B	14 00 32	+46 34.9	dM3 e	9.95		89.1	9.70	
441	NN 4065		18 34 01	+13 33.7	M3.5	12.46		89.0	12.21	LTT 15483 Ross 149
442	Gl 653		17 02 27	-04 59.0	K5 V	7.73	1.16	88.7	7.47	Wolf 635 LFT 1316
443	Gl 706		18 07 58	+38 27.2	K2 V	6.40	0.87	88.7	6.14	
444	Gl 838.6		21 51 37	-47 14.1	M1	11.98	1.56	88.7	11.72	L 355-062 Sm 93
445	Gl 327		08 51 50	-05 14.6	G3 V	6.00	0.67	88.6	5.74	
446	Gl 349		09 27 19	+05 52.4	K3 Ve	7.20	1.00	88.6	6.94	
447	Gl 735		18 53 03	+08 20.3	dM3 e	10.11	1.53	88.6	9.85	AC+08:142- 393
448	Gl 399		10 37 12	-06 39.7	m	11.30	1.53	88.5	11.03	L 897-16
449	Gl 325	A	08 50 44	+70 59.4	K5 V	8.70	1.39	88.4	8.43	ADS 7067 V (AB) = 8.03 d (m) = 0.18
450	Gl 325	B	08 50 44	+70 59.4	K6 V	8.90		88.4	8.60	a = 5.73" P = 680 yr
451	Gl 617	A	16 16 37	+67 21.5	M0 Ve	8.60	1.41	88.3	8.33	
452	Gl 617	B	16 16 39	+67 22.6	M2.5	10.72	1.49	88.3	10.45	
453	NN 3148	A	02 14 27	-31 13.4	M4	12.00		88.0	11.70	LFT 200 LTT 1165 L 512-14

454	NN 3149	S	02 14 21	-31 12.2	M4	13.00		88.0	13.00	LFT 199 LTT 1164 L 512-15 LP 885-38 sep 105" 312d
455	NN 3909		15 29 19	+14 25.7	G5	7.70		88.0	7.42	
456	NN 4048	A	18 16 25	+38 46.2	m	11.87	1.58	88.0	11.59	
457	NN 4049	B	18 16 24	+38 46.2	m	13.53	1.77	88.0	13.25	sep 8.5" 290d
458	Gl 138		03 17 07	-62 41.8	G1 V	5.24	0.60	87.5	4.95	ZET(2) Ret LTT 1576
459	Gl 103		02 32 28	-44 00.6	K7 Ve	8.85	1.39	87.2	8.55	CC Eri
460	Gl 739		18 55 20	-48 20.2	M3	11.15	1.46	87.1	10.85	CFS 18398 Sm 26
461	Gl 2		00 02 32	+45 30.6	dM2 e	9.93	1.49	87.0	9.63	
462	Gl 4	A	00 03 02	+45 32.2	dK6 e	8.97	1.44	87.0	8.67	ADS 48AB d (m) = 0.09
463	Gl 4	B	00 03 02	+45 32.1	M0.5 V	9.02	1.45	87.0	8.72	a = 6.179" P = 362.3 yr or a = 11.698" P = 1506.68 yr
464	NN 3500		08 25 40	-44 49.7	M3	11.85		87.0	11.55	LTT 3139 L 387-102
465	Gl 317		08 38 49	-23 17.3	m	11.98	1.52	87.0	11.68	L 675-081
466	NN 3550		09 16 33	+73 19.8	m	15.02	1.90	87.0	14.70	LP 36-181
467	Gl 356	A	09 32 40	+36 02.2	G8 V	5.41	0.77	87.0	5.11	
468	Gl 356	B	09 32 40	+36 02.2		13.00		87.0	12.70	a = 3.84" P = 201 yr Heintz AJ 94, p 1077
469	Gl 534.1	A	13 53 14	-54 27.4	G8 V	6.00	0.78	87.0	5.70	
470	Gl 534.1	B	13 53 14	-54 26.0		13.80		87.0	13.50	L 259-140 sep 33" nf d (pg) = 7.1 (NLTT)

471	GI 553.1	wissenschaft in die schulen	14 28 20	-12 04.1	M3	11.92	1.57	87.0	11.60	AC-12:2306-155
472	NN 3966		16 33 37	+35 07.2	m	12.95		87.0	12.65	LP 275-68
473	GI 567		14 51 07	+19 21.2	K2 V	6.02	0.84	86.9	5.72	
474	GI 96		02 18 57	+47 39.1	dM1.5e	9.41	1.49	86.8	9.10	
475	GI 87		02 09 51	+03 22.0	dM2.5	10.06	1.44	86.7	9.75	
476	GI 275.2	A	07 27 02	+48 19.4	sdM5	13.56	1.71	86.5	13.25	
477	GI 275.2	B	07 27 06	+48 17.8	DC	14.63	0.99	86.5	14.32	
478	GI 12		00 13 12	+13 16.4	dM3.5	12.58	1.66	86.3	12.26	LP 462-42 L 1154-029
479	GI 208		05 33 44	+11 17.9	dM0	8.80	1.40	86.1	8.48	
480	GI 212		05 37 27	+53 28.3	M1	9.75	1.48	86.1	9.43	
481	GI 772		19 53 56	-01 10.0	DA6	13.70	0.28	86.1	13.38	LTT 7879 LFT 1503 LP 634-1 L 997-021
482	NN 3039		00 30 00	+07 13.0	m	12.70		86.0	12.37	LP 525-39
483	GI 78		01 49 19	-11 02.6	M3.5	11.80	1.50	86.0	11.47	Ross 555
484	NN 3442		07 26 00	-18 42.0	k-m	13.65		86.0	13.32	LTT 2844 L 744-10 LP 782-2
485	GI 540.2		14 10 26	-11 47.2	dM5.5e	13.86	1.53	86.0	13.53	LTT 5568 Ross 845
486	NN 3873		14 52 26	+35 45.8	M3.5	12.31		86.0	11.98	LTT 14424 Ross 1041
487	GJ 1234		19 17 15	+38 38.0	DC7	14.57	0.44	85.6	14.23	
488	GI 169		04 26 02	+21 48.7	K7 V	8.27	1.35	85.4	7.93	
489	GI 806		20 43 18	+44 18.7	dM3	10.77	1.53	85.4	10.43	AC+44:871-589
490	GI 146		03 33 26	-48 35.3	K7 V	8.60	1.31	85.3	8.25	
491	GI 660	A	17 09 18	-01 47.3	M3.5 J	12.05	1.60	85.3	11.70	L 989-020 V (AB) = 11.35 d(m) = 0.1

492	Gl 660	B	17 09 18	-01 47.3		12.20		85.3	11.90	a = 0.69" P = 33.5 yr Heintz AJ 101, 1071
493	Gl 528	A	13 46 47	+27 13.7	K4 V	7.61	1.12	85.1	7.26	ADS 9031 v (AB) = 7.04 d (m) = 0.42
494	Gl 528	B	13 46 47	+27 13.7	dK6	8.03		85.1	7.68	a = 2.433" P = 155.75 yr Heintz AJ 94, 1077 (1987)
495	Gl 575	A	15 02 08	+47 50.9	F9 V n	5.19	0.65	85.1	4.84	44 I Boo ADS 9494 V (AB) = 4.76 d (m) = 0.77
496	Gl 575	B	15 02 08	+47 50.9	dG2	5.96		85.1	5.61	a = 3.772" P = 225 yr
497	Gl 585		15 21 35	+17 39.6	M4	13.68	1.78	85.1	13.33	Ross 508
498	NN 3325		05 01 07	-17 26.2	M3	11.69	1.63	85.0	11.30	LTT 2153 L 736-49 LP 776-46
499	Gl 668.1		17 17 19	-05 51.9	G9 V	6.32	0.85	85.0	5.97	
500	NN 4070		18 40 07	+31 46.8	M3	11.27		85.0	10.92	LTT 15513 Ross 145
501	GJ 2020		00 59 24	-26 09.3	F0 V	9.75	0.33	84.9	9.40	
502	Gl 127.1	A	03 10 04	-68 47.2	DA3	11.40	0.05	84.9	11.04	LB 3303
503	Gl 127.1	B	03 10 04	-68 47.2		14.73	0.62	84.9	14.37	sep 8"
504	Gl 369		09 48 40	-12 04.5	dM2	10.04	1.48	84.8	9.68	LFT 685
505	NN 3266		04 07 34	+64 36.6	m	13.71	1.69	84.5	13.34	
506	GJ 1055		03 06 17	+09 50.5	m	14.85	1.72	84.2	14.48	
507	Gl 603		15 54 08	+15 49.4	F6 V	3.85	0.48	84.1	3.47	GAM Ser
508	NN 3472		07 56 48	-36 52.9	K0/1 V	7.00	0.98	84.0	6.62	LTT 3018
509	Gl 505	A	13 14 22	+17 17.0	K1 V	6.59	0.94	84.0	6.21	ADS 8841 V (AB) = 6.52 d (m) = 3.03

510	GI 505	wissenschaft in die schulen B	13 14 22	+17 17.0	M1 V	9.60		84.0	9.20	sep 1.3" 122d - 6.4" 108d (1881- 1959)
511	NN 3954		16 23 56	-17 16.5	m	14.30		84.0	13.90	LP 805-10
512	NN 4106		19 15 48	-53 48.0	M2	10.82	1.58	84.0	10.44	Sm 36 BPM 26134
513	Wo 9780		22 21 59	-48 06.8	M3.5	12.51		84.0	12.13	LTT 9012 LFT 1714
514	GI 598		15 44 01	+07 30.5	G0 V	4.43	0.60	83.9	4.05	LAM Ser
515	GJ 1243		19 49 37	+46 21.0	m	12.83	1.64	83.9	12.45	
516	GI 180		04 51 35	-17 50.7	M3 :	10.90	1.54	83.8	10.52	L 736-030
517	GI 512	A	13 25 46	-02 05.6	dM4	11.32	1.52	83.8	10.94	Ross 486
518	GI 512	B	13 25 46	-02 05.6	M4	13.69	1.68	83.8	13.31	sep 9" 59d (NLTT)
519	GI 79		01 50 25	-22 40.9	K5/M0 V	8.90	1.41	83.7	8.51	
520	GI 403		10 49 30	+14 15.7	dM3	12.67	1.65	83.7	12.28	
521	GJ 1223		18 01 03	+37 31.8	m	14.85	1.77	83.5	14.46	
522	GJ 1179	A	13 45 58	+23 51.6	dM4 :	15.32	1.96	83.4	14.93	
523	GJ 1179	B	13 45 48	+23 49.6	DC9	15.65	1.10	83.4	15.26	
524	GJ 1140		10 55 07	-07 15.4	DA6	14.31	0.32	83.3	13.91	
525	GI 676	A	17 26 15	-51 35.7	M0	9.58	1.46	83.3	9.18	
526	GI 676	B	17 26 20	-51 35.6	m	13.31	1.51	83.3	12.91	
527	GI 488		12 48 10	-00 29.4	M0.5Ve	8.49	1.40	83.1	8.09	
528	GI 97		02 20 15	-24 02.6	G1 V	5.20	0.60	83.0	4.80	KAP For
529	NN 3331	A	05 04 42	-21 39.0	M2	10.29	1.52	83.0	9.89	Steph 546
530	NN 3332	BC	05 04 41	-21 39.0	M3:	11.66	1.51	83.0	11.26	Steph 545 sep (AB) 8.3" 319d, sep (BC) 1.3" 30d V(BC) = 11.30 d(m) = 1
531	GI 277	A	07 28 40	+36 19.8	dM3.5e	10.58	1.47	83.0	10.18	VV Lyn
532	GI 277	B	07 28 39	+36 20.4	dM4.5e	11.78	1.52	83.0	11.38	Ross 989

533	GJ 2092	wissenschaft in die schulen	12 23 48	-65 56.0	DA/F	13.97	0.40	83.0	13.57	L 104-2 BPM 7543
534	NN 3727	A	12 26 19	-10 23.3	M2	10.96	1.51	83.0	10.56	LTT 4730 Ross 948
535	NN 3728	B	12 26 18	-10 23.3	g	11.00		83.0	11.00	LP 735-11 sep 4" 222d
536	Wo 9492		14 41 28	+66 16.1	M3	10.83	1.55	83.0	10.43	LTT 14363
537	Gl 851.3		22 11 56	-16 03.7	G8 V	6.54	0.90	83.0	6.14	LTT 8921
538	GJ 1053		03 05 16	+73 35.8	sdM6	14.64	1.79	82.9	14.23	
539	Gl 521		13 37 20	+46 26.0	dM2	10.23	1.42	82.9	9.82	
540	Gl 211		05 37 17	+53 27.8	K1 Ve	6.23	0.84	82.7	5.82	
541	Gl 851		22 09 05	+18 10.6	dM2 e	10.22	1.50	82.5	9.80	AC+17:536- 125 Ross 271 LFT 1691
542	Gl 145		03 31 17	-44 52.3	M3.5	11.48	1.57	82.4	11.06	
543	Gl 853	A	22 15 00	-53 52.1	G1 V	5.39	0.60	82.4	4.97	BS 8501 V (AB) = 5.37 d (m) = 4.5
544	Gl 853	B	22 15 00	-53 52.1		9.90		82.4	9.50	sep 2.3" 16d - 3.4" 32d (1900-1959)
545	Gl 309		08 30 54	-31 20.4	K0 V	6.39	0.78	82.3	5.97	
546	Gl 359		09 38 11	+22 15.5	M4	14.23	1.78	82.2	13.80	Ross 92
547	Gl 452	A	11 50 43	-07 05.3	M3	11.87	1.54	82.2	11.44	L 901-010
548	Gl 452	B	11 50 44	-07 05.4	f	19.40		82.2	19.00	LP 673-42b
549	Gl 601	A	15 50 43	-63 16.7	F2 IV	2.84	0.29	82.1	2.41	BET Tra cpm with LTT 6333 = L 153-157 ?
550	Gl 55		01 12 56	-45 47.9	F8 V	4.96	0.58	82.0	4.53	NU Phe
551	NN 3435		07 13 20	+58 29.8	DA4	12.00		82.0	11.60	GD 294
552	NN 3518		08 53 10	-23 40.8	m	14.00		82.0	13.60	LP 844-28
553	NN 3533		09 04 49	-21 56.4	k-m	14.30		82.0	13.90	LP 845-23
554	Gl 364		09 39 59	-23 41.4	F9 IV	4.93	0.53	82.0	4.50	

555	NN 3647	S	wissenschaft in die schulen	11 09 09	+33 48.4	dM4	12.38		82.0	11.95	
556	G1 443			11 44 08	-13 43.6	M3	11.69	1.48	82.0	11.26	L 829-026
557	NN 3800			13 39 30	-15 45.2	m	13.50		82.0	13.10	LP 798-25
558	G1 798			20 38 37	-52 51.8	K7 V	8.82	1.31	82.0	8.39	CD-53:8617 Sm 63
559	G1 680			17 31 24	-48 39.3	M0	10.15	1.56	81.9	9.72	
560	GJ 1288			23 40 23	+30 32.9	m	14.36	1.77	81.9	13.93	
561	GJ 1263			21 44 04	-00 24.0	M3.5	12.65	1.61	81.8	12.21	Wolf 940
562	G1 269	A		07 16 03	-46 53.7	K1 V	7.15	0.99	81.6	6.71	V(AB) = 6.69 d(m) = 0.70
563	G1 269	B		07 16 03	-46 53.7	K4 V	7.90		81.6	7.50	a = 0.609" P = 84.0 yr
564	G1 420	A		11 11 57	+73 44.8	dK5	7.68	1.06	81.6	7.24	
565	G1 420	B		11 11 57	+73 44.8	M2	11.40		81.6	11.00	ADS 8100C sep 7" 305d d (m) = 3.4 V (AC) = 7.63
566	G1 590			15 33 21	-37 43.4	M4	12.80	1.60	81.6	12.40	L 480-069
567	G1 400	A		10 42 30	+38 46.4	dM2	9.30	1.41	81.5	8.86	ADS 7915 V (AB) = 9.23 d (m) = 2.9
568	G1 400	B		10 42 30	+38 46.4		12.20		81.5	11.80	sep 1.2" 326d - 0.7" 290d (1896- 1965)
569	G1 32	A		00 43 25	-42 10.9	K5 V	8.41	1.17	81.4	7.96	
570	G1 32	B		00 43 25	-42 10.9	K7 V	9.06	1.27	81.4	8.61	
571	G1 64			01 35 26	-05 14.7	DA7	12.84	0.35	81.4	12.39	L 870-002
572	GJ 1206			16 47 38	+59 08.8	DAV4	12.23	0.18	81.2	11.78	LP 101-148
573	NN 3052			00 41 42	+08 51.2	m	13.80		81.0	13.30	LTT 10257
574	G1 118			02 51 14	-63 53.5	m	11.38	1.56	81.0	10.92	L 127-097
575	NN 3263			04 05 13	-24 36.6	M3.5	12.40		81.0	11.90	LP 833-42

576	NN 3285	S	wissenschaft in die schulen	04 23 07	+12 05.2	DC8	15.50		81.0	15.00	LP 475-70 LB 1320
577	NN 3333			05 04 54	+17 55.3	k	11.78	1.66	81.0	11.32	LTT 11586 Wolf 230
578	GJ 1075			05 04 56	-57 37.3	K7 V	9.02	1.40	81.0	8.56	BPM 18005 CP-57:737
579	NN 3567			09 44 30	+60 29.5	M2	12.73	1.64	81.0	12.30	LTT 12597 L 1820-21 LP 91-105
580	GJ 480.1			12 38 08	-43 18.4	M3.5	12.24	1.73	81.0	11.80	L 399-068
581	GJ 549	A		14 23 30	+52 04.9	F7 V	4.06	0.50	81.0	3.60	THE Boo
582	GJ 549	B		14 23 29	+52 03.7	M3	11.50	1.50	81.0	11.04	
583	NN 4004			17 20 40	-80 08.1	m	12.10		81.0	11.60	LTT 6920 L 21-3
584	GJ 688			17 36 48	+03 35.0	K3 V	6.52	0.96	81.0	6.06	
585	NN 4098			19 06 37	+32 12.1	m	11.80		81.0	11.34	LTT 15607 L 1499-34 LP 336-4
586	NN 4201			21 30 06	+24 20.4	m	12.66		81.0	12.20	LP 397-34
587	NN 4350			23 34 08	-36 45.5	M4	13.72	1.62	81.0	13.26	LFT 1809 LTT 9624 L 504-27 LP 986-92
588	GJ 835			21 35 45	+27 29.9	M0 e	9.88	1.50	80.8	9.42	
589	NN 3356			05 32 02	+13 51.1	M3.5	11.81	1.59	80.7	11.34	LTT 11684 Ross 46
590	GJ 95			02 16 44	-26 10.9	G5 V	6.34	0.73	80.5	5.87	
591	GJ 361			09 38 30	+13 26.4	dM2 e	10.37	1.50	80.3	9.89	AC+13:1301- 119 Ross 85 LFT 670
592	GJ 816			20 59 20	-06 30.6	M2.5	11.23	1.49	80.3	10.75	LTT 8338 Wolf 906 opt. comp. sep 6.5" 313.5d
593	GJ 480			12 36 25	+11 58.4	dM4	11.52	1.48	80.2	11.04	Wolf 433
594	GJ 1101			07 44 56	+83 31.3	m	13.09	1.68	80.1	12.61	
595	GJ 611	A		16 03 13	+39 17.4	G8 V	6.66	0.73	80.1	6.18	

596	GI 843	wissenschaft in die schulen	21 59 12	-19 43.5	M3	12.03	1.59	80.1	11.55	L 715-089
597	GJ 1068		04 09 17	-53 42.0	pec	13.58	1.93	80.0	13.10	
598	NN 3466	AB	07 52 52	-29 12.6	M4	13.38		80.0	12.90	LTT 2982 L 601-78 LP 898-1 V(AB) = 12.85 d(m) = 0.5 ; sep 0.8" 290d
599	NN 3487		08 11 48	+10 20.5	G5	7.32		80.0	6.84	
600	NN 3543		09 14 05	-18 25.0	M2	10.75	1.55	80.0	10.27	LTT 3412 L 749-34 LP 787-52
601	NN 3028		00 17 48	+32 49.3	M6	16.05	1.98	79.9	15.56	LP 292-67 RV G&L ApJ 305, 784
602	NN 3497		08 21 00	+69 13.0	dM5.2	15.67	2.09	79.9	15.18	LP 35-347 USNO 710
603	GI 390		10 22 44	-09 58.6	M1.5	10.17	1.49	79.9	9.68	
604	GI 507	A	13 17 14	+35 23.0	dM1.5	9.51	1.47	79.9	9.02	
605	GI 507	B	13 17 14	+35 23.0	M3	12.10	1.58	79.9	11.61	
606	GI 848		22 04 41	+25 06.0	F5 V	3.76	0.44	79.9	3.27	IOT Peg
607	GI 435		11 38 37	-44 07.9	K5 Ve	7.77	1.06	79.8	7.28	
608	NN 3250		03 44 37	+08 33.1	k-m	14.51	1.87	79.7	14.02	LTT 11262
609	GI 200	A	05 16 40	-03 07.6	K3 V	7.70	1.04	79.7	7.21	ADS 3900 V (AB) = 7.67 d (m) = 4.
610	GI 200	B	05 16 40	-03 07.6	M2	11.70		79.7	11.20	sep 4.9" 46d - 2.7" 29d (1900-60)
611	GJ 1029		01 02 47	+28 13.6	m	14.80	1.89	79.6	14.30	
612	GI 525		13 42 39	+18 03.7	dM1	9.80	1.41	79.6	9.30	Wolf 497 optical comp. 20" d(m) = 1. (Worley)
613	GI 791		20 24 40	-27 54.1	M3	11.41	1.52	79.6	10.91	

614	GI 836.5		21 40 22	+20 46.7	DQ6	13.24	0.17	79.6	12.74	LTT 16348 LFT 1655 LP 458-64 L 1363-003
615	GI 914	A	23 59 33	+26 49.0	G3 V	5.81	0.67	79.6	5.31	BS 9088 ADS 17175 V(AB) = 5.75 d(m) = 3.20
616	GI 914	B	23 59 33	+26 49.0	K6 V	9.00		79.6	8.50	a = 0.83" P = 26.27 yr
617	GI 26		00 36 13	+30 20.5	dM4	11.06	1.53	79.5	10.56	AC+31:719
618	GI 462		12 19 25	+42 25.1	M0 Ve	9.45	1.36	79.5	8.95	LFT 898
619	GI 107	A	02 40 46	+49 01.1	F7 V	4.13	0.49	79.3	3.63	THE Per
620	GI 107	B	02 40 46	+49 01.1	M1 V	10.06	1.48	79.3	9.56	
621	GI 302		08 16 01	-12 27.7	G7.5 V	5.97	0.76	79.3	5.47	
622	NN 3112		01 41 36	-67 32.2	DA7	13.88	0.44	79.0	13.37	LFT 158 LTT 934 L 88-59
623	NN 3292		04 26 28	+14 07.2	m	13.50		79.0	13.00	LTT 11438
624	GI 194	A	05 12 59	+45 57.0	G5 III	0.71	0.80	79.0	0.20	ALF Aur BS 1708 ADS 3841 V(AB) = 0.08 d(m) = 0.15 source?
625	GI 194	B	05 12 59	+45 57.0	G0 III	0.96		79.0	0.45	
626	NN 3357		05 33 30	-07 41.0	M4	12.80	1.63	79.0	12.30	LTT 2321 L 882-76 Wolf 1457
627	GI 261		06 59 27	-06 22.1	DA	15.27	0.88	79.0	14.80	L 886-6
628	NN 3459		07 36 29	-21 06.1	m	11.70		79.0	11.20	LTT 2906 L 672-19 LP 783-1
629	NN 3722		12 21 13	+67 28.0	m	11.25		79.0	10.74	LTT 17123
630	NN 3780		13 20 55	-25 38.9	m	12.90		79.0	12.39	LTT 5161 L 617-35 LP 855-10

631	NN 3916		15 44 42	-10 44.3	M2	11.25		79.0	10.74	LTT 6305 L 841-9 LP 743-31
632	NN 4062		18 30 22	+40 38.5	m	11.99		79.0	11.48	
633	GJ 2147		20 07 51	-30 21.9	DA4	12.18	0.07	79.0	11.67	LTT 7987 L 565-18
634	NN 4154		20 38 07	-81 53.8	m	11.50		79.0	11.00	LTT 8178 L 23-30
635	Gl 177		04 45 21	-17 01.5	G1 V	5.49	0.63	78.9	4.98	
636	Gl 448		11 46 31	+14 51.1	A3 V	2.14	0.09	78.9	1.63	BET Leo
637	GJ 1248		20 01 24	+05 51.9	k-m	12.09	1.60	78.9	11.58	
638	Gl 810	A	20 52 48	-14 13.2	M3.5 J	12.45	1.59	78.9	11.94	L 856-054
639	Gl 810	B	20 52 47	-14 15.0		14.55	1.72	78.9	14.04	
640	Gl 477		12 33 15	-45 39.2	M1	11.10	1.48	78.8	10.58	
641	GJ 1215		17 15 25	+11 43.7	m	15.10	1.88	78.8	14.58	
642	Gl 82		01 55 54	+58 16.9	dM4 e	12.21	1.56	78.5	11.68	Ross 15 AC +58:13565
643	Gl 454		11 58 10	-10 09.7	K0 IV	5.55	0.77	78.2	5.02	
644	GJ 2045		05 39 46	-05 30.1	m	15.28	1.86	78.1	14.74	LP 658-44
645	NN 4054		18 20 45	+60 59.9	DC:9	15.65	0.97	78.1	15.11	LP 103-294
646	NN 3130		02 00 49	+35 21.1	G5	8.36		78.0	7.82	
647	Gl 113.1		02 45 42	+30 54.6	G9 e	6.76	0.96	78.0	6.22	VY Ari SBO (A&A 195,129)
648	Gl 395		10 27 26	+56 14.3	F8 V	4.84	0.52	78.0	4.30	
649	NN 3668		11 28 35	-14 39.6	m	14.29	1.81	78.0	13.75	LP 732-35
650	Gl 469		12 26 27	+08 42.4	M3.5	12.06	1.60	78.0	11.52	Wolf 414
651	NN 3892		15 07 07	+03 21.0	M3	11.46	1.50	78.0	10.90	LTT 14507 Ross 1047
652	Gl 620.1	A	16 20 38	-39 04.7	G3/5 V	5.39	0.63	78.0	4.85	
653	Gl 620.1	B	16 20 10	-39 06.8	DA2	11.00	-0.14	78.0	10.46	
654	GJ 1210		17 05 17	+07 26.3	m	14.01	1.88	78.0	13.47	
655	GJ 1218		17 23 33	-62 24.1	m	12.68	1.48	78.0	12.14	

656	NN 4326	S	23 14 58	+19 20.5	M4	12.10	1.59	78.0	11.60	LTT 16843 L 1295-9 LP 462-19
657	NN 4387		23 57 14	-34 22.9	M4	12.80		78.0	12.30	LFT 1844 LTT 9829 L 577-87 LP 936-49
658	Gl 891		23 07 32	-26 12.2	M2.5	11.27	1.52	77.7	10.70	
659	Gl 897	A	23 30 09	-17 01.5	M3.5 J	10.95	1.51	77.5	10.40	V(AB) = 10.42 d(m) = 0.5 , triple with Gl 898 sep 336" 353d
660	Gl 897	B	23 30 09	-17 01.5		11.40		77.5	10.80	sep 0.5" 358d - 0.2" 345d (1934- 1962)
661	Gl 898		23 30 12	-17 07.1	K5/M0 V	8.60	1.28	77.5	8.05	SpT: dK5e Wilson
662	GJ 1073		04 49 02	+40 38.3	k	13.43	1.61	77.4	12.87	
663	GJ 1214		17 12 49	+05 01.7	m	14.67	1.74	77.4	14.11	
664	Gl 671		17 18 17	+41 46.5	M3	11.37	1.56	77.4	10.81	AC+41:726- 154
665	Gl 401	A	10 43 19	-18 50.5	M1	11.03	1.44	77.3	10.47	
666	Gl 401	B	10 43 19	-18 50.5	DQ9	16.50		77.3	15.90	
667	Gl 842		21 55 56	-59 59.4	M2	9.75	1.49	77.2	9.19	L 165-2 CD- 60:7821 Sm 96
668	Gl 529		13 47 05	-21 51.4	K6 V	8.17	1.26	77.1	7.61	
669	NN 3131		02 01 01	-21 27.8	M3	11.21	1.46	77.0	10.60	LTT 1081
670	GJ 1049		02 37 36	-58 24.1	M0 Ve	9.65	1.39	77.0	9.08	
671	NN 3224		03 23 04	+05 41.5	m+	14.70		77.0	14.13	LP 532-81 V- R = 1.71 Weis
672	NN 3309		04 41 19	+27 46.5	M2.5	11.26	1.53	77.0	10.70	LTT 11502
673	NN 3981		16 56 09	+14 02.6	m	13.13		77.0	12.56	

674	GI 805		20 43 08	-25 27.1	F5 V	4.13	0.43	77.0	3.56	PSI Cap
675	NN 4368		23 48 01	+09 40.0	M1	11.50	1.45	77.0	10.93	LTT 17025
676	GJ 1077		05 19 38	-78 19.6	M1.5 V	11.91	1.48	76.8	11.34	
677	NN 3106		01 37 39	+63 33.6	B5	10.07	0.47	76.7	9.50	
678	GI 125		03 06 09	+45 32.9	dM1	10.15	1.49	76.7	9.57	AC+45:133-65
679	GI 179		04 49 24	+06 23.8	dM4 e	11.98	1.56	76.7	11.40	Wolf 1539
680	GI 422		11 14 03	-57 17.5	m	11.65	1.47	76.7	11.07	L 192-072
681	GI 833		21 33 17	-51 04.1	K2 V	7.14	0.88	76.6	6.56	
682	GI 324	A	08 49 37	+28 31.4	G8 V	5.95	0.86	76.4	5.37	
683	GI 324	B	08 49 42	+28 30.5	M3.5	13.14	1.64	76.4	12.56	
684	GI 592		15 34 13	-13 57.5	M4	12.70	1.58	76.4	12.12	Ross 802
685	GI 195	A	05 13 42	+45 47.5	dM2	10.20	1.50	76.3	9.61	AC+45:217-363 V(AB) = 10.16 d(m) = 3.5
686	GI 195	B	05 13 42	+45 47.5	M4 :	13.70		76.3	13.10	sep 1.8" 117d - 3.0" 143d (1935-58)
687	GI 472		12 30 39	-68 28.5	K0 V	7.13	0.85	76.3	6.54	
688	GI 500		13 07 00	-21 55.3	G6 V	7.36	0.73	76.3	6.77	
689	NN 3506		08 31 12	+68 14.9	M3	11.67	1.57	76.2	11.08	LFT 592 LTT 12230 L 1866-6
690	GI 813		20 55 09	+22 10.4	M3	12.01	1.61	76.2	11.42	AC+22:308-605 Wolf 1373 LFT 1588
691	GI 807		20 44 16	+61 38.6	K0 IVe	3.43	0.92	76.1	2.84	ETA Cep
692	NN 3036		00 26 09	+50 05.9	m	13.15		76.0	12.55	
693	GI 41		00 50 04	+60 51.0	F8 V	4.82	0.53	76.0	4.22	
694	GJ 1031		01 05 52	-29 04.3	dM5	13.42	1.70	76.0	12.82	
695	NN 3371	A	05 55 14	+58 35.6	M1	10.25	1.51	76.0	9.65	

696	NN 3372	S	wissenschaft in die schulen	05 55 32	+58 34.3	m	13.56		76.0	12.96	sep 161" 119d
697	GJ 2049			06 19 50	-22 42.1	M1.5	10.76	1.44	76.0	10.16	LTT 2531
698	NN 3564			09 41 05	+27 12.1	M3	12.05	1.56	76.0	11.50	LTT 12583 Ross 93
699	NN 3704			12 03 03	+69 49.1	M4	13.07		76.0	12.47	LFT 880 LTT 13356 Ross 689 LHS.
700	GJ 1180			13 49 42	+26 53.0		10.83	0.75	76.0	10.23	
701	NN 3817			13 55 49	+12 48.7	M3	12.26	1.66	76.0	11.70	LTT 14082 Ross 837
702	NN 4044			18 11 05	+26 01.0	m	13.32		76.0	12.72	LP 390-16
703	GJ 1092			06 45 41	+37 11.7	m	13.76	1.66	75.8	13.16	
704	GJ 675			17 25 09	+67 20.9	K0 V	6.43	0.76	75.7	5.83	
705	GJ 167			04 14 39	-53 26.3	K5 V	7.64	1.13	75.6	7.03	
706	NN 3612			10 32 04	+69 43.0	k-m	11.93	1.55	75.6	11.32	LTT 12827 LFT 723 L 1912-9 LP 37-179
707	GJ 164			04 09 09	+52 29.7	M3.5	13.50	1.67	75.3	12.88	Ross 28
708	GJ 368			09 45 22	+46 15.3	G0.5 Va	5.09	0.62	75.3	4.47	
709	GJ 613			16 05 41	-56 19.1	K3 V	7.11	0.85	75.3	6.49	
710	NN 3001			00 00 06	-34 29.7	DC9	14.90	0.46	75.2	14.28	LTT 3
711	GJ 597			15 42 15	+76 09.6	M3	12.22	1.65	75.2	11.60	AC+76:5308
712	NN 3971			16 40 22	+67 41.5	m	15.65	1.95	75.2	15.03	LP 069-457
713	GJ 732	A		18 50 15	-38 39.8	sdG0	12.70	1.53	75.2	12.08	L 489-58
714	GJ 732	B		18 50 15	-38 39.8		16.00		75.2	15.00	sep 12" (LHS, but not in NLTT)
715	GJ 862			22 26 25	-30 15.8	K5 V	7.65	1.10	75.2	7.03	
716	GJ 69			01 40 12	+63 34.8	K5 V	8.41	1.22	75.1	7.79	
717	GJ 458	A		12 09 50	+54 45.7	dM1.5	9.79	1.43	75.1	9.17	

718	GI 458	wissenschaft in die schulen	12 09 51	+54 45.9	m	13.33	1.61	75.1	12.71	sep 15" in 7d (NLTT)
719	NN 3244		03 38 15	-02 29.4	K0	6.96	0.96	75.0	6.34	LTT 1736
720	GJ 1088		06 09 25	-43 24.5	M3.5	12.32	1.59	75.0	11.70	
721	NN 3423		07 00 05	+34 46.2	m	13.17		75.0	12.55	LP 255-11
722	NN 3586		10 06 19	+51 32.4	k-m	13.47	1.66	75.0	12.85	LP 127-132
723	GJ 1135		10 38 52	-36 37.9	M0 V	9.97	1.48	75.0	9.35	LTT 3919 L 465-43
724	NN 3679		11 36 29	-24 26.4	G6/8 V	6.41	0.82	75.0	5.79	BS 4489 LTT 4310
725	NN 3900		15 16 29	-12 34.1	M3	12.58	1.52	75.0	12.00	LTT 6104 L 839-21 LP 742-61
726	NN 4239		21 54 16	-02 08.9	dM5	14.64	1.76	75.0	14.02	LP 639-1
727	GJ 1267		22 19 04	-54 49.0	M0 V	9.06	1.35	75.0	8.44	LTT 8985 BPM 27793
728	GJ 1012		00 26 08	-06 55.8	M4	12.19	1.48	74.8	11.56	
729	GI 731		18 49 38	+16 31.8	dM1.5	10.15	1.47	74.8	9.52	AC+16:247- 80
730	GI 742		19 00 39	+70 35.1	DXP5	13.20	0.05	74.8	12.57	LFT 1446 AC +70:8247
731	GI 126		03 09 33	-46 42.7	m	11.52	1.44	74.6	10.88	LTT 1509 CFS 873
732	GI 774	A	19 59 20	-65 43.7	m	11.35	1.48	74.6	10.71	L 115-021 Sm 48
733	GI 774	B	19 59 20	-65 43.7	m	12.82	1.56	74.6	12.18	sep 16" 284d (LHS)
734	GI 282	A	07 37 29	-03 28.7	K2 Ve	7.20	0.96	74.3	6.55	
735	GI 282	B	07 37 33	-03 29.0	K5	8.94	1.33	74.3	8.29	
736	GI 572		14 59 09	+45 37.1	dM0	9.13	1.43	74.3	8.48	
737	GI 771	A	19 52 51	+06 16.8	G8 IV	3.72	0.86	74.3	3.07	BET Aql
738	GI 771	B	19 52 51	+06 16.8	M3	11.40		74.3	10.80	
739	GI 427		11 21 39	+21 38.1	DA7	14.24	0.28	74.2	13.59	Ross 627
740	GI 504		13 14 18	+09 41.1	G0 V	5.20	0.58	74.2	4.55	

741	Gl 360		09 38 22	+70 15.9	M3	10.57	1.50	74.1	9.92	AC+70:4336
742	Gl 767	A	19 44 26	+31 53.9	M0.5	10.15	1.48	74.1	9.50	
743	Gl 767	B	19 44 26	+31 53.9	M2 :	11.10	1.52	74.1	10.45	
744	NN 3009		00 05 54	-57 22.0	M4	12.07	1.54	74.0	11.42	LTT 57 BPM 16015 L 217- 28 Sm 154 R- I = 1.44 Weistrop
745	Gl 259		06 59 11	-25 52.6	K0 Ve	6.71	0.89	74.0	6.06	
746	Gl 334		09 04 20	-08 36.5	dM0	9.51	1.42	74.0	8.86	
747	NN 3708	A	12 08 38	-19 40.8	M2:	11.68	1.59	74.0	11.03	LTT 4562 L 758-108 LP 794-30
748	NN 3709	B	12 08 43	-19 41.5	m	12.62	1.68	74.0	11.97	LP 794-31 sep 85" 121d
749	Gl 527	A	13 44 53	+17 42.3	F7 V	4.50	0.48	74.0	3.85	TAU Boo
750	Gl 527	B	13 44 53	+17 42.3	M2	11.00		74.0	10.30	
751	Gl 133		03 13 56	+79 46.9	M2	11.20	1.56	73.8	10.54	AC+79:1584
752	Gl 672		17 18 47	+32 31.9	G2 V	5.39	0.62	73.7	4.73	
753	NN 4006		17 23 39	+01 50.9		10.90	0.67	73.7	10.20	VVO 251 AC +02:2142- 173
754	Gl 763		19 32 09	+04 28.1	dM0.5	9.36	1.39	73.7	8.70	
755	Gl 599	A	15 44 14	-37 45.6	G6 V	6.01	0.72	73.5	5.34	
756	Gl 599	B	15 44 14	-37 45.6	DA7	12.78	0.33	73.5	12.11	
757	Gl 225		05 54 08	-14 10.5	F1 III	3.72	0.33	73.4	3.05	ETA Lep
758	Gl 377		09 59 01	-30 09.5	M3	11.43	1.49	73.3	10.76	
759	GJ 1194	A	15 38 16	+43 39.5	m	12.48	1.57	73.3	11.81	V(AB) = 12.20 d(m) = 1.35:
760	GJ 1194	B	15 38 17	+43 39.4	m	13.80		73.3	13.10	sep 5" 146d (LHS)
761	GJ 1035		01 14 18	+83 53.3	m	14.77	1.79	73.2	14.09	
762	Gl 93		02 15 50	-54 13.5	m	11.43	1.41	73.2	10.75	
763	Gl 414	A	11 08 20	+30 43.2	K8 V	8.33	1.34	73.2	7.65	
764	Gl 414	B	11 08 18	+30 43.2	M2 V	9.98	1.52	73.2	9.30	

765	Gl 67	A	01 38 44	+42 21.8	G1.5 V	4.95	0.62	73.1	4.27	
766	Gl 737	A	18 53 21	-56 03.1	K7 V	9.45	1.42	73.1	8.77	Sm 24 V (AB) = 8.96 d (m) = 0.55
767	Gl 737	B	18 53 21	-56 03.1	K5 V	10.00		73.1	9.32	sep 5.0" 295d - 3.6" 319d (1892- 1959)
768	Gl 111		02 42 46	-18 47.0	F6 V	4.46	0.48	73.0	3.78	TAU(1) Eri
769	Gl 112.1		02 43 34	+11 34.1	dK8	8.59	1.28	73.0	7.91	
770	NN 3326		05 01 29	+10 59.1	m	13.75		73.0	13.07	LTT 17736
771	Gl 189		05 04 39	-57 32.4	F7 V	4.71	0.52	73.0	4.03	BS 1674 ZET Dor
772	Gl 398		10 33 28	+05 22.7	dM4 e	12.60	1.60	73.0	11.92	L 1113-055
773	Gl 646	A	16 55 26	-39 29.2	K5 V	8.50	1.16	73.0	7.82	V(AB) = 8.31 d(m) = 1.9
774	Gl 646	B	16 55 26	-39 29.2		10.40		73.0	9.70	sep 3.9" 9d (1931)
775	Gl 788		20 17 02	+66 41.6	G5 V	5.93	0.58	72.9	5.24	
776	NN 3520		08 54 39	+73 09.4	m	14.32	1.70	72.8	13.63	LP 36-98 USNO 713
777	Gl 333		08 57 52	-47 15.0	M3	12.19	1.56	72.8	11.50	L 316-062
778	Gl 127	A	03 09 57	-29 11.0	F7 IV	3.95	0.51	72.7	3.26	ALF For BS 963 ADS 2402 V(AB) = 3.86 d(m) = 2.75
779	Gl 127	B	03 09 57	-29 11.0	G7 V	6.70		72.7	6.00	a = 4.367" P = 314 yr
780	Gl 162		04 05 23	+33 30.2	M1	10.18	1.51	72.7	9.49	AC +33:10883 Ross 587
781	Gl 895.2		23 26 16	+04 58.5	DAV4	13.04	0.16	72.7	12.35	LTT 16907 ZZ Psc PG
782	Gl 750	A	19 13 03	-45 58.4	K9 V J	10.12	1.42	72.6	9.42	Sm 34 V (AB) = 9.37 d (m) = 0.0

783	GI 750	B	19 13 03	-45 58.4		10.10		72.6	9.40	sep 0.2" 348d - 0.2" 43d (1929- 1949)
784	NN 3779		13 20 36	+24 44.3	M3.5	12.93	1.62	72.5	12.23	LFT 999 LTT 13887 Ross 1020
785	GI 611	B	16 03 07	+39 17.6	m	14.23	1.72	72.5	13.53	
786	GI 760		19 22 59	+03 00.8	F0 IV	3.36	0.32	72.5	2.66	DEL Aql
787	GI 904		23 37 23	+05 21.3	F7 V	4.13	0.51	72.5	3.43	IOT Psc
788	GJ 1270		22 27 32	+41 13.1	m	13.25	1.65	72.3	12.55	
789	GI 311		08 34 47	+65 11.7	G1 V	5.64	0.62	72.2	4.93	PI(1) Uma
790	GI 521.1		13 37 33	-03 56.4	K7	9.59	1.40	72.2	8.88	
791	GI 524		13 41 36	-53 51.0	k	12.50	1.54	72.2	11.79	L 258-146
792	NN 4169		20 51 10	+10 26.0	m	13.97	1.73	72.2	13.26	USNO 764
793	GI 25	A	00 34 47	-25 02.5	G7 V	6.23	0.72	72.1	5.52	BS 159 ADS 520 LTT 328 V(AB) = 5.57 d(m) = 0.21, SB2
794	GI 25	B	00 34 47	-25 02.5	G8 V	6.40		72.1	5.70	sep 0.5"
795	GI 394		10 27 14	+56 15.4	K7 Ve	8.69	1.33	72.1	7.98	
796	GJ 1292		23 55 07	+23 02.4	k-m	11.72	1.54	72.1	11.01	
797	NN 3053		00 42 29	-15 32.3	m	14.20		72.0	13.50	
798	NN 3336		05 06 33	+48 47.1	M2	11.39	1.53	72.0	10.70	LTT 11590 L 1672-14 LP 158-9
799	NN 3898		15 10 57	+45 54.6	m	13.35		72.0	12.64	
800	NN 3972		16 44 00	+16 34.4	m	11.65		72.0	10.94	LTT 14970 L 1276-44 LP 446-6
801	NN 4055		18 21 31	+28 08.6	M3	12.49	1.61	72.0	11.80	LTT 15435 Ross 708
802	NN 4056		18 21 33	+01 39.6	g	11.84	1.56	72.0	11.10	LTT 15437 L 1064-69 LP 630-11

803	GJ 2138	wissenschaft in die schulen	18 35 54	-14 31.7	dM1	11.26	1.56	72.0	10.55	
804	NN 4279		22 24 32	+06 34.3	dM3 :	13.22	1.66	72.0	12.50	LTT 16577 L 1149-75 LP 580-17 Rob 320 V-I = 2.72 Robertson
805	NN 4340		23 30 08	-77 39.7	G2 V	5.81	0.68	72.0	5.10	BS 8935
806	Gl 407		10 56 40	+40 41.9	G0 V	5.05	0.61	71.9	4.33	
807	NN 3637		10 58 41	+03 16.8	m	14.07	1.73	71.9	13.35	LTT 12949
808	Gl 142		03 25 36	-19 58.9	K7 V	8.39	1.33	71.8	7.67	
809	GJ 1182		14 13 04	+04 54.0	m	14.30	1.72	71.8	13.58	
810	Gl 722		18 35 54	-21 05.7	G5 V	5.86	0.68	71.8	5.14	
811	Gl 838		21 45 01	-47 31.9	G2 V	5.58	0.60	71.8	4.86	
812	Gl 46		00 55 58	-28 07.3	M3.5	11.77	1.57	71.7	11.05	
813	Gl 703		18 05 04	+15 56.5	G6	8.68	0.65	71.7	7.96	
814	Gl 710		18 17 15	-01 57.7	dM1	9.66	1.37	71.7	8.94	
815	Gl 770		19 51 18	-24 04.0	K3/4 V	6.17	1.02	71.7	5.45	
816	Gl 836		21 36 06	-24 22.5	M3.5	13.43	1.56	71.7	12.71	L 714-088
817	Gl 215		05 41 05	+62 13.7	K7	9.02	1.40	71.6	8.29	
818	Gl 895		23 22 14	+57 35.0	dM2 e	10.04	1.50	71.6	9.31	
819	GJ 1072		04 47 49	+22 02.7	m	15.21	1.95	71.4	14.48	
820	Gl 331	A	08 55 48	+48 14.4	A7 IV	3.14	0.19	71.3	2.41	ADS 7114 IOT UMa
821	Gl 331	B	08 55 48	+48 14.4	dM1 J	10.80		71.3	10.10	AB: a = 9.092" P = 817.91 yr
822	Gl 331	C	08 55 48	+48 14.4		11.00		71.3	10.30	BC: a = 0.68" P = 39.69 yr
823	NN 4040		17 56 28	+46 35.2	m	11.79	1.56	71.3	11.06	
824	Gl 20		00 23 45	-43 57.4	A7 Vn	3.94	0.17	71.2	3.20	KAP Phe
825	Gl 174		04 38 22	+20 48.6	K3 V	8.00	1.10	71.2	7.26	
826	Gl 204		05 25 57	-03 31.7	K5 V	7.65	1.10	71.2	6.91	

827	G1 685	wissenschaft in die schulen!	17 35 02	+61 43.1	M1 Ve	9.97	1.47	71.1	9.23	AC +61:26806
828	G1 875		22 47 43	-07 21.4	dM1 e	9.85	1.48	71.1	9.11	
829	G1 14		00 14 26	+40 40.2	dM0.5	9.00	1.36	71.0	8.26	
830	NN 3060	A	00 47 52	+24 32.7	m	12.70		71.0	12.00	LTT 10301 LP 350-20 V (AB) = 12.09 d(m) = 0.3 , V-R = 1.50 Weis
831	NN 3061	B	00 47 52	+24 32.7	m	13.30		71.0	12.60	LP 350-19 sep 1" 315d d (R) = 0.3 d (pg) = 0.3 (NLTT)
832	G1 238		06 33 07	-58 29.9	m	11.62	1.51	71.0	10.88	L 182-044
833	NN 3452		07 31 12	+54 58.0	dM0	11.29	1.55	71.0	10.55	
834	NN 3489	A	08 14 19	-35 43.7	G8/K0 V	7.20	0.94	71.0	6.50	V, B-V from CPC
835	NN 3490	B	08 14 19	-35 43.7		11.00		71.0	10.30	
836	G1 510		13 23 04	-28 06.8	M2.5	11.02	1.53	71.0	10.30	
837	G1 533		13 51 02	+13 11.8	dM0	9.80	1.40	71.0	9.06	
838	GJ 1181	AB	13 52 12	-28 50.7	K7 V	9.59	1.45	71.0	8.85	LTT 5419 L 619-94 sep 1.2" 34d (1950), V (AB) = 9.57 d (m) = 4.3
839	NN 3861		14 35 24	+58 34.4	m	11.74		71.0	11.00	LP 98-132
840	NN 4038		17 54 49	+15 47.2	m	12.21		71.0	11.47	LTT 15306 L 1279-91 LP 449-6
841	G1 716		18 28 23	-18 56.5	K3 V	6.81	0.85	71.0	6.07	
842	G1 726		18 44 50	-03 41.5	K7	8.81	1.29	71.0	8.07	
843	NN 4287		22 35 16	+39 07.6	M2	9.41		71.0	8.67	LTT 16634

844	NN 4288	A	22 35 36	-29 36.4	m	10.92		71.0	10.18	LTT 9123 L 645-74 LP 932-12
845	NN 4289	B	22 35 37	-29 36.5	m	12.64		71.0	11.90	LTT 9124 L 645-73 LP 932-13 sep 15" 132d
846	GI 878		22 52 26	+60 43.7	M3	12.76	1.60	71.0	12.02	Ross 226
847	GI 206		05 29 30	+09 47.3	dM4 e	11.52	1.63	70.9	10.77	Ross 42
848	GJ 1220		17 36 50	+82 06.8	m	14.18	1.76	70.9	13.43	
849	GI 844		21 59 24	+16 13.4	M2 V	10.62	1.58	70.9	9.87	AC+16:734- 144
850	GI 899		23 31 33	-00 05.1	M4	11.17	1.45	70.9	10.42	Wolf 1039
851	NN 4073		18 41 45	+40 36.8	m	18.23		70.8	17.48	LP 229-30
852	GI 455.3		12 05 50	-24 27.0	F2 III-IV	4.02	0.32	70.7	3.27	ALF Crv
853	GI 130.1	A	03 12 17	+57 59.3	M1.5	10.92	1.54	70.6	10.16	AC +57:22428 Ross 370 LFT 265 V (AB) = 10.31 d(m) = 0.3
854	GI 130.1	B	03 12 17	+57 59.3	M2	11.20		70.6	10.40	AC +57:22429 LFT 266 sep 5" 10d (NLTT)
855	NN 3693		11 51 18	+07 17.3	M6 :	17.89	1.72	70.6	17.13	LP 553-59
856	GI 775		20 00 17	+03 11.0	K4 V	7.46	1.14	70.6	6.70	
857	GI 59	A	01 30 53	-24 25.9	G8 V	6.97	0.76	70.4	6.21	
858	GI 59	B	01 30 35	-24 29.7	m	12.77	1.30	70.4	12.01	L 654-050 LTT 840
859	GI 192		05 09 44	+19 36.2	M3.5:	10.76	1.54	70.4	10.00	AC+19:1165- 38
860	GI 277.1		07 29 57	+63 03.1	dM0	10.49	1.55	70.4	9.73	AC +63:14097
861	GI 348	A	09 26 37	-02 33.0	F6 V	4.60	0.45	70.4	3.84	
862	GI 348	B	09 26 37	-02 31.9	K0	7.18	0.87	70.4	6.42	

863	GI 383		10 09 47	-18 22.2	K7 V	9.94	1.48	70.4	9.18	
864	GI 5		00 04 01	+28 44.7	K0 Ve	6.14	0.75	70.2	5.37	
865	NN 3655		11 19 20	-12 56.6	M8	19.57		70.2	18.80	LP 732-94
866	GI 589	A	15 33 08	+17 52.9	M4.5:	12.41	1.58	70.2	11.64	AC+18:1890-112
867	GI 589	B	15 33 08	+17 52.9	M6	14.99	1.81	70.2	14.22	L 1272-021
868	NN 3211		03 11 47	+00 28.1		10.90		70.1	10.10	
869	GI 168.1		04 19 15	+19 21.9		15.04	1.00	70.1	14.30	LOWNE 1
870	GI 796		20 37 13	-23 57.5	G8 V	6.36	0.72	70.1	5.59	
871	GI 44		00 54 48	-02 05.0	K1	9.46	0.86	70.0	8.69	
872	NN 3136		02 05 38	+49 13.0	M5 :	12.47	1.54	70.0	11.70	
873	GI 90		02 11 35	+67 26.6	K2 V	7.09	0.90	70.0	6.32	
874	NN 3237		03 34 04	+03 19.7	dM5 :	13.86		70.0	13.09	LP. Rob 233
875	GI 281		07 36 48	+02 18.2	dM0	9.61	1.44	70.0	8.84	
876	NN 3467		07 55 29	+07 25.2	m	13.77		70.0	13.00	LTT 12102
877	NN 3729		12 26 37	+42 00.6	m	12.90		70.0	12.13	
878	NN 3943		16 07 56	-70 01.2	k-m	13.75		70.0	12.98	LTT 6453 L 74-208
879	NN 4060		18 29 24	-62 47.0	K7	9.52	1.45	70.0	8.75	Sm 15
880	NN 4205		21 33 05	+51 18.4	M3.5	11.78	1.46	70.0	11.00	LTT 16311 LFT 1644 Wolf 926
881	GI 855.1	A	22 20 22	-72 30.0	G0 V J	5.98	0.65	70.0	5.21	NU Ind BS 8515 V(AB) = 5.28 d(m) = 0.1
882	GI 855.1	B	22 20 22	-72 30.0		6.10		70.0	5.30	sep 0.1" (1928) not seen since 1933
883	GJ 1279		23 06 33	-68 00.1	K5 V	8.39	1.20	70.0	7.62	LTT 9379

884	Gl 292	wissenschaft in die schulen A	07 50 24	-34 34.7	F5 V	5.05	0.44	69.9	4.27	BS 3079 V (AB) = 5.01 d (m) = 3.55
885	Gl 292	B	07 50 24	-34 34.7	K3	8.60		69.9	7.80	sep 3.0" 274d (1959)
886	Gl 615		16 09 47	-57 25.5	K0 V	7.53	0.83	69.9	6.75	
887	Gl 156		03 52 09	-06 58.8	M0 V	9.02	1.36	69.8	8.24	
888	Gl 556		14 31 51	+53 07.4	K3 V	7.23	0.99	69.8	6.45	
889	Gl 652		17 01 19	-28 30.6	G8 IV-V	6.58	0.83	69.8	5.80	
890	Gl 240		06 35 55	-49 59.7	K0	9.62	1.46	69.7	8.84	
891	Gl 564		14 48 02	+24 07.0	G2 V	5.85	0.56	69.7	5.07	
892	Gl 253		06 53 51	-55 11.5	G7 V	8.17	0.78	69.6	7.38	
893	Gl 197		05 15 37	+40 03.4	G2 IV-V	4.71	0.63	69.5	3.92	LAM Aur
894	Gl 476		12 32 30	+10 06.5	M3	11.42	1.42	69.4	10.63	AC+10:95- 26
895	Gl 794		20 32 14	+24 54.0	DA3	11.52	-0.07	69.4	10.73	LTT 16005 LFT 1554 Wolf 1346 AC+24:747- 102
896	Gl 363		09 38 57	+56 13.2	M3.5	12.50	1.53	69.3	11.70	LTT 12565
897	Gl 8		00 06 30	+58 52.4	F2 III-IV	2.27	0.34	69.2	1.47	BET Cas
898	Gl 40	A	00 49 04	-23 10.8	K5 V	8.96	1.29	69.2	8.16	
899	Gl 40	B	00 49 06	-23 10.7	m	17.30		69.2	16.50	LP 826-170 sep 17" 71d d (pg) = 7.5 d (R) = 7.2 (NLTT)
900	NN 3093	A	01 20 12	+00 16.7	m	13.97	1.76	69.2	13.17	V(AB) = 13.61 d(m) = 1.02
901	NN 3094	B	01 20 12	+00 16.7	m	15.00		69.2	14.20	LP 587-50 sep 2.5" 70d
902	NN 4026		17 44 04	+24 39.7	m	12.67	1.51	69.2	11.87	LTT 15264 L 1350-84 LP 389-32
903	Gl 714		18 25 51	-58 18.1	M1	9.85	1.48	69.2	9.05	Sm 14
904	Gl 354	A	09 29 31	+51 54.4	F6 IV	3.17	0.46	69.1	2.37	THE Uma

905	GI 354	B	09 29 31	+51 54.4		13.80		69.1	13.00	
906	GI 375		09 56 34	-46 10.7	M3.5	11.27	1.55	69.1	10.47	LTT 3661 CAZ 60674 CFS 20559 NSV 4689
907	GI 456		12 05 52	-00 12.2	dM2	11.24	1.41	69.1	10.44	AC+00:1514-64
908	GJ 1171		13 28 08	+19 26.0		14.73	1.80	69.1	13.93	
909	GI 546		14 19 48	+29 51.7	K8 V	8.55	1.26	69.1	7.75	SB? in ApJ 314, 272
910	GI 712		18 19 44	+06 18.9	M3	12.58	1.48	69.1	11.78	Ross 136
911	GI 868		22 37 55	-29 56.1	K5 Ve	7.82	1.13	69.1	7.02	
912	GJ 1009		00 19 27	-31 41.0	dM2	11.16	1.48	69.0	10.35	BPM 46239
913	GI 42		00 50 34	-30 37.7	K3 V	7.17	0.93	69.0	6.36	
914	GI 104		02 33 03	+20 00.3	dM2	10.66	1.51	69.0	9.85	AC+19:1154-111
915	NN 3222	AB	03 21 45	-40 15.2	K0 V	6.92		69.0	6.11	CP-40:310 sep 2.1" 221d (1927) d (m) = 4.4 (IDS)
916	NN 3476		08 02 08	-65 52.7	K1 V	7.14	0.94	69.0	6.33	CD-65:599 LTT 3046 V, B-V from CPC
917	NN 3614		10 36 32	-20 25.8	DQP9	16.46		69.0	15.65	LTT 3902 L 681-8 LP 790-29
918	GJ 1157		12 20 26	-46 20.7	k	13.62	1.61	69.0	12.81	
919	GJ 1177	A	13 44 49	-32 10.9	K5 V	8.94	1.32	69.0	8.13	A=seq
920	GJ 1177	B	13 44 50	-32 10.9		9.12	1.36	69.0	8.31	B=pr
921	NN 3866		14 44 41	-17 29.5	DC9	16.48	0.94	69.0	15.67	LP 801-9
922	NN 3893		15 07 48	+19 33.2	m	13.35		69.0	12.54	LTT 14512 L 1271-10 LP 442-10 LHS.
923	GI 630.1	A	16 33 29	+57 14.8	dM4 e	12.90	1.60	69.0	12.09	LP 101-015
924	GI 630.1	B	16 33 31	+57 15.2	DQ8	15.00	0.49	69.0	14.19	LP 101-016

925	GI 654.2	wissenschaft in die schulen	17 04 00	+15 17.8	K0 V	7.09	0.94	69.0	6.28	
926	NN 3997		17 13 39	+19 03.3	M2	10.36	1.55	69.0	9.55	Steph 1453
927	GI 822.2		21 13 45	+25 13.5	G5 V	6.99	0.89	69.0	6.18	
928	GI 912		23 53 07	-06 24.9	M2	11.15	1.48	69.0	10.30	
929	GI 154		03 43 18	+26 03.8	K7	9.61	1.47	68.9	8.80	
930	GI 326	A	08 51 42	-12 55.6	M6 J	12.52	1.61	68.7	11.70	LP 726-18 L 820-019 V (AB) = 11.91 d(m) = 0.3
931	GI 326	B	08 51 42	-12 55.6		12.80		68.7	12.00	LP 726-19 sep 2" 75d d (R) = 0.5 ,d (pg) = 0.5 (LHS)
932	GI 105.4	A	02 37 09	-12 05.0	F5 V	5.50	0.44	68.6	4.68	BS 781 EPS Cet V(AB) = 4.82 d(m) = 0.15 , SBO (A&A 195,129)
933	GI 105.4	B	02 37 09	-12 05.0	F5 V	5.60		68.6	4.80	sep 0.1"
934	GI 532		13 50 01	+50 11.9	dM0 p	8.90	1.33	68.6	8.08	LTT 14050
935	NN 4203	A	21 31 16	+01 34.3	dM	13.35	1.68	68.6	12.53	LTT 16303
936	NN 4204	B	21 31 16	+01 34.3	m	14.50		68.6	13.70	LP 638-66
937	GI 255	A	06 55 30	-35 26.4	F8 IV-V	6.91	0.46	68.4	6.09	BS 2612 V (AB) = 6.23 d (m) = 0.16
938	GI 255	B	06 55 30	-35 26.4	F8 IV-V	7.10		68.4	6.30	a = 0.218" P = 16.74 yr
939	GJ 1141	A	10 59 38	+16 47.4	dM0	11.51	1.48	68.4	10.69	LTT 12954 LDS 917
940	GJ 1141	B	10 59 38	+16 47.4	dM0	11.63	1.48	68.4	10.81	LTT 12955
941	GI 841	A	21 53 35	-51 14.4	M0	10.40	1.50	68.4	9.60	

942	GI 841	wissenschaft in die schulen	21 53 35	-51 14.4	DQ7	14.68	0.16	68.4	13.86	LTT 8768 L 283-007 BPM 7606 LDS 765 WD2154- 512 sep 26.6" 252d
943	GI 108		02 40 51	-51 00.9	G3 IV	5.41	0.56	68.3	4.58	IOT Hor
944	GI 278	A	07 31 25	+32 00.0	A1 V	1.94	0.04	68.3	1.11	ALF Gem BS 2891 ADS 6175 V (AB) = 1.56 d (m) = 0.95
945	GI 278	B	07 31 25	+32 00.0	A m	2.85		68.3	2.02	BS 2890 a = 6.295" P = 420.07 yr
946	GI 278	C	07 31 26	+31 58.8	M0.5Ve	9.07	1.49	68.3	8.24	YY Gem sep (AC) 72.5" 64d (1835- 1955) d(m) = 0.0
947	NN 3252		03 48 27	-01 01.3	m	18.02		68.2	17.19	LP 593-68
948	GJ 1099		07 31 43	+01 06.2	m	11.93	1.47	68.2	11.10	
949	GI 819	A	21 04 24	-14 07.4	K1 Ve	7.15	0.90	68.1	6.32	
950	GI 819	B	21 04 24	-14 07.4	M0	10.20		68.1	9.40	
951	GI 837		21 44 17	-16 21.3	A6 m	2.87	0.29	68.1	2.00	DEL Cap A5MF2 (IV) Mich
952	NN 3203		03 05 53	-24 57.6	m	9.50		68.0	8.70	LTT 1480 L 587-3 cmp with LTT 1486 = - 25:1278 ?
953	GI 157	A	03 54 57	-01 18.0	K4 V	8.04	1.11	68.0	7.20	
954	GI 157	B	03 54 57	-01 18.0	dM3 e	11.61	1.47	68.0	10.77	
955	NN 3305		04 35 06	-02 35.5	M1	10.59	1.45	68.0	9.75	Steph 497
956	GI 298		08 08 42	-52 49.7	m	11.77	1.50	68.0	10.93	L 242-066
957	GI 378		09 59 14	+48 21.1	dM2	10.07	1.37	68.0	9.23	

958	NN 3649	S	wissenschaft in die schulen	11 10 00	+19 12.4	M1	10.77	1.50	68.0	9.93	Steph 928
959	GJ 2084	AB		11 19 37	-24 30.2	K4 V J	9.08	1.26	68.0	8.24	ADS 8131
960	NN 3775			13 15 30	+02 29.9	m	12.97		68.0	12.13	LTT 13861 L 1049-51 LP 557-46
961	NN 3809	AB		13 46 28	+03 02.6	M2:	11.19	1.57	68.0	10.35	LTT 14032 Wolf 1495 has 11.3 V, M2, comp. 0.6"
962	NN 3894			15 09 12	-10 02.9	M4	14.26	1.66	68.0	13.42	
963	GJ 619			16 19 12	+41 04.6	dM0 p	8.98	1.30	68.0	8.14	
964	GJ 2128			17 14 17	+08 06.8	M3.5	11.49	1.55	68.0	10.65	LTT 15114
965	GJ 707			18 08 44	-43 27.1	K7 Ve	8.37	1.31	68.0	7.53	Sm 11
966	GJ 743.1	A		19 03 02	-37 08.2	F8 V	4.87	0.52	68.0	4.03	GAM Cra V (AB) = 4.19 d (m) = 0.13
967	GJ 743.1	B		19 03 02	-37 08.2	F8 V	5.00		68.0	4.16	a = 1.907" P = 120.42 yr Heintz 1963
968	NN 4228			21 49 23	+13 22.3	m	13.93		68.0	13.09	LP 518-058
969	GJ 684	A		17 34 28	+61 54.8	G0 Va	5.34	0.56	67.9	4.50	LTT 15223 ADS 10660 V(AB) = 5.23 d(m) = 2.89
970	GJ 684	B		17 34 28	+61 54.8	K3 V	8.06	1.10	67.9	7.22	AB: a = 1.52" 76.00 yr, comp C in LTT 15224 m = 11.2
971	GJ 656			17 05 40	-60 40.4	K0 V	7.41	0.89	67.8	6.57	
972	GJ 720	A		18 33 50	+45 41.8	dM2	9.85	1.42	67.8	9.01	LFT 1421
973	GJ 720	B		18 33 59	+45 42.9	m	13.02	1.60	67.8	12.18	VB 9 LTT 18475
974	GJ 231.3			06 16 55	-06 37.6	M4	13.06	1.70	67.6	12.21	Ross 417

975	GI 397		10 28 27	+45 47.5	K7 V	8.86	1.33	67.6	8.01	
976	NN 3770		13 10 11	-47 12.2	DC9+	17.05	1.40	67.6	16.20	ER 8 IAU Coll. 114 or ApJ 346, 456
977	GI 184		04 59 17	+53 04.8	dM0	9.93	1.41	67.5	9.08	
978	NN 4338	B	23 26 55	+41 11.7	M3 :	12.44	1.61	67.5	11.59	USN 780 sep 17" 215d
979	GI 13		00 14 24	-52 55.9	G2 V	6.84	0.64	67.4	5.98	
980	GI 514.1		13 27 29	-08 26.6	M4 :	14.25	1.65	67.4	13.39	Ross 476
981	GI 236		06 30 07	-26 59.5	M0	11.41	1.37	67.3	10.55	L 597-031
982	GI 310		08 31 55	+67 28.1	dM1	9.30	1.42	67.3	8.44	
983	GI 565		14 48 50	-24 05.6	K5 V	7.83	1.00	67.3	6.97	
984	GI 52		01 03 45	+63 40.2	K7 V	8.98	1.30	67.2	8.12	
985	NN 4029		17 47 56	+22 42.0	m	20.10		67.2	19.20	LP 389-18
986	GJ 1228		18 29 22	+54 45.0	DXP8	15.50	0.49	67.2	14.64	
987	GI 800	A	20 40 04	-19 05.2	dM2	10.84	1.43	67.2	9.98	V(AB) = 10.78 d(m) = 3.2
988	GI 800	B	20 40 04	-19 05.2		14.00		67.2	13.10	sep 2" 240d, two optical companions
989	NN 4337	A	23 26 56	+41 11.9	M2	11.87	1.52	67.2	11.01	USN 781
990	GJ 1096		07 13 03	+33 14.8	m+	14.48	1.75	67.1	13.61	
991	NN 3097		01 22 58	+09 30.2	dM3.5	13.13	1.68	67.0	12.30	LTT 10514 Wolf 66
992	NN 3117	A	01 48 12	+64 11.4	dM2	11.37		67.0	10.50	
993	NN 3118	B	01 48 12	+64 11.2	DA6	14.50		67.0	13.60	sep 10" 178d, y = 13.97 b-y = 0.134 -> mod = 1.99 uvby
994	NN 3208		03 11 10	+28 30.2	m	16.77	2.15	67.0	15.90	LP 299-36
995	NN 3256		03 52 01	-09 18.3	M3	11.22	1.53	67.0	10.35	Steph 430

996	GI 167.3		04 15 37	-59 25.3	K2 IV	4.44	1.07	67.0	3.57	EPS Ret
997	NN 3856		14 29 48	+16 14.1	m	13.61		67.0	12.74	LP 440-38
998	NN 3860		14 33 33	+09 58.0	K0	7.50	0.99	67.0	6.63	LTT 14312
999	GI 637		16 42 30	-72 52.8	m	11.35	1.57	67.0	10.48	L 074-113
1000	NN 4109		19 23 08	+28 15.0	M3.5	12.48	1.56	67.0	11.60	LTT 15670 Ross 164 = LTT 15673 L 1427-13
1001	GI 826		21 17 23	+62 22.4	A7 IV-V	2.44	0.22	67.0	1.57	ALF Cep
1002	GI 828	A	21 23 45	-45 01.7	K0 V	7.48	0.91	67.0	6.61	
1003	GI 828	B	21 23 36	-45 01.0	m	14.10		67.0	13.20	L 353-009
1004	NN 4276		22 23 28	+59 09.8	m	12.91		67.0	12.04	
1005	NN 4352		23 35 33	-16 30.8	M2	11.34	1.57	67.0	10.47	LTT 9634 L 792-25
1006	GI 319	A	08 40 02	+09 44.7	M0 J	9.70	1.41	66.8	8.82	V(AB) = 9.65 d(m) = 3.2
1007	GI 319	B	08 40 02	+09 44.7		13.10		66.8	12.20	sep(AB) 2"
1008	GI 319	C	08 40 09	+09 44.5	M3.5	11.79	1.54	66.8	10.91	sep(AB-C) 115" 96d (LHS)
1009	GI 471		12 28 46	+09 05.6	dM1	9.70	1.45	66.8	8.82	
1010	NN 3181		02 43 51	+16 13.1	M6	16.86	2.02	66.7	15.98	LP 411-6
1011	GI 116		02 48 58	+34 11.9	dM0	9.55	1.34	66.7	8.67	LTT 10932 Wolf 1323
1012	GI 289		07 45 15	+20 30.4	M2	11.46	1.52	66.7	10.58	Wolf 1421
1013	GI 481		12 38 35	+15 39.4	K4	7.96	1.12	66.7	7.08	
1014	GI 233	AB	06 23 14	+18 47.3	K2 V e	6.76	0.94	66.6	5.88	ADS 5054 sep 1.3" 162d d(m) = 6.8
1015	GI 141		03 22 32	-05 31.7	K5 V	7.86	1.16	66.5	6.97	
1016	NN 3965		16 33 25	+43 24.0	DA8	14.82	0.42	66.5	13.93	PG

1017	Gl 903		23 37 17	+77 21.2	K1 IVe	3.21	1.03	66.5	2.32	GAM Cep
1018	Gl 622		16 22 17	-21 49.1	K5	10.40	1.45	66.4	9.51	
1019	Gl 792		20 29 34	+38 22.9	M4	13.48	1.76	66.4	12.59	Ross 188
1020	Gl 207.1		05 31 09	+01 54.8	dM2.5e	11.53	1.57	66.3	10.64	V 371 Ori
1021	Gl 332	A	08 57 24	+41 58.9	F3 V	4.11	0.37	66.3	3.22	Kpr 37
1022	Gl 332	B	08 57 24	+41 58.9	G5 V	6.18	0.65	66.3	5.29	
1023	Gl 245		06 43 08	+43 37.8	G0 V	5.24	0.56	66.2	4.34	PSI(5) Aur
1024	Gl 553		14 28 12	-08 25.3	K7 V	9.40	1.40	66.1	8.50	
1025	Gl 815	A	20 58 09	+39 52.7	dM3 eJ	10.34	1.52	66.1	9.44	AC +39:57322 F 54 V(AB) = 10.12 d(m) = 1.9 : SBO in A&A 200, 135
1026	Gl 815	B	20 58 09	+39 52.7		11.90		66.1	11.00	sep 0.9" 82d
1027	Gl 836.7		21 42 07	+14 32.6	G0 V	5.94	0.59	66.1	5.04	
1028	NN 3069		00 59 04	+53 54.8	m	15.12	1.84	66.0	14.20	
1029	NN 3095		01 20 20	+07 09.3	G5	7.33		66.0	6.43	LTT 10501
1030	GJ 1046		02 16 59	-37 00.9	M3	11.62	1.50	66.0	10.70	
1031	GJ 1050		02 37 44	-34 19.5	m	11.75	1.52	66.0	10.85	
1032	NN 3213		03 13 48	+45 11.4	m	12.39		66.0	11.49	LTT 17492
1033	NN 3235		03 32 09	-05 00.3	k-m	13.10		66.0	12.20	LTT 1682 L 876-3 LP 653-8
1034	NN 3247		03 40 57	-09 43.6	m	14.70		66.0	13.80	
1035	Gl 225.2	A	05 58 28	-31 02.2	K5 V	8.28	1.14	66.0	7.38	V(ABCD) = 7.85 d(m) = 0.78
1036	Gl 225.2	B	05 58 28	-31 02.2		9.10		66.0	8.20	AB: a = 0.94" P = 72.0 yr

1037	GI 225.2	A	05 58 28	-31 02.2	K5 V	8.30		66.0	7.40	a(AB-C) = 3.95" 390.6 yr; D(12.8m) opt. sep(A- D) 11.9" 191d (1960)
1038	GI 264.1	A	07 02 25	-43 32.3	G3 V	5.55	0.64	66.0	4.65	
1039	GI 264.1	B	07 02 25	-43 32.3	K0 V	6.79	0.80	66.0	5.89	
1040	NN 3438		07 14 44	+39 22.0	M0.5	10.33	1.51	66.0	9.43	LTT 12003 Ross 987
1041	GJ 2070		08 31 53	-00 58.0	M3.5	12.73	1.62	66.0	11.80	LTT 3171
1042	NN 3753		12 47 52	+55 22.3	DA4	12.31	0.03	66.0	11.41	GD 319 WD1247 +553
1043	NN 3846		14 22 27	+09 06.7	m	12.26	1.63	66.0	11.36	LTT 14237 L 1124-13 LP 500-19
1044	GI 620		16 20 07	-24 35.1	M1	10.23	1.47	66.0	9.33	
1045	NN 3953		16 23 29	+26 08.4	m	12.24		66.0	11.34	LTT 14889 L 1418-61 LP 386-49
1046	GI 723		18 37 32	-10 30.3	M0.5	11.49	1.55	66.0	10.59	Wolf 1466
1047	NN 4216		21 42 24	-06 00.7	M3.5	12.81	1.64	66.0	11.90	LTT 8678 Wolf 937
1048	NN 4224	AB	21 46 00	-41 46.0	M6	12.20	1.59	66.0	11.30	LTT 8708 BPM 44196 L 427-34 Sm 89 V(AB) = 11.51 d(m) = 0.
1049	GI 863		22 30 31	+09 07.1	M0	10.37	1.51	66.0	9.47	LFT 1723
1050	NN 4367		23 47 55	-09 49.9	m	13.45		66.0	12.55	LP 763-12
1051	GJ 1081		05 29 38	+44 47.2	k-m	12.21	1.60	65.9	11.30	
1052	GI 538		14 01 05	+11 01.8	G8 V	6.30	0.74	65.8	5.39	
1053	GI 562		14 44 03	+16 43.1	K5 V	9.25	1.27	65.8	8.34	
1054	GI 864		22 33 35	-01 05.6	dM1	10.01	1.44	65.8	9.10	
1055	GI 907		23 45 31	+48 44.2	M1.5	12.07	1.66	65.6	11.15	Ross 249

1056	GJ 1006	wissenschaft in die schulen A	00 13 36	+19 35.6	M4	12.27	1.50	65.5	11.35	LP 404-61 L 1226-9
1057	GJ 1006	B	00 13 38	+19 35.8	M4.5	13.22	1.60	65.5	12.30	LP 404-62 L 1226-8
1058	GI 330		08 54 21	+11 50.7	dM5	10.60	1.53	65.5	9.68	
1059	GI 353		09 28 54	+36 32.9	dM2	10.19	1.50	65.5	9.27	
1060	GI 655		17 05 01	+21 37.1	M3	11.61	1.56	65.5	10.69	Ross 863
1061	GI 65.2		01 37 37	-46 45.7	M0	9.86	1.16	65.4	8.94	
1062	GJ 1059		03 19 41	+41 50.3	m	15.33	1.89	65.4	14.41	
1063	GI 227		06 03 49	+15 33.0	dK0 e	6.76	0.81	65.3	5.83	
1064	GI 329		08 52 47	-24 12.3	K2/3 III	8.66	1.00	65.3	7.73	
1065	GI 202		05 21 30	+17 20.3	F8 Ve	4.99	0.53	65.2	4.06	
1066	GJ 1204		16 33 43	+08 54.9	m	13.80	1.65	65.2	12.87	
1067	GI 616		16 12 54	-08 14.3	G1 V	5.49	0.65	65.1	4.56	
1068	GJ 2021		01 06 53	-24 46.3	m	14.52		65.0	13.58	PS 131 LP 826-603 TS 336
1069	NN 3135		02 03 38	-30 25.0	M3.5	12.15		65.0	11.21	LFT 180 LTT 1101
1070	NN 3198		03 01 47	-20 33.9	M3	12.84	1.59	65.0	11.90	LP 771-77
1071	NN 3233		03 29 05	+37 53.6	G5	7.28		65.0	6.34	
1072	NN 3279		04 21 16	-57 33.2	m	11.80		65.0	10.90	LTT 1960 L 178-49
1073	NN 3426		07 03 51	+48 46.2	m	13.40		65.0	12.46	
1074	NN 3503		08 29 01	-10 19.5	m	15.00		65.0	14.10	LP 725-15
1075	NN 3508		08 34 20	+15 19.0	k	11.80		65.0	10.90	LTT 12243
1076	NN 3720		12 16 15	+30 02.5	m	16.32	1.98	65.0	15.40	LP 320-359 San 47
1077	GJ 1158		12 26 49	-55 42.8	M4	13.27	1.62	65.0	12.33	
1078	NN 3876		14 53 34	+82 43.2	F9 V	5.64	0.68	65.0	4.70	LTT 14431
1079	NN 3890		15 03 14	+60 34.6	M2	11.00	1.50	65.0	10.06	LTT 14486 Ross 1051

1080	NN 4185	A	21 13 56	+29 39.3	m	12.68		65.0	11.74	LTT 16240 Ross 776
1081	NN 4186	B	21 13 54	+29 39.2	m	13.49		65.0	12.55	LP 341-14 sep 26" 259d
1082	NN 4206		21 34 00	-63 57.0	M2	10.62	1.44	65.0	9.68	BPM 14175 Sm 85
1083	G1 875.1		22 49 30	+31 29.4	dM3.5e	11.63	1.55	65.0	10.69	LFT 1741 AC +31:70565
1084	NN 4306		22 53 32	+17 32.7	M0	10.50	1.49	65.0	9.56	Steph 2065
1085	G1 132		03 13 24	-45 50.7	G3 V	6.76	0.58	64.9	5.82	
1086	G1 163		04 07 56	-53 30.7	M3.5	11.81	1.50	64.9	10.87	L 229-091
1087	GJ 1062		03 35 48	-11 36.7	M2	13.01	1.66	64.8	12.07	Ross 578
1088	NN 3542		09 14 02	+58 38.9	m	15.11	1.85	64.8	14.17	
1089	NN 3077	A	01 09 19	+04 39.6	m	12.89	1.62	64.6	11.94	G070-043 LTT 10438
1090	NN 3078	B	01 09 21	+04 38.6	m	13.91	1.70	64.6	12.96	sep 63.5" 146d
1091	NN 3162		02 30 15	-14 24.5	DC	15.76	0.75	64.6	14.81	LP 710-047 USNO 695
1092	G1 681		17 32 37	+12 35.7	A5 III	2.08	0.15	64.6	1.13	ALF Oph
1093	G1 9.1		00 06 53	-46 01.4	K0 III	3.88	1.03	64.5	2.90	EPS Phe
1094	G1 316.1		08 37 42	+18 35.0	m	17.68	2.02	64.5	16.70	LP 425-140
1095	G1 376		09 58 08	+32 10.2	G2 Va	5.35	0.66	64.5	4.40	
1096	G1 328		08 52 32	+01 45.1	dM1	9.99	1.40	64.3	9.03	
1097	G1 728		18 46 40	+17 23.2	dM1.5	9.22	1.28	64.3	8.26	
1098	G1 759		19 22 35	+11 50.2	G8 IV	5.16	0.77	64.3	4.20	
1099	G1 808		20 44 30	-79 29.0	M2.5	11.85	1.50	64.3	10.89	L 046-163
1100	G1 134		03 14 52	+38 04.7	dM1.5e	10.28	1.48	64.2	9.32	
1101	G1 351	A	09 28 44	-40 14.8	F3 IV	4.12	0.36	64.2	3.16	PSI Vel V (AB) = 3.60 d (m) = 0.66
1102	G1 351	B	09 28 44	-40 14.8	F0 IV	4.65		64.2	3.69	a = 0.795" P =33.99 yr
1103	G1 121.1		03 00 20	-18 21.6	m	11.80	1.53	64.1	10.80	LP 771-72 L 730-041

1104	GI 557	wissenschaft in die schulen	14 32 30	+29 57.7	F2 V	4.46	0.36	64.1	3.50	SIG Boo
1105	GI 727		18 46 07	+10 41.7	dK4	7.97	1.07	64.1	7.00	
1106	NN 3020		00 13 33	-48 32.1	M5	11.54	1.46	64.0	10.57	LTT 123 L 290-72 BPM 30080 CFS 56 Sm 156
1107	GJ 1014		00 33 16	+10 12.4		15.32	1.89	64.0	14.35	
1108	GI 101.1		02 29 18	-46 54.4	m	11.27	1.03	64.0	10.30	
1109	NN 3296		04 30 36	+20 38.7	m	14.60		64.0	13.60	LTT 11454
1110	NN 3404	A	06 39 33	+03 37.9	m	12.06		64.0	11.09	
1111	NN 3405	B	06 39 36	+03 38.6	m	13.33		64.0	12.36	sep 51" 39d
1112	NN 3654		11 14 13	-27 40.3	M4	13.70		64.0	12.70	LTT 4168 L 611-67 LP 906-9
1113	NN 3685	A	11 45 08	+00 32.0	m	13.25		64.0	12.28	LTT 13239 L 1044-70 LP 613-49
1114	NN 3686	B	11 45 09	+00 31.8	m	17.60		64.0	16.60	LP 613-50 sep 24" 125d (NLTT)
1115	NN 3815		13 51 34	+67 04.2	m	15.69	1.90	64.0	14.70	LP 66-274
1116	NN 3942		16 07 47	+53 04.4	dM0	10.19	1.45	64.0	9.22	
1117	GI 626.2		16 26 40	+36 52.2	DZA6	13.85	0.17	64.0	12.88	Ross 640
1118	NN 4024		17 40 33	+05 48.7	M2	10.67		64.0	9.70	
1119	NN 4069		18 39 59	+39 39.4	m	13.42		64.0	12.45	
1120	Wo 9716		20 59 30	-57 09.3	M4	12.85	1.65	64.0	11.88	LTT 8340 L 211-59 GJ 2151 Sm 70
1121	NN 4231		21 49 40	+05 23.5	dM2	12.11	1.53	64.0	11.14	Steph 1950 Rob 299
1122	GI 492		12 57 38	+03 45.5	DC9	15.79	0.64	63.9	14.82	Wolf 457
1123	GJ 1037		01 15 20	+15 55.1	DQ6	13.82	0.12	63.8	12.84	Wolf 1516

1124	G1 303		08 17 02	+27 22.9	F6 V	5.14	0.47	63.8	4.16	CHI Cnc
1125	NN 3666		11 26 23	+10 26.8	M3	12.56	1.60	63.8	11.58	LTT 13128 Wolf 398
1126	GJ 1010	A	00 20 41	+76 54.7	k-m	11.30	1.49	63.7	10.32	LP 12-361
1127	GJ 1010	B	00 20 43	+76 54.8	m	14.00		63.7	13.00	LP 12-362 sep 11" 64d (LHS)
1128	G1 548	A	14 23 24	+23 51.4	dM1	9.75	1.44	63.7	8.77	
1129	G1 548	B	14 23 27	+23 51.6	dM2	10.00	1.46	63.7	9.02	
1130	G1 123		03 03 50	+01 47.2	M0 V	9.09	1.38	63.6	8.11	
1131	G1 421	A	11 12 50	-17 51.7	K7 V	9.97	1.36	63.6	8.99	U260
1132	G1 421	B	11 12 51	-17 51.6	K7 V	10.04	1.38	63.6	9.06	
1133	G1 421	C	11 12 46	-17 50.6	M3.5	13.64	1.58	63.6	12.66	LTT 4155 L 755-50
1134	G1 830		21 27 16	-12 43.6	M0 V	9.10	1.28	63.6	8.12	
1135	G1 366		09 41 42	+76 17.3	M1.5	10.62	1.41	63.5	9.63	AC+76:3952
1136	G1 425	A	11 18 57	-20 10.7	K4/5 V J	8.74	1.36	63.5	7.75	ADS 8138 SZ Crt V (AB) = 8.61 d (m) = 2.2
1137	G1 425	B	11 18 57	-20 10.7	m	11.00		63.5	10.00	sep 6.3" 207d - 5.1" 329d (1877- 1959)
1138	G1 484		12 42 38	+39 33.0	G0 V	5.95	0.55	63.5	4.96	
1139	G1 795	A	20 37 05	+04 47.6	K4 V	8.18	1.22	63.5	7.19	Kpr 99 V (AB) = 7.87 d (m) = 1.2
1140	G1 795	B	20 37 05	+04 47.6	K8 V	9.40		63.5	8.40	a = 0.80" P = 39.40 yr
1141	G1 812	A	20 54 07	-05 02.2	M3	11.91	1.51	63.5	10.92	Ross 193
1142	G1 812	B	20 54 06	-05 02.0	DC9+	16.60	1.16	63.5	15.61	Ross 193B VB 11
1143	NN 4312		23 05 25	+68 23.8	m	12.45	1.54	63.5	11.46	
1144	GJ 1030		01 04 03	+15 00.5	k-m	11.43	1.47	63.4	10.44	
1145	GJ 1094		07 00 17	-06 43.3	K5 V	8.38	1.08	63.3	7.39	LTT 2722

1146	Gl 314	A	08 36 57	-22 29.4	G3 V	5.28	0.73	63.3	4.29	ADS 6914 V (AB) = 5.04 d (m) = 1.30
1147	Gl 314	B	08 36 57	-22 29.4	K0 V	6.80		63.3	5.80	a = 1.888" P = 140.0 yr
1148	Gl 802		20 41 53	+55 08.8	dM5 e	14.68	1.79	63.3	13.69	Wolf 1084
1149	Gl 782		20 07 26	-20 38.2	K4 Vp	8.92	1.29	63.2	7.92	
1150	Gl 483		12 41 59	+52 02.1	K3 V	7.04	0.94	63.1	6.04	
1151	Gl 582		15 18 25	-48 08.1	G2 V	5.65	0.65	63.1	4.65	NU(2) Lup
1152	GJ 1212		17 10 59	-08 21.4	dM1	12.05	1.61	63.1	11.05	
1153	NN 4129		19 55 45	+01 54.6	k	11.95	1.55	63.1	10.95	LTT 15840 LP 634-2 L 1069-28
1154	GJ 1036		01 14 57	-35 58.6	m	11.42	1.53	63.0	10.42	
1155	NN 3139		02 07 10	-14 35.4	M3	11.82	1.54	63.0	10.80	LFT 185 LTT 1122 L 728-1 LP 709-40
1156	Gl 89		02 10 42	-30 57.5	A2 Vn	5.28	-0.02	63.0	4.30	MU For
1157	NN 3218		03 19 19	-06 51.1	M2	11.37	1.50	63.0	10.37	LTT 17505
1158	NN 3261		04 02 59	+05 36.6	dM5 e	12.89		63.0	11.89	Rob 256
1159	NN 3294		04 27 31	+17 23.3	k-m	14.57	1.75	63.0	13.60	VA575 LP 415-148
1160	NN 3320		04 58 11	+24 48.4	M2.5	11.51	1.48	63.0	10.50	LTT 11561 Ross 794
1161	Gl 260		06 59 25	-61 16.1	K0 IV-V	6.82	0.80	63.0	5.82	
1162	Gl 294	A	07 56 52	-60 10.1	G2 V	5.60	0.57	63.0	4.60	BS 3138 CP- 59:944
1163	Gl 294	B	07 57 00	-60 09.8	k	9.88	1.34	63.0	8.88	V(BC) = 9.83 d(m) = 3.6
1164	Gl 294	C	07 57 00	-60 09.8		13.50		63.0	12.50	sep(BC) = 2.3" 270d (1940)
1165	NN 3492		08 14 51	-76 00.0	k-m	11.85		63.0	10.85	LTT 3096 L 34-16

1166	NN 3625	S	wissenschaft in die schulen	10 47 30	-79 12.0	m	13.45		63.0	12.45	L 37-56
1167	NN 3633			10 53 55	+07 39.4	K0	7.34	0.92	63.0	6.34	LTT 12921
1168	NN 3689	A		11 49 48	+10 13.5	K0	7.54	1.06	63.0	6.54	LTT 13274
1169	NN 3690	B		11 49 45	+10 17.6	m	15.00		63.0	14.00	LP 493-64 sep 232" 348d
1170	G1 461	AB		12 17 52	+00 51.7	M0 V	10.10	1.47	63.0	9.10	RST 5366 sep 1.3" d(m) = 2.4 , V (AB) = 9.99 (= 10.15 Rossello)
1171	GJ 1167	A		13 07 13	+29 15.2	dM5	14.18	1.72	63.0	13.18	LDS 1365A LTT 13799 LP 322-836 San 224 comp B doesn't exist
1172	G1 516	A		13 30 18	+17 04.2	dM3.5e	12.01	1.53	63.0	11.01	AC+18:1204- 96 V(AB) = 11.40 d(m) = 0.3
1173	G1 516	B		13 30 18	+17 04.2	dM3.5e	12.30		63.0	11.30	LP 438-8 a = 3.17" P = 430 yr : Heintz AJ 99, 420 (1990)
1174	NN 3885			14 58 51	+05 45.0	M3	12.10	1.45	63.0	11.10	LTT 14454 L 1126-121 LP 561-68 comp B: SpT. K: optical
1175	NN 3973			16 45 54	-15 39.0	M2	10.94	1.50	63.0	9.94	LP 806-8
1176	G1 708.3			18 13 48	+01 30.8	M5	12.52	1.61	63.0	11.52	L 1064-075
1177	NN 4102			19 09 13	-82 37.8	M3.5	12.70		63.0	11.70	LTT 7606 L 22-69

1178	NN 4262	S	22 08 37	-02 47.4	k-m	12.14	1.56	63.0	11.10	LTT 8900 L 1003-48 LP 699-52
1179	GJ 1268		22 22 56	+51 44.8	m+	14.94	1.81	63.0	13.94	
1180	NN 4292		22 40 57	+21 52.6	m	15.00		63.0	14.00	
1181	NN 4319		23 13 36	+06 28.4	k	13.14	1.63	63.0	12.10	LTT 16837
1182	NN 4355		23 36 16	-07 58.1	DA	13.26	0.18	63.0	12.26	GD 1212
1183	GJ 1113		08 37 15	+43 17.8	K2 V	9.32	1.08	62.9	8.31	Wolf 318
1184	NN 3833		14 11 47	+30 26.9	K4	8.04	1.08	62.9	7.03	LTT 14171
1185	NN 3463		07 49 11	+05 41.0	m	14.75	1.82	62.8	13.74	LTT 12076
1186	GJ 1169		13 14 14	+28 08.0	m	13.26	1.65	62.8	12.25	LTT 13849 San 259
1187	G1 291	A	07 49 27	-13 45.8	F9 V	5.72	0.57	62.7	4.71	ADS 6420 V (AB) = 5.17 d (m) = 0.73
1188	G1 291	B	07 49 27	-13 45.8	G4 V	6.17	0.65	62.7	5.16	a =0.622" P = 23.30 yr ; UBV from d (m) =0.7 (Eggen) !
1189	G1 246		06 44 15	+37 35.1	DA2	12.06	-0.08	62.6	11.04	L 1534-001
1190	G1 787		20 16 07	-46 35.1	K5 V	8.72	1.16	62.6	7.70	Sm 51
1191	G1 36		00 46 57	-23 29.2	G9 V	7.16	0.78	62.5	6.14	
1192	NN 3366		05 44 39	-05 12.9	m	14.54	1.78	62.5	13.52	LP 658-33
1193	G1 288	A	07 43 43	-34 04.4	G0 V	5.36	0.59	62.5	4.34	
1194	G1 288	B	07 43 51	-33 49.2	m	16.59	1.20	62.5	15.57	VB3
1195	G1 339.3		09 13 45	-37 12.2	F5 III	4.62	0.45	62.5	3.60	K Vel
1196	GJ 1254		20 32 40	+61 34.0	m	12.52	1.52	62.5	11.50	
1197	NN 3232		03 27 37	+19 55.7	K7 V	10.79	1.39	62.4	9.77	Hy 207

1198	GI 271	A	07 17 08	+22 04.6	F1 IV-V	3.53	0.34	62.4	2.51	DEL Gem BS 2777 ADS 5983 V (AB) = 3.52 d (m) = 4.67
1199	GI 271	B	07 17 08	+22 04.6	K3 V	8.20		62.4	7.20	a = 6.975" P 1200 yr
1200	GI 579		15 05 16	+25 07.2	K7 V	10.09	1.41	62.2	9.06	
1201	GJ 1174		13 38 08	+44 01.3	M3	12.76	1.64	62.1	11.73	Ross 1026
1202	GI 734	A	18 52 33	+10 54.6	dM0	9.44	1.36	62.1	8.41	V(AB) = 9.37 d(m) = 2.5 :
1203	GI 734	B	18 52 33	+10 54.6		12.30		62.1	11.30	sep 5.2" 21d (1961)
1204	GI 10		00 08 43	-15 44.5	F7 V	4.89	0.49	62.0	3.85	Viln 82 no 157
1205	GJ 2010		00 34 56	-21 10.1	DA7	14.53	0.45	62.0	13.49	
1206	GJ 1033		01 11 00	-23 10.0		14.16	1.58	62.0	13.12	PS 151 BPM 46989 (V, V- I = 14.26, 2.86: PS)
1207	NN 3183		02 48 51	+29 17.1	m	13.96		62.0	12.92	LP 298-42
1208	NN 3223		03 22 38	-01 59.0	DZ9	16.12	0.80	62.0	15.08	
1209	GI 150.1	A	03 41 02	+16 31.1	dM0	9.96	1.45	62.0	8.92	
1210	GI 150.1	B	03 40 55	+16 30.8	dM0	10.81	1.48	62.0	9.77	AC+17:449- 111
1211	Wo 9189		05 41 08	-80 30.5	G1 V	5.65	0.60	62.0	4.61	LFT 429
1212	NN 3455		07 34 52	-51 48.5	m	12.45		62.0	11.41	LTT 2899 L 240-16
1213	GJ 1118		08 56 58	-31 01.0	k-m	13.80	1.64	62.0	12.76	
1214	NN 3540		09 09 06	+28 07.1	m	12.29	1.56	62.0	11.25	
1215	NN 3563		09 40 17	-19 00.2	M3	11.96	1.58	62.0	10.90	LTT 3561 L 750-79 LP 788-24
1216	NN 3573		09 53 40	+22 53.5	m	14.20		62.0	13.20	

1217	NN 3702	S	wissenschaft in die schulen	12 01 27	-32 44.8	M4.5	14.00		62.0	13.00	LTT 4503 L 541-90 LP 908-11
1218	GJ 1161	A		12 32 54	-34 36.3	K4 V	7.91	1.04	62.0	6.87	LTT 4787 LDS 413
1219	GJ 1161	B		12 32 58	-34 37.7		11.91	1.60	62.0	10.87	LTT 4788
1220	NN 3764			13 06 27	-39 52.3	M3.5	12.86	1.60	62.0	11.80	LTT 5034 L 472-66
1221	Gl 511.1			13 24 17	+63 31.0	dG6	6.50	0.74	62.0	5.46	
1222	NN 3813			13 50 11	+14 40.2	M2	11.63	1.50	62.0	10.59	LTT 14049 Wolf 515
1223	Gl 570.1			14 54 42	-48 39.5	G5 V	6.35	0.71	62.0	5.31	
1224	NN 3884			14 58 45	+07 21.7	M3.5	12.73	1.49	62.0	11.70	LTT 14453 L 1126-79 LP 561-36
1225	NN 3910			15 29 52	+29 01.2	m	14.30		62.0	13.26	
1226	NN 3945			16 11 17	-28 22.6	M3.5	12.96		62.0	11.92	LTT 6474 L 626-41 LP 917-1
1227	GJ 1226			18 18 24	-01 03.8	M3.5	12.71	1.66	62.0	11.70	
1228	NN 4198			21 27 36	-40 55.4	M3	13.19	1.62	62.0	12.20	LTT 8542 L 425-35
1229	GJ 1269	A		22 25 39	+11 59.6	K0 V	7.15	0.90	62.0	6.11	LTT 16584 ADS 15962A V (AB) = 7.08 d (m) = 3.0
1230	GJ 1269	B		22 25 39	+11 59.6		10.10		62.0	9.10	ADS 15962B sep 0.9" 227d (1959)
1231	Gl 115			02 48 52	-44 17.0	F8 V	8.17	0.55	61.9	7.13	mod = 3.63 uvby
1232	Gl 165	AB		04 09 27	+50 24.2	M3.5	13.67	1.75	61.9	12.63	Ross 29 comp.B: CHARA 15 (AJ 93, 688) sep 1.261" (1983)
1233	Gl 614			16 08 47	+43 57.0	K0 V	6.66	0.88	61.9	5.62	

1234	GI 375		00 47 37	-10 54.8	F7 IV-V	5.17	0.50	61.8	4.12	PHI(2) Cet BS 235
1235	GJ 1183	A	14 25 23	-00 09.2	m	13.95	1.65	61.8	12.90	
1236	GJ 1183	B	14 25 24	-00 09.1	m	14.03	1.68	61.8	12.98	
1237	GI 586	A	15 25 27	-09 10.2	K2 V	6.92	0.81	61.8	5.87	LTT 6180
1238	GI 586	B	15 25 30	-09 10.8	K2 V	7.58	0.92	61.8	6.53	LTT 6181
1239	GI 651		17 01 12	+47 08.4	G8 V	6.77	0.73	61.8	5.72	
1240	GI 489		12 55 07	-14 11.6	K4 V	9.12	1.12	61.7	8.07	
1241	GJ 1013		00 29 02	-06 07.9	m	12.75	1.64	61.6	11.70	
1242	GI 43		00 53 10	-52 06.5	m	12.36	1.51	61.6	11.31	L 220-80 Sm 178
1243	GI 121		03 00 11	-23 49.2	A4 IV	4.08	0.16	61.6	3.03	TAU(3) Eri
1244	GI 515		13 27 40	-08 18.6	DA5	12.31	0.08	61.6	11.26	LFT 1014 Wolf 485A PG
1245	GI 894		23 14 51	-42 27.9	K3/5 V	10.38	1.32	61.6	9.33	Sm 131
1246	GI 263		07 01 56	-10 25.3	M3.5	11.29	1.52	61.5	10.23	Ross 54
1247	GI 699.1		17 56 40	+82 44.1	DA7	14.30	0.35	61.5	13.24	LP 9-231
1248	GI 23	A	00 32 40	-03 52.1	F6 V	5.65	0.57	61.4	4.59	BS 142 ADS 490 V(AB) = 5.20 d(m) = 0.73, SBO
1249	GI 23	B	00 32 40	-03 52.1	G1 V	6.40		61.4	5.30	sep 0.3"
1250	GJ 1133		10 19 37	+63 42.6	DA7	14.71	0.38	61.4	13.65	LP 062-147
1251	GI 405		10 52 53	+56 18.0	M1.5	12.72	1.53	61.4	11.66	Ross 107
1252	NN 3836		14 13 23	+45 15.1	M2.5	11.60		61.3	10.50	LTT 14183 Ross 992
1253	GI 889.1		23 05 32	+03 03.3	dM0	10.91	1.52	61.3	9.85	AC+03:2781- 116
1254	GI 73		01 42 18	+16 06.0	M3	14.11	1.67	61.2	13.04	Wolf 1530
1255	GI 201		05 20 43	+17 16.7	dK5 e	7.95	1.09	61.2	6.88	
1256	GI 607		15 59 45	+30 19.0	M3	12.51	1.56	61.2	11.44	AC +30:35150
1257	GI 744		19 03 30	-37 53.0	G5 IV	6.15	0.71	61.2	5.08	
1258	GJ 1011		00 20 52	+24 01.5	k-m	14.27	1.59	61.1	13.20	
1259	GI 171.2	A	04 33 42	+27 02.0	dK5 ep	8.42	1.12	61.1	7.35	

1260	GI 171.2	B	04 33 39	+27 03.9	DC8	15.80	0.65	61.1	14.73	LP 358-525
1261	NN 3014	A	00 10 40	+80 23.2	M1.5	11.12	1.50	61.0	10.05	LTT 17095 AC+80:7
1262	NN 3015	B	00 10 48	+80 23.1	m	17.40		61.0	16.30	LP 12-304 sep 12.5" 127d (NLTT) d(R) = 4.2, d(pg) = 4.3
1263	NN 3105		01 37 24	+31 32.3	m	13.91		61.0	12.84	LTT 17245 V-R = 1.52 Weis
1264	NN 3121		01 48 56	+46 45.2	DA3	12.44	0.06	61.0	11.37	GD 279
1265	NN 3180		02 43 39	-05 10.3	m	15.86	1.50	61.0	14.79	
1266	NN 3243		03 38 00	-69 07.1	m	11.95		61.0	10.88	LTT 1735 LFT 302 L 91-140
1267	GI 152		03 42 18	-38 26.5	K0 V	6.99	0.88	61.0	5.92	
1268	GI 182		04 56 59	+01 42.6	dM0.5	10.09	1.39	61.0	9.02	AC+01:1951- 103
1269	GI 199	A	05 16 40	-21 26.7	K3/5 V	9.33	1.27	61.0	8.26	V(AB) = 9.31 d(m) = 4.2 , dM0 (Wilson)
1270	GI 199	B	05 16 40	-21 26.7		13.50		61.0	12.40	sep 4.1" 73d - 5.0" 75d (1930-59)
1271	NN 3370		05 51 34	+48 59.9	K2	7.83	1.07	61.0	6.76	
1272	NN 3389		06 11 41	-23 50.9	G5 V	6.38	0.72	61.0	5.31	BS 2225
1273	GI 231.1	A	06 14 37	+05 07.0	F9 V	5.70	0.60	61.0	4.63	
1274	GI 231.1	B	06 14 32	+05 08.1	m+	13.42	1.41	61.0	12.35	
1275	GJ 1114		08 48 57	+18 18.9	M2	11.54	1.48	61.0	10.47	Ross 622
1276	NN 3566		09 43 40	-04 12.0	m	14.15		61.0	13.08	

1277	Gl 414.1	A	11 08 35	+43 41.7	M3	11.47	1.49	61.0	10.40	AC+44:472-15 V(AB) = 10.88 d(m) = 0.35
1278	Gl 414.1	B	11 08 35	+43 41.7	M3	11.82	1.54	61.0	10.75	Kui 55 sep 3.76" 78d USNO 613/4
1279	NN 3748		12 44 45	+46 54.2	M2.5	11.76	1.50	61.0	10.69	LFT 941 LTT 13622 Ross 991
1280	NN 3758		12 57 30	-05 21.7	M3.5	12.54	1.56	61.0	11.50	LTT 4969 Ross 972
1281	Gl 508.2		13 18 38	+34 32.7	dM1	10.62	1.44	61.0	9.55	
1282	NN 3808		13 46 17	+04 21.1	m	14.34		61.0	13.27	LTT 14031 Wolf 1494
1283	Gl 530		13 48 35	-24 08.4	G5 V	6.44	0.69	61.0	5.37	dG5 (Wil)
1284	Gl 552.1		14 27 30	-53 52.6	k-m	11.63	1.51	61.0	10.56	L 260-093
1285	NN 3871		14 50 05	+12 36.0	k	11.61	1.52	61.0	10.50	LTT 14408 L 1198-31 LP 501-31
1286	NN 3929		15 56 27	+35 32.7	M6 :	12.69	1.59	61.0	11.62	
1287	Gl 626		16 25 32	+07 25.2	dK8	8.83	1.23	61.0	7.76	
1288	Gl 824		21 14 05	+09 11.1	dK8	7.95	1.02	61.0	6.88	
1289	Wo 9773		22 10 06	+08 18.8	M3	12.00	1.56	61.0	10.90	LTT 16502 LFT 1693 Wolf 1014
1290	Gl 98	A	02 25 09	+04 12.3	K7 V	9.36	1.39	60.9	8.28	ADS 1865 V (AB) = 8.69 d (m) = 0.18
1291	Gl 98	B	02 25 09	+04 12.3	K7 V	9.50		60.9	8.40	a = 0.545" P = 25.32 yr
1292	NN 3553		09 18 21	+03 35.8	m	13.33	1.60	60.8	12.25	LTT 12460 USNO 715
1293	Gl 387	A	10 14 30	+23 21.5	F8 Vbw	5.82	0.50	60.8	4.74	BS 4039 ADS 7712
1294	Gl 387	B	10 14 30	+23 21.5	M1	11.40		60.8	10.30	sep 7.4" 299d (1851-1958) d(m) = 6.0

1295	GI 859	A	22 23 52	-16 59.8	G3 V	6.21	0.62	60.8	5.13	V(AB) = 5.54 d(m) = 0.17 dG2 Wil
1296	GI 859	B	22 23 51	-16 59.8	G3 V	6.40		60.8	5.30	
1297	GI 508.1		13 17 47	-36 26.9	A2 V	2.75	0.04	60.6	1.66	IOT Cen
1298	GI 290		07 48 07	+80 23.7	G8 V	6.56	0.73	60.5	5.47	
1299	GI 632.1		16 34 52	+31 12.2	dK6	9.49	1.20	60.5	8.40	
1300	GI 641		16 50 27	+00 04.5	G8 V	6.64	0.76	60.5	5.55	
1301	GI 429	A	11 24 13	+03 17.1	K0 IV	6.50	0.80	60.4	5.41	
1302	GI 429	B	11 24 14	+03 16.7	K2 IV-V	7.58	1.00	60.4	6.49	
1303	GJ 2095		12 36 02	-49 32.5	DA6	13.96	0.18	60.4	12.87	
1304	NN 3937		16 01 40	-06 07.9	dM4.5-5	15.51	1.89	60.4	14.42	LP 684-17
1305	GI 786		20 12 24	+77 04.8	dM0	8.88	1.33	60.4	7.79	
1306	GI 270		07 16 15	+32 55.7	dM1.5	10.07	1.44	60.3	8.97	
1307	GI 621		16 21 32	-13 31.5	K3 V	8.40	0.96	60.2	7.30	
1308	GI 762		19 30 10	-62 56.9	m+	12.17	1.48	60.2	11.07	L 160-102
1309	GI 779		20 01 51	+16 56.0	G1 V	5.80	0.61	60.2	4.70	
1310	GJ 1025		00 58 20	-04 43.5		13.32	1.73	60.0	12.21	
1311	NN 3142		02 10 19	-00 13.8	m	13.50		60.0	12.40	
1312	GI 101		02 27 44	+57 09.5	M3.5	13.21	1.52	60.0	12.10	Ross 21
1313	GI 130		03 10 30	-38 17.2	M3	11.46	1.56	60.0	10.40	
1314	GI 140	A	03 21 09	+23 36.6	dM0	10.64	1.51	60.0	9.53	AC+23:368- 59 V(AB) = 10.38 d(m) = 1.4
1315	GI 140	B	03 21 09	+23 36.6		12.00		60.0	10.90	sep 1.6" 357d (1965)
1316	GI 140	C	03 21 16	+23 35.9	m	11.89	1.50	60.0	10.78	L 1307-14
1317	NN 3225		03 23 53	+19 04.3	m	14.96		60.0	13.85	LTT 11134
1318	NN 3286		04 23 19	-40 09.3	M3.5	14.10		60.0	13.00	LTT 1976 L 374-6

1319	NN 3317	S	wissenschaft in die schulen	04 48 04	-35 11.5	K2 V	7.45	0.90	60.0	6.34	V, B-V from CPC
1320	GJ 2040			05 16 57	+03 49.4	M0 V	9.86	1.42	60.0	8.80	AG+03: 619
1321	G1 264			07 02 18	-43 29.5	K5 V	8.68	1.18	60.0	7.57	
1322	NN 3491			08 14 45	+31 17.0	k	11.22	1.49	60.0	10.10	LTT 18046
1323	NN 3514			08 44 22	+61 20.5	m	15.17	1.82	60.0	14.10	LP 90-39
1324	NN 3523			08 56 23	-15 56.5	F6 V	5.83	0.53	60.0	4.72	LTT 3317
1325	NN 3528			08 59 37	+08 40.1	k	11.75	1.45	60.0	10.64	LTT 12371
1326	NN 3630			10 49 31	+00 48.6	m	13.85		60.0	12.74	LTT 12899
1327	NN 3659			11 21 29	-18 05.3	M3	13.05		60.0	11.94	LTT 4217 L 755-53 LP 792-20
1328	NN 3672			11 32 33	-05 22.0	m	15.10		60.0	14.00	LP 673-13
1329	NN 3681			11 39 28	+15 03.0	M3.5	12.58	1.48	60.0	11.50	LTT 13214 Ross 115
1330	NN 3692			11 50 45	-31 07.1	M4	13.61	1.70	60.0	12.50	LTT 4414 L 541-21 LP 907-40
1331	NN 3731	A		12 27 22	-05 10.6	M3.5	13.00		60.0	11.90	LTT 4740 L 903-4A LP 675-76
1332	NN 3732	B		12 27 22	-05 10.6	M3.5:	14.25		60.0	13.14	LTT 4741 L 903-4B LP 675-77 sep 8" 62d
1333	G1 486.1			12 46 21	+25 06.8	G7 V	6.31	0.70	60.0	5.20	
1334	NN 3762			13 04 24	+31 08.0	m	15.48	1.86	60.0	14.40	LP 322-628 San 214
1335	NN 3786			13 24 33	-30 55.0	M4	13.60		60.0	12.50	LTT 5190 L 546-85 LP 911-13
1336	GJ 1175			13 38 10	-34 12.6	K1 V	6.98	0.86	60.0	5.87	LTT 5300
1337	G1 531			13 49 27	-50 40.5	K1 V	7.38	0.90	60.0	6.27	

1338	NN 3878	A	14 54 11	+18 06.6	M5	15.50		60.0	14.40	LP 441-33 Mv: G&L ApJ 305, 784
1339	NN 3879	B	14 54 12	+18 06.8	M7 :	18.60		60.0	17.50	LP 441-34 sep 9" 48d Mv: G&L ApJ 305, 784
1340	GJ 2112	AB	15 19 11	-27 39.5	M3 :	13.28	1.70	60.0	12.20	LTT 6133 LP 915-27 L 623-94
1341	GJ 606.2		15 59 08	+33 27.2	G0 V	5.41	0.60	60.0	4.30	RHO Crb
1342	NN 3960		16 30 29	+09 56.6	m	13.05	1.66	60.0	11.94	
1343	NN 4003		17 19 47	+21 28.4	m	13.84		60.0	12.73	
1344	NN 4013		17 34 52	-29 59.1	k-m	10.94	1.47	60.0	9.80	LP 920-69 BPM 62452
1345	GJ 754.2		19 17 53	+37 14.4	G8 V	6.31	0.68	60.0	5.20	
1346	NN 4113		19 31 56	+39 25.3	M2.5	11.70		60.0	10.59	LTT 15711 Ross 1063
1347	NN 4132		20 01 19	-08 16.1	k-m	13.40		60.0	12.30	LP 694-16
1348	NN 4202		21 31 10	-07 04.2	M3.5	14.01	1.58	60.0	12.90	LTT 8582 Wolf 923
1349	NN 4226		21 48 25	-10 16.4	G0	7.50		60.0	6.39	
1350	NN 4267		22 13 59	+65 58.3	m	12.90		60.0	11.79	
1351	GJ 913		23 56 07	+46 27.0	dM0.5	9.62	1.44	60.0	8.51	
1352	GJ 1294	A	23 59 34	-68 33.4	M0 V	9.66	1.39	60.0	8.55	LTT 9859 L 86-80 CP- 68:3594 V (AB) = 9.30 d (m) = 1.0
1353	GJ 1294	B	23 59 34	-68 33.4		10.60		60.0	9.50	sep 1.5" 95d - 3.7" 120d (1912-1955)
1354	GJ 45		00 55 10	-62 31.0	K7 V	9.50	1.30	59.9	8.39	L 123-59 CD- 62:39 Sm 181

1355	Gl 781	wissenschaft in die schulen	20 03 55	+54 18.2	dM3 e	11.99	1.54	59.9	10.88	AC+55 50103
1356	Gl 143		03 26 08	-63 40.1	K5 V	8.00	1.12	59.8	6.90	
1357	Gl 219		05 46 06	-51 05.0	A5 V	3.85	0.17	59.8	2.73	BET Pic
1358	Gl 347	A	09 26 25	-07 08.5	M3.5	12.08	1.53	59.8	10.96	Ross 439
1359	Gl 347	B	09 26 28	-07 08.5	m	15.00	1.87	59.8	13.88	
1360	Gl 670	A	17 18 00	-21 03.7	F2 V	4.41	0.39	59.8	3.29	XI Oph V (AB) = 4.39 d (m) = 4.5
1361	Gl 670	B	17 18 00	-21 03.7	K3	8.90		59.8	7.80	sep 2.7" 66d - 3.7" 50d (1931-1959)
1362	Gl 692		17 40 26	-21 39.6	F5 V	4.87	0.47	59.8	3.75	
1363	GJ 1222		17 51 55	+07 23.5	m	13.11	1.55	59.8	11.99	
1364	Gl 777	A	20 01 34	+29 45.7	G8 IV-V	5.71	0.73	59.8	4.59	
1365	Gl 777	B	20 01 23	+29 43.9	M4 :	14.37	1.67	59.8	13.25	faint comp (?): Heintz AJ 96 : sep 4.4" 114d (1971.2) m = 15.5
1366	NN 4385		23 57 12	+47 29.2	m	16.10	1.87	59.8	14.98	USNO 786 LP 149-14
1367	Gl 265	A	07 02 35	+27 32.9	M0 Ve	10.22	1.32	59.7	9.10	
1368	Gl 713.1		18 24 53	-25 27.1	K1+ IIIb	2.82	1.04	59.7	1.70	LAM Sgr
1369	Gl 894.5		23 20 27	-11 02.5	K2 V	7.80	0.89	59.7	6.68	Viln 82 no 55
1370	Gl 584	A	15 21 08	+30 28.0	G2 V	5.62	0.58	59.6	4.50	ETA Crb ADS 9617 V (AB) = 5.02 d (m) = 0.34
1371	Gl 584	B	15 21 08	+30 28.0	G2 V	5.96		59.6	4.84	a = 0.907" P = 41.623 yr
1372	Gl 645		16 53 24	-36 58.7	M1	11.44	1.51	59.6	10.32	L 484-031
1373	Gl 746		19 05 43	+16 46.6	G5 V	6.07	0.70	59.5	4.94	
1374	GJ 1058		03 19 27	+02 46.4	m	14.78	1.76	59.4	13.65	
1375	Gl 147		03 34 19	+00 14.7	F8 V	4.28	0.57	59.4	3.15	
1376	Gl 304		08 19 41	-39 32.9	G6 V	7.17	0.71	59.4	6.04	

1377	GI 460		12 17 47	+26 16.7	F0 IV	6.15	0.30	59.4	5.02	
1378	GI 493		12 57 45	-02 26.1	dM0.5	9.78	1.20	59.4	8.65	
1379	GJ 1042		02 08 13	+39 41.6	DZ7	14.52	0.33	59.2	13.38	
1380	GI 704	A	18 05 08	+30 33.2	F7 V	5.09	0.50	59.2	3.95	
1381	GI 704	B	18 05 08	+30 33.2	K5 V	8.45	1.10	59.2	7.31	
1382	GI 168.2		04 19 18	+19 22.3	m	15.77	1.00	59.1	14.60	LOWNE 2 LP 415-26 ppm(NLTT)
1383	GI 274	A	07 25 54	+31 53.1	F0 V	4.18	0.32	59.1	3.04	RHO Gem
1384	GI 274	B	07 25 54	+31 53.1		12.50		59.1	11.40	
1385	NN 3029		00 19 15	-46 21.4	M3:	12.29	1.46	59.0	11.10	L 290-28 LTT 183 Sm 163 R-I = +1.42 Weistrop
1386	GI 57		01 19 16	-41 54.7	dM0.5	10.14	1.40	59.0	8.99	
1387	GJ 1038		01 22 43	-33 06.8	k-m	9.80	1.45	59.0	8.65	BPM 47129
1388	GI 80		01 51 52	+20 33.9	A5 V	2.64	0.13	59.0	1.49	BET Ari
1389	NN 3173		02 35 52	+06 24.8	DA8	15.09	0.44	59.0	13.94	PG WD0235 +064
1390	NN 3241		03 36 30	+24 48.2	dM3.1	12.79		59.0	11.64	LTT 11203 Wolf 1246
1391	NN 3328		05 03 24	+04 16.2	g	11.54	1.51	59.0	10.40	LTT 17742
1392	GJ 2039		05 07 58	+16 22.3	K0	8.55	1.12	59.0	7.40	Wolf 231
1393	GJ 1085		05 46 06	-04 06.4	G2 V	5.97	0.64	59.0	4.82	LTT 2380 BS2007
1394	GI 252		06 52 14	+25 26.4	G0 V	5.74	0.57	59.0	4.59	
1395	NN 3481	A	08 05 18	+21 15.3	K5	9.80	1.38	59.0	8.70	LTT 12130 V (AB) = 9.49 d (m) = 1.2
1396	NN 3482	B	08 05 18	+21 15.2	m	11.00		59.0	9.90	LTT 12131 sep 9" 157d
1397	NN 3545		09 15 22	-61 52.3	m	12.70		59.0	11.60	LTT 3423 L 140-119
1398	NN 3555		09 21 19	+00 21.4	M3:	11.54	1.51	59.0	10.40	LTT 12478 L 1038-40 LP 607-39

1399	GJ 2079	wissenschaft in die schulen	10 11 35	+21 19.7	dM0 e	10.20	1.36	59.0	9.05	AC+22:214-129
1400	NN 3599		10 22 44	+26 39.0	k-m	13.19	1.57	59.0	12.04	
1401	NN 3673		11 32 55	+39 12.3	m	13.11		59.0	11.96	
1402	NN 3684		11 44 23	+70 18.7	m	13.60		59.0	12.45	LP 38-393
1403	NN 3760		13 03 12	+37 24.3	M4	11.72		59.0	10.57	
1404	NN 3843		14 18 40	-00 53.1	M3	13.15	1.66	59.0	12.00	LFT 1096 LTT 5651 LP 620-3 L 980-5
1405	NN 3852		14 27 39	+42 01.2	G5 V	6.35	0.70	59.0	5.20	LTT 14271
1406	Gl 648		16 55 45	+65 12.7	F6 V	4.89	0.48	59.0	3.74	
1407	NN 3998		17 13 40	+11 07.0	M2.5	10.84	1.38	59.0	9.69	LTT 15111
1408	Gl 747.3		19 07 10	-47 14.0	K7 V	9.36	1.32	59.0	8.21	Sm 29 CD-47:12773
1409	Gl 768.1	A	19 48 38	+10 17.4	F8 V	5.11	0.55	59.0	3.96	OMI Aql ADS 13012AC ADS 13012B optical
1410	Gl 768.1	B	19 48 38	+10 17.4	M3	13.10		59.0	11.95	
1411	Gl 781.3		20 07 21	-21 55.4	DA6	14.44	0.19	59.0	13.30	LTT 7983 LP 870-43 L 710-30
1412	GJ 1251		20 21 33	-76 49.9	M4.5	13.82	1.74	59.0	12.67	
1413	NN 4176	A	20 59 13	+33 02.8	m	12.29		59.0	11.14	LTT 16147 L 1504-143 LP 340-547
1414	NN 4177	B	20 59 17	+33 02.7	m	13.12		59.0	11.97	LTT 16148 L 1504-142 LP 340-548 sep 57" 95d
1415	NN 4184		21 13 00	+25 35.4	m	12.13		59.0	10.98	LTT 16234 L 1433-38 LP 397-41

1416	NN 4219	S	21 45 00	+46 24.2	M3.5	13.36		59.0	12.21	LTT 16369 Wolf 944
1417	G1 849.1		22 07 13	-32 47.7	F6 V	4.92	0.48	59.0	3.77	TAU Psa
1418	NN 4282		22 30 44	-09 52.3	M3	12.41	1.57	59.0	11.26	Steph 2018
1419	NN 4381		23 55 18	+38 21.2	m	12.64		59.0	11.49	LP 291-34
1420	G1 580	A	15 11 20	-01 09.5	K0 V J	7.35	0.77	58.9	6.20	ADS 9544 V (AB) = 6.60 d (m) = 0.0
1421	G1 580	B	15 11 20	-01 09.5		7.35		58.9	6.20	sep 0.1" rapidly moving
1422	G1 604		15 54 16	-42 28.7	K5 V	8.05	1.12	58.9	6.90	
1423	G1 730		18 47 31	+03 02.1	dM1.5	10.74	1.47	58.9	9.59	AC+03:2528- 176
1424	G1 188	A	05 04 30	+18 34.8	G4 V	5.60	0.65	58.8	4.45	BS 1656 ADS 3701 V (AB) = 4.90 d (m) = 0.10
1425	G1 188	B	05 04 30	+18 34.8	G4 V	5.70		58.8	4.55	a = 0.10" P = 2.38 yr or a = 0.18" P = 1.19 yr
1426	NN 3289		04 23 43	+03 30.7	m	18.32		58.7	17.16	LP 535-12
1427	GJ 1216		17 19 26	+49 19.2	m	14.48	1.66	58.7	13.32	
1428	NN 3414		06 52 18	+55 02.9	k-m	11.80		58.6	10.60	
1429	G1 272		07 19 37	+46 11.3	dM2	10.53	1.46	58.6	9.37	AC+47:256- 150
1430	GJ 1102	A	07 47 33	+07 20.7	DC9	16.69	1.10	58.6	15.53	LP 543-33 USNOP
1431	GJ 1102	B	07 47 32	+07 20.9	DC9	16.98	1.30	58.6	15.82	LP 543-32
1432	G1 818		21 02 51	+06 52.6	K6 V	8.30	1.22	58.6	7.14	
1433	G1 886		22 59 15	-04 06.9	K4 V	7.46	0.95	58.6	6.30	
1434	G1 28		00 38 04	+39 55.3	K2 Ve	7.36	0.94	58.5	6.20	

1435	GJ 1026	A	01 00 32	+19 49.8	M1.5	11.88		58.5	10.72	LP 406-76 L 1229-11 LDS 873 V (AB) = 11.35 d(m) = 0.5 :
1436	GJ 1026	B	01 00 32	+19 49.8	M3.5	12.40		58.5	11.20	LP 406-77 sep 2" 28d (LHS)
1437	GJ 539		14 03 44	-36 07.5	K0- IIIb	2.06	1.01	58.5	0.90	THE Cen
1438	GJ 610		16 02 44	-20 18.6	K3/4 V	7.40	1.04	58.5	6.24	K3 Kui
1439	NN 4124		19 48 05	+32 27.2	M3	12.41	1.62	58.5	11.25	LTT 15792 LFT 1498 L 1501-39 LP 338-2
1440	GJ 391		10 23 24	-73 46.6	F2 IV	4.00	0.35	58.4	2.83	I Car
1441	GJ 882		22 55 00	+20 30.0	G4 V	5.50	0.67	58.4	4.33	
1442	GJ 900		23 32 26	+01 19.7	dM0.5	9.56	1.35	58.4	8.39	X-ray src: Fleming et al. 1988
1443	GJ 499	A	13 03 49	+20 59.7	dM0	9.44	1.29	58.3	8.27	V(AB) = 9.43 d(m) = 5.7
1444	GJ 499	B	13 03 49	+20 59.7		14.90		58.3	13.70	sep 0.8" 34d - 1.0" 337d (1902-1962)
1445	GJ 594		15 37 45	-44 29.8	F5 IV-V	4.64	0.40	58.3	3.47	
1446	GJ 700.1	A	18 00 21	-08 10.9	dF3 J	5.24	0.38	58.3	4.07	TAU Oph ADS 11005 V(AB) = 4.76 d(m) = 0.69
1447	GJ 700.1	B	18 00 21	-08 10.9		5.93		58.3	4.76	a = 1.494" P = 280.03 yr
1448	GJ 700.1	C	18 00 27	-08 11.9		9.40		58.3	8.20	sep(AB-C) 100.3" 127d; discrepant photometry
1449	GJ 131		03 12 35	-26 38.0	K7 V	9.15	1.24	58.2	7.97	
1450	GJ 340	A	09 14 56	+28 46.7	K3 V	7.86	1.00	58.2	6.68	ADS 7284 V (AB) = 7.21 d (m) = 0.22

1451	GI 340	B	09 14 56	+28 46.7	K3 V	8.10		58.2	6.90	a = 0.660 P = 34.20 yr
1452	GI 540		14 09 12	+80 50.4	M1 e	10.35	1.43	58.2	9.17	
1453	NN 3248		03 42 52	+73 23.6	m	11.31	1.54	58.1	10.13	LP 31-218
1454	GI 341.1		09 21 06	+80 48.2	K5	9.30	1.23	58.1	8.12	
1455	NN 3042		00 33 26	+45 14.5	M2	11.71	1.54	58.0	10.53	
1456	GI 60	A	01 32 42	-30 10.0	K3 V	7.78	0.92	58.0	6.60	V(ABC) = 7.10 AB: d (m) = 0.27
1457	GI 60	B	01 32 42	-30 10.0	K4 V	8.00		58.0	6.80	AB: a = 0.171" 4.559 yr
1458	GI 60	C	01 32 42	-30 10.0	M2 V	10.40		58.0	9.20	AB-C: a = 1.419" P = 111.8 yr d (m) = 3.19
1459	GI 67.1		01 39 09	-83 13.8	G2 V	5.88	0.61	58.0	4.70	
1460	NN 3129		02 00 01	+13 20.3	dM5 :	14.27		58.0	13.09	LTT 10691 L 1159-15 LP 469-73 Rob 100
1461	NN 3143		02 12 35	+33 44.1	m	13.58		58.0	12.40	LTT 17342
1462	GJ 1095		07 12 08	+47 19.9	G0 V	5.64	0.58	58.0	4.46	BS 2721
1463	NN 3478		08 02 57	+26 25.5	M0	10.21	1.46	58.0	9.03	Steph 681
1464	GJ 1108	A	08 05 46	+32 58.2	dM0.5e	10.05	1.35	58.0	8.87	AC +33:29235
1465	GJ 1108	B	08 05 45	+32 57.9	dM3 e	12.12	1.53	58.0	10.94	sep 12.3" 243d (GSC 1983.13)
1466	GI 312		08 35 31	-39 58.3	G4 IV-V	6.54	0.60	58.0	5.40	
1467	NN 3554		09 18 36	+43 43.3	m	14.02		58.0	12.84	
1468	GJ 2074		09 39 21	+07 11.0	DA7	14.90	0.30	58.0	13.72	PG197-4
1469	GJ 1132		10 12 54	-46 54.7	k	13.50	1.72	58.0	12.32	
1470	GJ 1145		11 14 40	-27 32.4	M0 V	9.79	1.40	58.0	8.61	LTT 4170

1471	NN 3698	A	11 58 09	-13 32.5	M3	12.74	1.55	58.0	11.60	LTT 4477 L 829-24 LP 734-11
1472	NN 3699	B	11 58 08	-13 32.5	m	15.00		58.0	14.00	LP 734-10 sep 7.5" 234d
1473	NN 3840		14 15 26	-00 17.5	k-m	12.76	1.59	58.0	11.60	LTT 5623 L 980-1 LP 619-64
1474	NN 3848		14 24 44	+24 01.3	DC8	15.41		58.0	14.23	WD1424 +240
1475	NN 3923		15 49 21	+29 40.4	M7	13.01	1.58	58.0	11.83	
1476	GJ 2121		16 27 24	-14 33.3	M3	12.32	1.52	58.0	11.10	LTT 6579
1477	Gl 719		18 32 45	+51 41.0	K6 Ve	8.10	1.22	58.0	6.90	BY DRA
1478	NN 4079		18 45 48	-62 07.0	M3	10.72	1.46	58.0	9.54	Sm 22 BPM 11774 = Sm 21 Smethells, IAU Coll. 76
1479	NN 4083		18 49 23	+47 54.8	m	12.53		58.0	11.35	
1480	GJ 1231		19 06 15	+26 30.6	m	15.16	1.91	58.0	13.98	
1481	NN 4105		19 10 40	+35 28.8	m	12.01	1.56	58.0	10.83	
1482	NN 4122		19 43 52	+32 15.7	M0	10.86		58.0	9.68	LTT 15769 L 1501-53 LP 337-3
1483	NN 4143		20 16 30	+15 41.0	m	11.79		58.0	10.61	LTT 15944 L 1286-87 LP 455-12
1484	NN 4200		21 28 54	-09 57.9	G0	7.41		58.0	6.23	
1485	NN 4261		22 07 56	+19 22.3	G0 V	6.18	0.69	58.0	5.00	
1486	GJ 1278		23 02 32	+66 29.7	dM1	9.89	1.40	58.0	8.71	
1487	NN 4317		23 10 51	-81 36.7	k-m	10.10		58.0	8.90	LFT 1773 LTT 9424 L 10-21
1488	GJ 2017		00 57 26	-25 51.6	G0	9.87	0.50	57.9	8.70	
1489	Gl 547		14 20 42	+01 28.5	G1 V	6.27	0.63	57.9	5.08	

1490	GJ 1209	wissenschaft in die schulen!	17 02 08	+17 00.9	m	12.28	1.55	57.9	11.09	
1491	Gl 820.1		21 05 12	-82 01.0	DA6	13.56	0.25	57.9	12.37	LTT 8381 L 24-52 BPM 1266
1492	Gl 181		04 55 00	+49 46.5	dM2 e	9.78	1.44	57.7	8.59	
1493	NN 3657		11 20 33	+26 10.4	m	15.14	1.84	57.7	13.95	LP 374-39 USNO 721
1494	Gl 702.1		18 03 01	-36 01.5	G5 V	5.95	0.62	57.7	4.76	
1495	GJ 1060	A	03 26 45	-27 29.3	DA5	14.00		57.6	12.80	LFT 286 LTT 1648 LP888-064
1496	GJ 1060	B	03 26 45	-27 29.4	sdM3	13.80		57.6	12.60	
1497	Gl 160		04 02 22	+21 52.5	G5 V	5.90	0.62	57.5	4.70	
1498	Gl 602		15 50 57	+42 35.4	F9 V	4.61	0.57	57.5	3.41	CHI Her
1499	Gl 657		17 08 34	-43 10.5	F0 IVn	3.33	0.41	57.5	2.13	ETA Sco
1500	Gl 817		21 02 09	-17 07.8	M2	11.46	1.47	57.5	10.26	Ross 769
1501	GJ 1024		00 53 58	+17 11.6	m	13.71	1.64	57.4	12.50	
1502	Gl 61		01 33 51	+41 09.4	F8 V	4.09	0.54	57.4	2.88	50 UPS And
1503	Gl 305		08 19 51	-76 45.7	F6 IV	4.07	0.40	57.4	2.86	ALF Cha
1504	Gl 322		08 47 34	+66 19.1	dM0	9.28	1.34	57.4	8.07	
1505	GJ 1051		02 41 22	-09 02.4	M2.5	11.92	1.46	57.3	10.70	Wolf 1132
1506	Gl 511.2		13 24 47	-15 42.9	K1 III	4.75	1.10	57.3	3.54	
1507	GJ 1211		17 05 37	+03 01.7	DZ7	15.19	0.46	57.3	13.98	
1508	Gl 404		10 51 12	-44 08.7	F8 IV-V	8.09	0.52	57.2	6.88	
1509	NN 4133		20 02 46	-11 05.4	DC9	16.87	1.04	57.2	15.66	LP 754-16
1510	Gl 501.2		13 09 15	-37 32.3	G3 V	4.85	0.70	57.1	3.63	
1511	NN 3082		01 12 30	-54 13.0	M3	11.09	1.48	57.0	9.87	LTT 692 L 221-60 Sm 184
1512	Gl 56.5		01 17 50	+76 27.0	dK0	7.11	0.82	57.0	5.89	
1513	NN 3113		01 44 06	-08 53.8	M3	12.99	1.58	57.0	11.77	LTT 952 L 870-44 LP 708-416
1514	Gl 81.2		01 54 52	-60 28.4	K5 V	8.60	1.16	57.0	7.38	

1515	NN 3207		03 09 38	-38 58.4	M3.5	11.51	1.51	57.0	10.30	LTT 1507 L 443-59 LP 994-72
1516	GJ 2037		04 53 42	-28 38.3	K3/4 V	8.13	1.07	57.0	6.91	LTT 2124
1517	GJ 1084		05 46 00	-48 32.2	M0 V	9.74	1.38	57.0	8.52	LTT 2379
1518	Gl 241		06 38 12	+24 00.6	dK6	8.13	1.02	57.0	6.91	
1519	NN 3572		09 52 45	+35 36.1	M4	12.73		57.0	11.51	LTT 12639 Wolf 330
1520	Gl 397.1	A	10 28 30	+57 22.2	dM0 e	9.65	1.38	57.0	8.43	
1521	Gl 397.1	B	10 28 17	+57 20.5	m	16.20		57.0	15.00	LP 92-176 sep. 142" 225d (NLTT) d (pg) = 5.2 d (R) = 4.8
1522	Gl 404.1		10 51 27	-58 35.2	K1 III	3.78	0.95	57.0	2.60	
1523	NN 3652		11 12 33	+19 44.0	m	12.89	1.58	57.0	11.67	LFT 778 LTT 13033 L 1259-11 LP 432-24
1524	NN 3740		12 39 15	-71 21.4	k-m	13.50		57.0	12.28	LTT 4846 L 68-30
1525	NN 3777		13 17 17	-35 08.0	M3.5	12.80		57.0	11.60	LTT 5131 L 473-1
1526	GJ 1172		13 31 49	+04 55.5	dM0.5	9.97	1.38	57.0	8.75	Wolf 1487
1527	NN 3812		13 48 43	+36 59.0	M3.5	13.65		57.0	12.43	LTT 14045 Ross 1019
1528	Gl 541.1		14 15 21	-07 18.5	G8 V	6.47	0.73	57.0	5.25	
1529	NN 3963		16 32 19	-27 11.3	m	14.20		57.0	13.00	LP 862-184
1530	Gl 638.1		16 45 16	-47 37.9	K0 V	7.38	0.91	57.0	6.16	
1531	Gl 649.1	A	16 56 30	+47 26.3	dK8 J	7.83	0.98	57.0	6.61	LTT 15019
1532	Gl 649.1	B	16 56 30	+47 26.3		11.19	1.47	57.0	9.97	
1533	Gl 649.1	C	16 56 19	+47 26.0	dK8	7.90	1.00	57.0	6.68	LTT 15017
1534	NN 4032		17 50 48	+16 55.8	m	12.69		57.0	11.47	LTT 15290 L 1279-70 LP 448-41

1535	NN 4110	S	wissenschaft in die schulen	19 24 36	+16 37.0	m	13.09		57.0	11.87	LTT 15678 L 1284-53 LP 452-10
1536	GJ 1240			19 29 20	-11 23.0	K2 V	7.57	0.92	57.0	6.35	LTT 7720
1537	NN 4117			19 33 41	+53 08.3	M3	12.20	1.64	57.0	11.00	LTT 15717 Wolf 1108
1538	NN 4178			20 59 43	-50 34.4	m	13.10		57.0	11.90	LTT 8344 L 280-19
1539	NN 4207			21 35 38	-33 52.8	M2	12.57	1.62	57.0	11.30	LTT 8614 L 570-29
1540	NN 4214	A		21 41 46	+16 49.7	m	13.65		57.0	12.43	
1541	NN 4215	B		21 41 45	+16 50.8	m	14.81		57.0	13.59	sep 63" 347d
1542	NN 4254			22 03 13	-12 08.9	K7	10.15	1.45	57.0	8.93	LTT 8848
1543	G1 143.2	A		03 28 30	-63 06.8	F5 IV-V	4.71	0.39	56.9	3.49	KAP Ret
1544	G1 143.2	B		03 28 36	-63 07.3	m	10.75	1.42	56.9	9.53	L 128-037
1545	G1 176.1			04 40 17	-37 14.5	F1 V	5.05	0.38	56.9	3.80	BET Cae
1546	G1 230			06 10 26	+10 38.7	G2 V	6.45	0.67	56.9	5.23	
1547	G1 552			14 27 11	+15 44.2	dM2.5	10.68	1.47	56.9	9.46	
1548	G1 54.2	A		01 11 53	-08 11.5	F5 V	5.14	0.45	56.8	3.91	
1549	G1 54.2	B		01 11 51	-08 10.7	K1 V	7.85	0.78	56.8	6.62	
1550	G1 574			14 59 42	-46 05.9	K5 V	9.86	1.20	56.8	8.63	
1551	G1 855			22 20 13	-57 28.1	M3	10.74	1.50	56.8	9.51	Sm 107
1552	G1 29			00 38 06	-59 44.1	G1 V	5.90	0.56	56.7	4.67	
1553	NN 3259			03 57 46	+08 06.0	DC9	15.87	0.69	56.7	14.64	LTT 11318
1554	G1 217			05 42 35	+37 16.4	K1 V	7.36	0.83	56.7	6.13	
1555	G1 430.1			11 29 08	+22 56.5	dM1 e	10.30	1.48	56.7	9.10	
1556	G1 758			19 21 41	+33 07.3	K0 V	6.37	0.81	56.7	5.14	
1557	GJ 1007			00 14 22	+04 51.3	m	13.79	1.62	56.6	12.55	LTT 10099
1558	G1 385			10 10 59	-84 52.4		10.22	0.34	56.6	9.00	discrepant photometry; ident??

1559	NN 3919	S	wissenschaft in die schulen!	15 47 46	+34 57.5	m	13.16	1.64	56.6	11.92	LTT 14695 L 1489-5 LP 274-8
1560	NN 4383			23 55 59	+07 23.1	M3	11.74	1.51	56.6	10.50	LTT 17066 USNO 785
1561	G1 258			06 59 07	+68 21.7	M3.5	11.96	1.53	56.5	10.70	AC+68:2911
1562	G1 275			07 26 11	-51 18.0	G5 IV-V	6.73	0.70	56.5	5.50	
1563	G1 459			12 12 58	+57 18.6	A3 V	3.30	0.08	56.5	2.06	DEL Uma
1564	GJ 1200			16 12 27	+19 13.3	m	12.92	1.54	56.5	11.68	
1565	G1 738	A		18 55 09	+32 50.2	F9 V	5.34	0.59	56.5	4.10	ADS 11871 V(AB) = 5.22 d(m) = 2.32
1566	G1 738	B		18 55 09	+32 50.2	K1 V	7.70		56.5	6.50	a = 1.24" P = 61.203 yr
1567	G1 825.4	A		21 16 52	-26 33.6	G5 V	6.63	0.73	56.5	5.39	
1568	G1 825.4	B		21 16 52	-26 33.6	dG6	9.60		56.5	8.40	
1569	G1 571			14 56 14	-43 53.5	K7 V	10.15	1.31	56.4	8.91	
1570	G1 576			15 02 27	+05 50.3	K5	9.82	1.31	56.4	8.58	
1571	G1 151			03 41 41	+18 17.7	DQ8	15.19	0.31	56.3	13.94	Wolf 219
1572	G1 321			08 41 53	+41 51.8	K3 V	8.58	0.94	56.3	7.33	
1573	GJ 1131			10 04 09	+69 29.4	m	14.34	1.75	56.3	13.09	
1574	G1 790			20 24 38	-31 01.6	G5 V	6.61	0.73	56.3	5.36	
1575	G1 811.1			20 54 04	-10 37.6	dM4	11.47	1.51	56.3	10.22	AC-11:2439- 179
1576	G1 209			05 34 04	+20 42.4	G4 IV-V	7.67	0.66	56.2	6.40	
1577	G1 724			18 38 08	-13 25.1	M0	10.63	1.50	56.2	9.38	
1578	G1 857			22 21 38	-58 02.8	G4 V	5.32	0.67	56.2	4.07	
1579	G1 155			03 44 42	-23 23.8	F3 III	4.22	0.42	56.1	2.96	27 TAU(6) Eri
1580	G1 582.1	A		15 19 08	-47 44.4	G5 V J	8.29	0.70	56.1	7.00	V(AB) = 7.68 d(m) = 0.3
1581	G1 582.1	B		15 19 08	-47 44.4		8.60		56.1	7.30	sep 1.4" 217d - 0.7" 77d (1895- 1960)

1582	GI 629	wissenschaft in die schulen!	16 28 08	-38 54.1	K0 V	7.24	0.86	56.1	5.98	
1583	NN 4327		23 15 00	+37 56.6	m	11.46	1.54	56.1	10.20	
1584	GI 895.4		23 28 56	+58 53.3	K0 V	6.74	0.83	56.1	5.48	LTT 16916
1585	NN 3017		00 13 06	-30 02.7	dM3.4	14.31	1.57	56.0	13.05	GR 4
1586	GI 56.4		01 16 43	+79 53.5	dK8	9.66	1.29	56.0	8.40	
1587	NN 3114		01 45 17	+20 57.7	M3	12.16	1.58	56.0	10.90	LTT 10622 Wolf 87
1588	NN 3120		01 48 38	+21 09.1	M4	13.90		56.0	12.64	LTT 10640 Wolf 90
1589	NN 3141		02 10 02	-63 28.0	m	12.25		56.0	10.99	LTT 1137 LFT 188 L 125-51
1590	NN 3160		02 26 12	+11 52.0	M1	12.01	1.57	56.0	10.75	Rob 140
1591	GI 249		06 47 49	+47 26.2	dK6	8.99	1.24	56.0	7.73	
1592	GI 254		06 53 52	+30 49.6	K7	9.72	1.36	56.0	8.46	
1593	NN 3425		07 02 46	+67 16.8	dM0	11.18	1.51	56.0	9.92	LTT 11972 AC+67:2334
1594	GI 337.1		09 10 25	+61 37.9	F9 V	5.13	0.58	56.0	3.87	
1595	NN 3582		09 59 59	+15 13.9	m	14.23	1.70	56.0	13.00	LTT 12689
1596	GJ 1136	A	10 39 35	-36 22.2	K7 V	10.19	1.46	56.0	8.93	LDS 314 BPM 54256
1597	GJ 1136	B	10 39 35	-36 22.2		11.67	1.52	56.0	10.41	BPM 54257
1598	NN 3634		10 56 14	-30 52.5	m	11.95		56.0	10.69	LP 905-36
1599	GI 418		11 10 39	+04 45.3	K5 V	8.69	1.18	56.0	7.43	
1600	NN 3696		11 55 43	+42 51.5	m	14.08		56.0	12.82	
1601	GJ 1168		13 10 41	+20 27.2	dM	13.02	1.58	56.0	11.76	LTT 13826 LP 378-774 San 241
1602	NN 3791		13 31 40	-26 06.6	m	14.00		56.0	12.70	LP 855-34
1603	NN 3918		15 47 38	+01 06.6	m	12.45		56.0	11.19	LTT 14694 Wolf 587

1604	NN 3961	S	16 30 50	-53 28.7	m	12.00		56.0	10.70	LTT 6608 L 266-166
1605	GJ 696		17 47 53	-06 02.1	dM1.5	10.17	1.43	56.0	8.91	
1606	GJ 2133		17 50 48	-34 39.0	k	13.52	1.64	56.0	12.30	LTT 7123
1607	NN 4041		18 02 32	+35 57.4	M0	10.83	1.48	56.0	9.57	
1608	NN 4145		20 17 27	-51 57.0	M0	10.20	1.41	56.0	8.94	Sm 52
1609	NN 4296		22 45 19	+44 17.4	F8	9.60		56.0	8.30	
1610	GJ 904.1	A	23 38 19	+20 05.3	K2	8.32	1.11	56.0	7.06	ADS 16923 V(AB) = 8.27 d(m) = 3.4
1611	GJ 904.1	B	23 38 19	+20 05.3		11.70		56.0	10.40	sep 0.9" 184d - 0.7" 236d (1888- 1954)
1612	NN 4378	A	23 54 46	-13 15.5	M4	12.93		56.0	11.67	LP 704-15
1613	NN 4379	B	23 54 45	-13 15.4	M4	12.98		56.0	11.72	LP 704-14 sep 20" 294d
1614	GJ 1109		08 16 41	-36 30.2	A7 III	4.45	0.22	55.8	3.18	BS 3270
1615	NN 4241		21 54 56	+07 53.8	M1	11.01	1.50	55.7	9.74	LTT 16412 Wolf 953
1616	GJ 1241		19 35 10	+27 36.4	DAV5	12.98	0.17	55.6	11.71	
1617	GJ 905.2	A	23 41 23	+32 19.0	dM5	11.67	1.56	55.6	10.40	AC +32:86422
1618	GJ 905.2	B	23 41 21	+32 16.2	DA4	12.90	0.15	55.6	11.63	LTT 16991 LP 347-415 L 1512-34B AC+32 86401 PG
1619	GJ 409		10 59 29	-17 41.2		11.87	0.61	55.5	10.59	AC- 17:31766
1620	GJ 463		12 20 45	+64 18.2	M3	11.58	1.45	55.5	10.30	AC +64:14332
1621	GJ 906		23 43 18	+35 58.6	dM0	9.90	1.35	55.5	8.62	AC +36:64438
1622	GJ 84.2	A	02 03 48	+44 57.2	dM0	10.28	1.49	55.3	8.99	

1623	GI 84.2	wissenschaft in die schulen	02 03 48	+44 57.2		14.20		55.3	12.90	sep 4.4" 307d (1959) but no comp. in NLTT etc. ??
1624	GI 105.1		02 34 54	-34 47.5	G5 IV	5.78	0.65	55.2	4.49	LAM(2) For
1625	GI 159		04 00 03	-00 24.2	F6 V	5.37	0.50	55.2	4.08	
1626	NN 3398		06 33 20	+11 40.1	k-m	14.22	1.65	55.1	12.93	USNO 705
1627	GI 683		17 33 59	-54 28.2	A7 V	5.25	0.20	55.1	3.96	PI Ara
1628	NN 3006		00 03 40	-66 07.5	M4	12.16	1.55	55.0	10.86	LFT 12 LTT 38 L 86-21 Sm 153
1629	NN 3032		00 20 50	-51 10.3	M4	11.88	1.48	55.0	10.58	LTT 197 LFT 39
1630	NN 3051		00 41 42	+12 20.8	m	12.79	1.49	55.0	11.49	LP 465-77 LTT 10259
1631	GI 34.1		00 46 21	+16 40.3	F8 V	5.07	0.51	55.0	3.77	
1632	GI 58.2		01 26 20	+21 28.0	K2 V	7.73	0.96	55.0	6.43	
1633	GJ 2030	A	03 20 51	-07 58.1	G2 V	6.19	0.71	55.0	4.89	LTT 1601
1634	GJ 2030	B	03 20 51	-07 58.1		12.30		55.0	11.00	
1635	NN 3227		03 25 49	+26 19.0	m	13.40		55.0	12.10	LP 356-106
1636	GI 143.1		03 26 57	-11 50.7	M0 V	9.98	1.42	55.0	8.68	
1637	NN 3258		03 54 22	-25 19.3	G8 V	6.88		55.0	5.58	LTT 1829
1638	NN 3293		04 26 31	-25 16.4	M2.5	12.00		55.0	10.70	LTT 1993 L 591-6 LP 834-42
1639	NN 3307		04 38 06	+02 08.2	M0	11.24	1.47	55.0	9.94	Steph 502
1640	GJ 1079		05 24 22	-32 32.7	K2/3 V	7.74	0.94	55.0	6.44	LTT 2265
1641	NN 3388		06 10 06	+51 41.1	m	12.86		55.0	11.56	
1642	GI 262		07 00 20	+29 25.4	G4 V	5.94	0.60	55.0	4.64	
1643	GI 275.1		07 26 52	+68 43.7	dM0	10.89	1.43	55.0	9.59	AC+68:3124

1644	NN 3444	S	wissenschaft in die schulen	07 27 48	+58 02.0	M6 :	17.40		55.0	16.10	LP 88-196 Mv = 16.1 +- .9 G&L ApJ 305, 784
1645	GJ 1098			07 28 49	+64 16.1	DC9	16.38	0.91	55.0	15.08	LP 58-247
1646	NN 3453			07 31 39	+22 26.9	k	11.53	1.50	55.0	10.20	LP 365-24
1647	NN 3485			08 08 16	+04 07.8	m	13.51		55.0	12.21	LTT 12143
1648	GI 306			08 22 05	-03 35.3	F3 V	5.61	0.46	55.0	4.31	
1649	GJ 1120	A		08 58 31	+15 28.0	K5	9.43	1.30	55.0	8.13	ADS 7139 V (AB) = 8.71 d (m) = 0.1
1650	GJ 1120	B		08 58 31	+15 27.9	K5	9.49		55.0	8.19	LTT 12364 sep 4.1" 210d - 5.2" 189d (1830- 1955)
1651	NN 3590			10 12 15	+31 40.2	m	13.60		55.0	12.30	
1652	GI 389	A		10 20 37	-59 55.1	M3	10.72	1.43	55.0	9.42	L 190-266 sep 12" 23d
1653	GI 389	B		10 20 37	-59 54.9	m	12.63	1.49	55.0	11.33	L 190-265
1654	NN 3605			10 26 00	+00 14.9	DA	13.83		55.0	12.53	PG WD1026 +002
1655	NN 3643			11 03 04	+10 31.0	M3.5	12.40		55.0	11.10	LTT 12978 L 1187-43 LP 491-60
1656	NN 3759			12 58 16	-62 55.3	dM2	10.95		55.0	9.65	LTT 4974 LFT 963 L 147-101 BPM 7973
1657	NN 3822			13 59 54	+13 55.9	dM0.5	10.65	1.47	55.0	9.35	
1658	NN 3838			14 14 39	+10 49.5	M2	11.52	1.52	55.0	10.22	LTT 14191 L 1196-39 LP 499-59
1659	NN 3968			16 39 02	+36 24.6	M2	11.50	1.50	55.0	10.20	LTT 14949 Ross 812
1660	GI 654.3			17 04 36	-41 39.3	K5 V	8.29	1.05	55.0	6.99	

1661	GI 697		17 51 22	+21 20.0	dK5	8.48	0.95	55.0	7.18	
1662	NN 4068		18 39 36	+80 02.5	M4 e	13.22	1.72	55.0	11.90	LP 25-02
1663	NN 4099		19 07 39	+39 07.5	M0	11.33	1.53	55.0	10.03	Steph 1680
1664	GI 778		20 01 47	+23 12.7	K1 V	7.26	0.82	55.0	5.96	
1665	NN 4135		20 04 25	+52 49.4	m	13.16		55.0	11.86	LTT 15891 Wolf 1131
1666	GI 794.2		20 35 55	-60 43.1	F8 V	5.12	0.53	55.0	3.82	PHI(2) Pav
1667	NN 4165		20 47 10	+37 16.9	DA4	12.93	0.14	55.0	11.63	LTT 16093 L 1576-43 LP 284-13
1668	Wo 9732		21 15 54	-67 51.9	m	10.90	1.45	55.0	9.60	LTT 8456 L 117-123 AC- 68:3972-162
1669	GI 851.2		22 11 36	-41 37.2	G5 V	6.23	0.65	55.0	4.93	
1670	NN 4380		23 55 11	+19 29.9	m	13.01		55.0	11.71	
1671	GJ 1199		16 09 06	+13 30.4	DA6	15.09	0.23	54.9	13.79	
1672	GI 694.1	A	17 42 49	+72 10.4	F5 IV-V	4.58	0.42	54.9	3.28	PSI Dra
1673	GI 694.1	B	17 42 51	+72 10.9	F8 V	5.79	0.53	54.9	4.49	
1674	GI 711		18 18 43	-02 54.8	K0 III-IV	3.26	0.94	54.9	1.96	ETA Ser
1675	GI 81	A	01 54 01	-51 51.4	G5 IV	3.70	0.85	54.8	2.39	BS 566 CHI Eri
1676	GI 81	B	01 54 01	-51 51.4		10.70		54.8	9.40	sep 5.0" 202d (1947) d (m) = 6.5
1677	GI 94		02 16 00	+35 07.7	M3.5	12.55	1.47	54.8	11.24	Ross 19
1678	NN 3221		03 20 39	+11 30.7	m	12.19	1.56	54.8	10.88	LTT 11117
1679	GI 158		03 59 53	+35 09.3	K1 V	8.51	0.87	54.8	7.20	LTT 11321
1680	GJ 1074		04 54 50	+50 52.4	M1	10.98	1.48	54.8	9.67	
1681	GI 301	A	08 10 50	-13 45.5	M0 V	9.74	1.41	54.8	8.43	ADS 6664 V (AB) = 9.38 d (m) = 0.44
1682	GI 301	B	08 10 50	-13 45.5		10.70		54.8	9.40	a = 0.815" P = 64.65 yr
1683	GI 416		11 09 01	-14 42.7	K4 V	9.05	1.21	54.8	7.74	

1684	GI 471.2		12 29 29	-15 55.2	F0 IV	4.30	0.37	54.8	2.99	ETA Crv
1685	GI 634		16 37 56	-43 53.0	M3	11.57	1.55	54.8	10.26	
1686	GI 679		17 30 13	+34 18.3	G5 V	6.56	0.65	54.8	5.25	
1687	GI 30		00 40 52	+33 34.6	dK5	8.73	1.12	54.7	7.42	
1688	GI 239.1		06 34 30	-19 12.7	K1 III	3.96	1.05	54.7	2.65	NU Cma
1689	NN 3723		12 22 25	-03 56.7	G5	8.10		54.7	6.80	LTT 4689
1690	NN 3410		06 44 47	+02 34.4	DA8	15.68	0.32	54.6	14.37	
1691	GI 609.2		16 01 59	+25 22.9	G8 V	7.10	0.77	54.6	5.79	
1692	GI 31		00 41 05	-18 15.6	K1 IIIe	2.04	1.01	54.5	0.72	BET Cet
1693	GJ 1107		08 02 29	+34 13.4	dM0 p	10.14	1.35	54.5	8.82	
1694	NN 3768		13 09 59	+85 18.6	DC9	16.00	0.78	54.5	14.68	LP 7-226 LP 8-46
1695	GI 21		00 24 00	+69 52.1	dM0	10.52	1.49	54.4	9.20	AC+69:173
1696	GJ 1225		18 17 33	+68 32.8	m	15.39	1.88	54.3	14.06	
1697	GI 740.1		19 00 10	-00 47.0	dG5	8.43	0.73	54.3	7.10	
1698	GI 379	A	10 06 24	+75 23.0	dK6 eJ	10.18	1.40	54.2	8.85	V(AB) = 9.48 d(m) = 0.24
1699	GI 379	B	10 06 24	+75 23.0		10.30		54.2	9.00	a = 1.625" P = 192 yr Heintz AJ 94, 1077 (1987)
1700	GI 560	A	14 38 26	-64 45.5	F0 Vp	3.19	0.24	54.2	1.86	ALF Cir
1701	GI 560	B	14 38 26	-64 45.5	K5 V	8.47	1.15	54.2	7.14	
1702	NN 4225		21 46 02	+27 42.3	m	11.99	1.62	54.2	10.66	
1703	GI 207		05 29 53	+29 21.4	K7	12.07	1.46	54.1	10.70	AC +29:13493
1704	GI 284		07 41 24	-45 02.7	G6 IV	5.06	0.77	54.1	3.73	
1705	GJ 1124		09 19 17	+40 25.2	K2 V	7.63	0.99	54.1	6.30	
1706	GI 488.1		12 50 40	-39 54.4	A7 III	4.26	0.21	54.1	2.90	
1707	GI 543		14 16 36	-07 03.8	M3	13.40	1.64	54.1	12.07	Wolf 534
1708	GI 626.1		16 25 43	-78 47.3	K0 IV	3.89	0.91	54.1	2.60	GAM Aps

1709	GJ 1018	wissenschaft in die schulen	00 39 53	-36 59.5	m	12.65	1.54	54.0	11.31	BPM 46562 LP 937-95
1710	NN 3056		00 44 40	-23 46.8	m	14.40		54.0	13.06	
1711	NN 3058		00 46 10	+44 18.5	m	13.06		54.0	11.72	LP 193-584
1712	GJ 1039		01 23 02	-26 16.0	DC7	14.95	0.40	54.0	13.61	
1713	NN 3103		01 35 54	+00 23.7	k	11.55		54.0	10.21	
1714	GI 106		02 40 30	+19 13.1	dK4	8.28	1.07	54.0	6.94	
1715	NN 3209		03 11 14	+48 20.3	M1	11.43	1.49	54.0	10.10	LTT 11051 Ross 346
1716	NN 3242		03 36 35	+25 19.4	M3.5	12.70		54.0	11.36	LTT 11204 Wolf 204 cpm to Woolley 9120 !
1717	NN 3271		04 15 31	+75 01.8	M3	12.16	1.51	54.0	10.80	LTT 11395 SA 3-112
1718	NN 3327		05 02 53	-12 04.3	M4 e	12.97		54.0	11.63	LP 716-35
1719	GI 257.1		06 57 49	+48 27.4	K3 V	8.00	0.99	54.0	6.66	
1720	NN 3479		08 03 33	+36 54.6	m	12.95		54.0	11.61	LTT 18035
1721	NN 3495		08 19 50	+31 44.8	G5	8.11		54.0	6.77	
1722	GI 323	A	08 48 02	+08 03.1	dM0 pJ	9.77	1.36	54.0	8.43	ADS 7044 V (AB) = 9.07 d (m) = 0.1
1723	GI 323	B	08 48 02	+08 03.1		9.90		54.0	8.60	sep 1.9" 84d - 2.6" 121d (1912-65)
1724	NN 3530		09 02 29	+03 02.0	m	11.61		54.0	10.27	LTT 12385 L 1036-8 LP 546-48
1725	GI 335	A	09 06 01	+67 20.4	F7 IV-V	4.84	0.49	54.0	3.50	ADS 7203 13 SIG(2) UMa V(AB) = 4.81 d(m) = 3.65

1726	GI 335	B	09 06 01	+67 20.4	K2 V	8.44		54.0	7.10	a = 6.20" P = 1067.1 yr
1727	GI 344	A	09 25 18	-05 51.1	G2 V J	5.80	0.65	54.0	4.46	BS 3750 V (AB) = 5.38 d (m) = 0.8 , SBO (A&A 195,129)
1728	GI 344	B	09 25 18	-05 51.1		6.60		54.0	5.30	sep 0.2" 319d - 0.4" 153d (1938- 60)
1729	NN 3558		09 26 53	+39 50.7	m	12.13		54.0	10.79	LP 211-12
1730	NN 3568		09 44 53	+13 10.4	m	13.38		54.0	12.04	LP 488-37
1731	GI 412.3		11 05 43	-27 59.8	K7 V	9.33	1.25	54.0	7.99	
1732	GJ 1146		11 19 06	+06 26.1	k-m	13.58	1.64	54.0	12.24	
1733	GI 446		11 44 45	-30 00.3	G5 V	6.48	0.68	54.0	5.14	
1734	NN 3691		11 50 24	+24 45.3	m	14.60		54.0	13.26	
1735	GI 458.2		12 12 41	+49 00.7	M2 V	10.52	1.46	54.0	9.18	
1736	GJ 1163		12 41 09	+25 22.8	dM4	12.96	1.63	54.0	11.62	LTT 18236 San 128
1737	NN 3750		12 46 05	+58 36.8	DC8 :	15.56		54.0	14.22	WD1246 +586
1738	NN 3776		13 16 33	+33 42.1	K1 V	8.13	1.14	54.0	6.80	
1739	NN 3859		14 31 05	+81 01.9	G5	6.91	0.76	54.0	5.57	
1740	NN 3891		15 04 28	+55 16.1	m	13.35		54.0	12.01	LP 135-97
1741	GI 579.4		15 10 33	-25 07.3	G5 V	6.45	0.70	54.0	5.11	
1742	GI 583		15 19 27	-04 35.9	K7 V	9.47	1.33	54.0	8.13	
1743	GI 683.2	A	17 34 26	-37 49.8	G8 V	6.80	0.77	54.0	5.46	V(AB) = 6.68 d(m) = 2.3
1744	GI 683.2	B	17 34 26	-37 49.8		9.10		54.0	7.80	sep 1.4" 106d (1959)
1745	NN 4022		17 39 13	-40 59.9	M3	12.55		54.0	11.21	LTT 7044 L 414-103

1746	NN 4027	S	17 46 13	+36 07.9	G5	7.62		54.0	6.28	
1747	GI 747.4		19 08 19	-55 57.0	k-m	11.31	1.45	54.0	9.97	Sm 31
1748	GJ 1233		19 11 16	+57 34.8	G8 V	7.04	0.79	54.0	5.70	
1749	GI 765	A	19 35 06	+50 06.3	F4 V	4.48	0.38	54.0	3.14	THE Cyg ADS 12695
1750	GI 765	B	19 35 06	+50 06.3		13.00		54.0	11.70	
1751	NN 4134		20 02 53	+54 19.5	dK0	7.72	0.94	54.0	6.38	
1752	NN 4318		23 10 54	-70 19.9	G5 V	6.90		54.0	5.56	CD-70:1916
1753	NN 4358		23 37 44	+60 24.9	M2	11.41	1.57	54.0	10.07	
1754	NN 4370		23 49 12	+06 41.8	m	12.73		54.0	11.39	LTT 17035
1755	NN 4386		23 57 12	-44 21.0	M7	12.82	1.64	54.0	11.48	LTT 9828 LP 988-175 L 433-153 BPM 45308 Sm 148
1756	GJ 1186		14 51 13	+11 47.0	m	15.29	1.82	53.9	13.95	
1757	GI 848.4		22 06 52	-07 47.3	G8 IV	6.55	0.75	53.9	5.20	
1758	GI 474		12 31 20	+33 39.6	K0 III	6.24	1.05	53.8	4.89	
1759	GI 725.3		18 44 39	-50 45.4	G3 V	8.70	0.65	53.8	7.35	
1760	GJ 1070		04 19 08	+38 54.2	k-m	15.27	1.71	53.7	13.92	
1761	GI 385.1		10 11 12	-32 47.1	G1 V	6.38	0.59	53.7	5.03	
1762	GI 412.1		11 04 29	-62 09.2	G8 III	4.62	1.03	53.7	3.27	
1763	GI 690	A	17 39 18	+71 21.2	dM0	9.20	1.10	53.7	7.85	comp B optical
1764	NN 4294		22 43 47	-06 54.8	m	15.98	1.83	53.7	14.63	LP 701-7 USNO 777
1765	GI 156.1	A	03 52 55	+53 25.3	dM1.5e	10.86	1.43	53.6	9.51	LTT 11297 Ross 23 AC +53:2250-45 comp Wor 5 prob. optical
1766	NN 3420		06 57 36	+32 02.5	DC9	16.57	0.96	53.6	15.22	LP 308-010

1767	Wo 9342	S	wissenschaft in die schulen!	10 55 28	+48 33.6	dM0	10.52	1.37	53.6	9.17	
1768	GJ 564.1			14 48 06	-15 50.1	A3 IV	2.75	0.15	53.6	1.40	
1769	GJ 828.2			21 24 38	-07 03.4	M0	11.10	1.55	53.6	9.75	AC-07:388-38
1770	GJ 1003			00 04 46	+28 58.8	m	14.18	1.49	53.5	12.82	
1771	GJ 38			00 48 23	+58 01.5	dM2	10.67	1.39	53.5	9.31	AC+57:5559 Wolf 33
1772	GJ 816.2	A		21 01 34	-20 03.2	A5 V	5.10	0.17	53.5	3.70	ETA Cap V (AB) = 4.84 d (m) = 1.4
1773	GJ 816.2	B		21 01 34	-20 03.2		6.50		53.5	5.10	sep 0.370" 134.8d (1985.49)
1774	GJ 78.1			01 50 13	+29 20.2	F6 IV	3.42	0.48	53.4	2.06	ALF Tri
1775	Wo 9490	A		14 40 16	+19 41.5	K5	9.74	1.29	53.4	8.38	ADS 9352 LTT 14351 V (AB) = 9.12 d (m) = 0.28
1776	Wo 9490	B		14 40 16	+19 41.5		10.00		53.4	8.60	a = 0.624" P = 51.337 yr
1777	Wo 9490	C		14 40 09	+19 43.1	K5	10.08	1.34	53.4	8.72	LTT 14350 sep (AB-C) 135" 309d (NLTT)
1778	GJ 1023	A		00 51 05	+68 46.6	G0	9.70	0.55	53.3	8.30	ADS 737
1779	GJ 1023	B		00 51 07	+68 46.6		10.40	0.64	53.3	9.00	
1780	GJ 128	A		03 10 13	-01 22.9	F8 V	5.06	0.57	53.3	3.69	ADS 2406
1781	GJ 128	B		03 10 13	-01 22.9		11.50		53.3	10.10	sep 3.3" 231d (1958)
1782	GJ 822	A		21 12 03	+09 48.2	F7 V	5.11	0.50	53.3	3.74	BS 8123 ADS 14773 DEL Equ V (AB) = 4.49 d (m) = 0.29
1783	GJ 822	B		21 12 03	+09 48.2	F7 V	5.40		53.3	4.00	a = 0.26" P = 5.70 yr
1784	GJ 464.1			12 22 01	+31 33.4	G6 IV	8.78	0.74	53.2	7.40	

1785	GI 509	A	13 21 14	+29 29.7	dM0	9.52	1.33	53.2	8.15	ADS 8887 V (AB) = 8.87 d (m) = 0.31
1786	GI 509	B	13 21 14	+29 29.7	dK6	9.80		53.2	8.40	a = 2.14" P = 229.0 yr
1787	NN 3913		15 33 37	+22 19.1	k-m	12.69	1.51	53.2	11.32	LTT 14636 L 1344-37 LP 384-18
1788	GI 708.2		18 13 45	+13 54.1	dM0	10.20	1.44	53.2	8.83	
1789	GI 204.2		05 27 23	-03 28.4	M3.5	12.02	1.53	53.1	10.65	Wolf 1450
1790	NN 3621		10 44 38	+21 45.7	K5	10.13	1.22	53.1	8.76	LTT 12876
1791	GI 741		19 00 29	-13 38.1	M4 :	14.85	1.56	53.1	13.48	L 850-062
1792	GI 842.2		21 57 58	+75 20.9	dM1	10.56	1.45	53.1	9.19	AC+75:8347
1793	GI 3		00 02 48	-68 06.2	K5 V	8.48	1.06	53.0	7.10	
1794	GI 17.3		00 20 18	-12 29.2	G2 V	6.38	0.66	53.0	5.00	BS 88
1795	NN 3033		00 21 55	+29 45.8	m	14.54	1.67	53.0	13.16	
1796	NN 3034		00 22 45	+22 37.0	m	14.30		53.0	12.90	LTT 10142 L 1298-103 LP 349-18
1797	NN 3047		00 38 16	+31 06.8	m	13.83		53.0	12.45	
1798	GI 55.1	A	01 13 19	-69 05.1	K2 V	7.80	0.98	53.0	6.42	V(AB) = 7.24 d(m) = 0.43 cpm with GI 55.3
1799	GI 55.1	B	01 13 19	-69 05.1		8.20		53.0	6.80	a = 1.078" P = 81.29 yr
1800	GI 59.1		01 30 55	+68 41.5	G6 V	6.53	0.68	53.0	5.15	
1801	NN 3109		01 40 34	-53 59.4	F8 V	5.52	0.53	53.0	4.14	BS 506
1802	NN 3177		02 42 11	-36 31.1	G5 V	7.12		53.0	5.74	
1803	GI 118.2	A	02 52 41	+26 40.4	dK2	7.60	0.93	53.0	6.22	
1804	NN 3190		02 56 00	+36 25.0	M3.5	13.04	1.52	53.0	11.70	Ross 331
1805	NN 3205		03 07 37	+05 43.6	dM4	11.88		53.0	10.50	

1806	GJ 1066		03 54 53	-41 29.3	K4 V	8.94	1.21	53.0	7.56	
1807	NN 3313		04 44 36	+02 04.3	k	11.34	1.48	53.0	10.00	LTT 17686
1808	GJ 1082		05 32 48	+41 28.2	DA7	14.75	0.32	53.0	13.37	GD 69
1809	NN 3413		06 49 36	+18 20.0	m	13.18		53.0	11.80	LTT 11938 L 1246-11 LP 421-7
1810	GJ 1106		07 55 54	-33 49.2	K5 V	8.84	1.16	53.0	7.46	LTT 3008
1811	GJ 296		07 58 15	-39 53.5	K7 V	9.66	1.34	53.0	8.28	
1812	NN 3477		08 02 37	+56 02.4	M0	11.48	1.49	53.0	10.10	LP 123-75
1813	GJ 297.1		08 08 11	-61 09.0	F5 V	4.76	0.43	53.0	3.38	B CAR
1814	NN 3488		08 11 51	+13 10.5	K4	8.85	1.20	53.0	7.47	LTT 12158 Ross 620
1815	GJ 333.1		08 58 11	-58 53.5	F3 V	5.16	0.42	53.0	3.78	
1816	GJ 354.1	A	09 29 50	+27 12.8	dG9	7.01	0.77	53.0	5.63	
1817	GJ 354.1	B	09 29 54	+27 13.2	m	16.50		53.0	15.10	LP 314-20 sep 65" 67d (NLTT)
1818	GJ 378.2		10 04 22	+03 12.6	dM0 e	9.95	1.39	53.0	8.57	
1819	GJ 396		10 28 15	+84 39.4	K0	7.30	0.82	53.0	5.92	
1820	GJ 1144		11 13 52	-14 25.1	K7 V	10.00	1.40	53.0	8.62	LTT 4164 U263
1821	NN 3682		11 40 48	+25 34.9	m	13.83		53.0	12.45	LTT 13220 L 1405-42 LP 375-25
1822	NN 3769		13 10 10	-02 00.0	K0	7.56		53.0	6.18	
1823	NN 3796		13 36 20	-02 00.5	M3	12.12	1.58	53.0	10.70	LTT 5282 Ross 488
1824	NN 3816		13 53 32	-27 49.1	m	15.30		53.0	13.90	LP 912-32
1825	NN 3924		15 50 52	+13 21.1	G1 V	6.10	0.60	53.0	4.72	LTT 14713
1826	GJ 1202		16 29 22	+17 40.9	k-m	12.78	1.57	53.0	11.40	
1827	NN 4002		17 16 10	+18 12.2	m	13.02		53.0	11.64	LTT 15124 L 1277-48 LP 447-38

1828	NN 4005		17 21 39	-04 19.1	M2	12.19	1.51	53.0	10.81	LTT 6924 L 989-38 LP 687-31
1829	NN 4007		17 24 11	-25 06.7	M3.5	13.35		53.0	11.97	LTT 6936 L 630-44 LP 864-1
1830	NN 4036		17 53 48	-41 59.0	M3	11.36	1.51	53.0	9.98	LTT 7138 L 415-82 Sm 5
1831	GI 700.2		18 00 29	+26 19.2	K0 V	6.99	0.80	53.0	5.61	
1832	GJ 2139		18 40 12	-11 11.7	DA5	14.18	0.15	53.0	12.80	LTT 7421
1833	GI 776		20 00 34	-67 27.2	G2 V	6.08	0.65	53.0	4.70	
1834	GI 808.2		20 48 04	+29 11.9	K5 V	8.41	1.06	53.0	7.03	
1835	NN 4182		21 08 47	+29 13.3	M1	11.05	1.34	53.0	9.67	LTT 16206 Ross 824
1836	NN 4197		21 25 28	-22 31.4	M4	12.21	1.56	53.0	10.83	LTT 8526 L 714-46 LP 873-4
1837	NN 4210		21 37 40	+27 23.3	M3:	11.62		53.0	10.24	LTT 16329 L 1434-37 LP 342-8
1838	NN 4213		21 41 45	+06 24.8	dM3	12.07	1.53	53.0	10.70	Rob 526
1839	NN 4222		21 45 44	-63 21.3	m+	12.50		53.0	11.10	LTT 8706 L 165-102
1840	NN 4257		22 04 13	+03 10.7	M4	13.60	1.60	53.0	12.22	LTT 16471 Wolf 990
1841	NN 4273		22 18 00	-65 46.0	M5	11.98	1.56	53.0	10.60	LTT 8978 L 119-33 BPM 14722 Sm 105 R-I = 1.27 Weistrop
1842	GJ 2157		23 37 12	+58 41.6	K0 V	7.45	0.86	53.0	6.07	AG+58: 157
1843	GI 902.1		23 37 13	-33 01.0	K1 V	7.19	0.81	53.0	5.81	
1844	NN 4362		23 46 02	-27 56.1	M3.5:	12.40		53.0	11.00	LFT 1827 LTT 9718 L 649-24 LP 935-18
1845	GI 67.2		01 39 28	-45 40.3	G5 V	9.30	0.69	52.9	7.92	
1846	GI 196		05 14 17	+79 10.7	F6 V	5.05	0.47	52.9	3.67	

1847	GI 293.1	A	07 55 25	-00 40.7	K5 V	8.06	1.04	52.9	6.68	ADS 6487 V (AB) = 8.05 d (m) = 5.3
1848	GI 293.1	B	07 55 25	-00 40.7		13.30		52.9	11.90	sep 2.0" 93d to 4.1" 69d (1908-56)
1849	NN 3570		09 50 04	+03 22.0	K4	10.58	1.40	52.7	9.19	AC+03:2399- 47 VV230
1850	GJ 2102		13 31 05	+08 50.5	K0	7.98	1.00	52.7	6.59	
1851	GI 724.1		18 39 48	-50 12.8	G5 V	9.32	0.68	52.7	7.93	
1852	GI 112		02 43 20	+25 26.5	K1 IV	7.88	0.84	52.6	6.48	
1853	GI 544	A	14 17 00	-04 55.2	K1 V	7.58	0.84	52.6	6.18	
1854	GI 544	B	14 17 00	-04 55.2	M4	15.10		52.6	13.70	
1855	GI 561		14 41 09	+26 57.7	dK0	9.67	0.73	52.6	8.30	
1856	GI 828.1		21 24 11	+03 31.2	dM1	10.52	1.38	52.6	9.12	AC+03:2561- 36
1857	GJ 1271		22 40 08	+17 24.0	M3	11.78	1.56	52.6	10.38	
1858	GJ 1273		22 46 39	+22 20.5	DA5	14.36	0.19	52.6	12.96	LTT 18580 PG
1859	GI 764.1	A	19 34 02	-10 33.1	K2 V	8.58	1.01	52.5	7.18	ADS 12664 V(AB) = 8.36 d(m) = 1.6
1860	GI 764.1	B	19 34 02	-10 33.1	K7	10.20		52.5	8.80	sep 2.8" 340d - 5.0" 328d (1832- 1959)
1861	GI 170.1		04 27 42	+16 05.2	A6 IV	4.78	0.17	52.3	3.37	
1862	GJ 1080		05 25 38	+02 56.7	M5 V	12.80	1.60	52.3	11.39	or: B-V = 1.46, U-B = 0.86
1863	GI 268.2		07 12 42	-63 15.9	K5 V	9.10	1.25	52.3	7.69	
1864	GI 416.1		11 09 12	-22 33.1	A2 III	4.48	0.03	52.3	3.10	BET Crt
1865	GI 639		16 46 50	+37 06.3	K7 V	8.41	0.82	52.3	7.00	
1866	GI 836.8		21 42 30	+41 22.0	dK6	9.63	1.34	52.3	8.22	
1867	GI 220		05 50 10	+24 15.4	M1.5	10.81	1.48	52.2	9.40	AC+24:147- 263 Ross 59 LFT 437

1868	GI 503	AB	13 11 08	-58 50.2	F7 IV	4.92	0.48	52.2	3.51	BS 4989 Cp-58:4740 sep 2.7" d(m) = 5.3, B optical ?
1869	GI 187.1		05 02 30	-42 25.8	K0	10.04	0.74	52.1	8.62	
1870	NN 3406	A	06 39 54	+51 12.1	M3.5 J	12.44	1.59	52.1	11.02	LP 121-41 L 1750-12 USNO 706 V (AB) = 12.34 d(m) = 2.5
1871	NN 3407	B	06 39 54	+51 12.1		14.90		52.1	13.50	sep 1.8"
1872	GI 791.1	A	20 26 01	-17 58.8	F2 IV	4.78	0.38	52.1	3.36	RHO Cap ADS 13887AB V (AB) = 4.78 d(m) = 5.2
1873	GI 791.1	B	20 26 01	-17 58.8		10.00		52.1	8.60	sep 0.5" 158d (1958), optical?
1874	GI 836.9	A	21 43 02	-57 55.3	K7 V	9.47	1.32	52.1	8.05	CD-58:8156 Sm 88 Fin 283 V(AB) = 8.79 d(m) = 0.15
1875	GI 836.9	B	21 43 02	-57 55.3	K7 V	9.60		52.1	8.20	a = 0.205" P = 6.25 yr
1876	NN 3021		00 13 56	-80 07.7	G6 V	6.60		52.0	5.20	LTT 127 CD-80:9
1877	NN 3027		00 16 16	+27 32.3	m	13.86		52.0	12.44	LTT 10112 LP 292-66
1878	GI 18		00 21 53	-27 18.3	K3 V	7.92	0.95	52.0	6.50	
1879	GJ 1032		01 06 47	-24 57.4	dM2	12.38	1.53	52.0	10.96	PS 130 LP 826-605 TS 335
1880	NN 3108		01 40 25	+27 35.5	K7	10.40	1.46	52.0	8.98	LTT 10602
1881	NN 3157		02 22 33	+37 19.1	m	14.05		52.0	12.63	LTT 17364

1882	NN 3186	S	02 49 28	+26 46.4	dM0	11.11	1.49	52.0	9.69	LTT 10935 L 1378-25 LP 354-423
1883	Gl 118.2	B	02 52 41	+26 40.4	dM0	9.80	1.40	52.0	8.38	
1884	Gl 118.2	C	02 52 38	+26 40.3	m	13.86	1.58	52.0	12.44	L 1378-026
1885	Gl 161		04 04 23	+69 24.8	dK2	7.70	0.91	52.0	6.28	
1886	NN 3284		04 22 58	+15 24.3	dM0	12.13	1.40	52.0	10.70	VA366 GH7- 208
1887	NN 3312		04 42 56	+42 15.5	G0	6.52		52.0	5.10	
1888	NN 3344		05 16 50	-72 17.6	m	11.70	1.40	52.0	10.28	LTT 2235 L 57-44
1889	NN 3395		06 27 08	+50 05.0	M0	11.09	1.50	52.0	9.67	Steph 598
1890	Gl 316		08 37 32	-06 17.7	dM0	9.90	1.39	52.0	8.48	
1891	Gl 334.2		09 05 47	+34 05.2	F9 V	5.93	0.60	52.0	4.51	
1892	NN 3546		09 15 25	+27 31.2	K5	9.55	1.34	52.0	8.13	Steph 762
1893	Gl 355		09 30 01	-10 57.8	K0	7.82	0.92	52.0	6.40	pit Heintz AJ 101
1894	Gl 366.1	A	09 41 58	-27 32.4	F6 V	5.45	0.51	52.0	4.03	THE Ant V (AB) = 4.79 d (m) = 0.2
1895	Gl 366.1	B	09 41 58	-27 32.4	F8 V	5.60		52.0	4.20	a = 0.134" P = 18.32 yr
1896	NN 3604		10 25 53	+32 29.6	m	13.00		52.0	11.58	
1897	Gl 456.1	A	12 07 20	-45 55.7	K5 V	8.45	1.14	52.0	7.03	
1898	Gl 456.1	B	12 07 23	-45 54.8	m	13.25	1.56	52.0	11.83	L 326-041
1899	NN 3747		12 44 37	-03 17.9	M3	12.63	1.54	52.0	11.20	LTT 4891 L 976-35 LP 616-13
1900	NN 3757		12 56 55	+08 00.1	m+	16.00		52.0	14.60	LP 556-64
1901	NN 3765		13 06 45	+49 20.8	M0	11.04	1.54	52.0	9.62	Steph 1049
1902	Gl 517		13 32 07	-08 05.1	K5	9.31	1.21	52.0	7.89	EQ Vir
1903	Wo 9472		14 10 53	-06 43.6	dM0	10.16	1.43	52.0	8.74	LTT 5574

1904	GI 541.2	wissenschaft in die schulen!	14 15 29	+45 40.5	dM0 p	10.25	1.44	52.0	8.83	
1905	NN 3990		17 07 34	+11 59.3	m	13.99		52.0	12.57	LTT 15079 L 1205-52 LP 507-5
1906	NN 4059		18 24 04	+11 19.3	m	12.85		52.0	11.43	LTT 15455 L 1208-222 LP 510-10
1907	NN 4104		19 09 32	-39 07.2	M3	12.70		52.0	11.30	LTT 7605 L 491-42
1908	NN 4130		19 58 34	+22 34.6	G5	7.67		52.0	6.25	LTT 15851
1909	NN 4160	A	20 42 05	+08 43.0	k-m	11.27		52.0	9.85	LTT 16064 L 1143-65 LP 576-40
1910	NN 4161	B	20 42 04	+08 43.2	m	12.54		52.0	11.12	LTT 16065 L 1143-66 LP 576-39 sep 15" 345d
1911	GI 806.1	A	20 44 11	+33 46.9	K0- III	2.45	1.03	52.0	1.03	EPS Cyg
1912	GI 806.1	B	20 44 05	+33 46.8	M4	13.40	1.66	52.0	11.98	
1913	NN 4172		20 56 23	-33 48.6	K0 V	7.35	0.84	52.0	5.93	
1914	NN 4211		21 38 41	-01 00.2	m	12.57	1.56	52.0	11.20	LTT 8642 L 1002-29 LP 638-23
1915	NN 4240		21 54 17	+19 32.3	M3.5	12.90	1.58	52.0	11.50	LTT 16410 Ross 263
1916	NN 4300		22 48 22	+28 20.3	m	12.55		52.0	11.13	LP 344-047
1917	NN 4371		23 49 48	-14 57.9	m	15.50		52.0	14.10	LP 823-8
1918	GI 910		23 50 36	+28 44.4	dM0 e	9.74	1.39	52.0	8.32	
1919	GJ 1019		00 40 56	+28 11.1	m	14.52	1.59	51.9	13.10	
1920	GI 392	A	10 24 59	+49 03.2	F9 V	6.44	0.60	51.9	5.02	
1921	GI 392	B	10 24 59	+49 03.2		12.50		51.9	11.10	
1922	GI 852.1		22 14 53	+15 06.6	m	13.55	1.54	51.9	12.10	MWC 412- 76 SA 90: 166
1923	GI 122		03 03 15	+75 51.8	dM0	9.82	1.38	51.8	8.39	AC+75:1146

1924	Gl 153	A	03 43 04	+68 30.9	K7	9.33	1.28	51.8	7.90	LTT 11249 sep (A-BC) 17.0" 16d (1934)
1925	Gl 153	B	03 43 05	+68 31.2	M2.5 J	11.30	1.54	51.8	9.87	LTT 11250 AC+68:1482 V(BC) = 10.69 d(m) = 0.3
1926	Gl 153	C	03 43 05	+68 31.2		11.60		51.8	10.20	a = 0.67" P = 57.7 yr
1927	NN 3311		04 42 28	+48 40.0	m	17.29		51.8	15.86	LP 157-25 V- I = 3.79 (USNO), wrong chart in LHS
1928	Gl 513		13 26 52	+11 42.9	M5	12.13	1.46	51.8	10.70	L 1194-026
1929	Gl 615.1	A	16 10 58	+13 39.6	G8 V	7.36	0.76	51.8	5.93	ADS 9969 V (AB) = 6.68 d (m) = 0.15
1930	Gl 615.1	B	16 10 58	+13 39.6	G8 V	7.50		51.8	6.10	
1931	Gl 155.3		03 51 31	-37 11.9	M2.5	12.14	1.45	51.7	10.71	
1932	Gl 167.2		04 15 03	-26 10.6	M0	11.80	1.38	51.7	10.37	LP 834-41 L 590-10
1933	Gl 501	A	13 07 33	+17 47.6	F5 V	4.98	0.45	51.7	3.55	ADS 8804 42 ALF Com V(AB) = 4.32 d(m) = 0.19
1934	Gl 501	B	13 07 33	+17 47.6	F5 V	5.17		51.7	3.74	a = 0.662" P 25.87 yr
1935	Gl 455.2		12 04 15	-64 20.1	F2 III	4.15	0.34	51.6	2.71	ETA Cru
1936	Gl 571.1		14 58 01	-10 55.9	dM0.5	9.48	1.40	51.6	8.04	LTT 5983
1937	Gl 580.1		15 13 35	-58 37.0	A3 V	4.07	0.09	51.6	2.60	BET Cir
1938	Gl 629.3		16 32 33	-49 11.2	M1 :	12.38	1.48	51.6	10.90	L 339-106
1939	Gl 705.1		18 05 47	-62 00.9	G3 IV-V	5.48	0.58	51.6	4.04	IOT Pav
1940	Gl 773.4		19 57 07	-33 50.3	F8 V	5.66	0.49	51.6	4.22	
1941	Wo 9126		03 41 21	+24 43.1	K2	8.85	1.71	51.5	7.40	HZ 316 TR109 no member

1942	NN 3441	S	07 24 31	+22 08.9	m	11.23	1.49	51.5	9.79	LTT 12020 Ross 878
1943	Gl 295		07 57 27	+29 22.0	G8 V	7.00	0.71	51.5	5.56	
1944	Gl 296.1		08 04 58	-29 15.2	G4 IV-V	6.80	0.60	51.5	5.36	
1945	Gl 835.1		21 36 00	-77 36.8	K0 III	3.75	1.00	51.5	2.31	NU Oct
1946	Gl 16.1		00 16 07	-08 19.7	G5 IV-V	6.46	0.68	51.4	5.00	
1947	Gl 822.1	A	21 12 48	+37 49.9	F0 IV	3.82	0.38	51.4	2.37	TAU Cyg
1948	Gl 822.1	B	21 12 48	+37 49.9	G0 V	6.42	0.60	51.4	4.97	
1949	Gl 822.1	C	21 12 47	+37 48.4	M3	12.00	1.53	51.4	10.55	L 1577-019
1950	NN 4328		23 15 00	+09 25.2	dK8	9.72	1.13	51.4	8.27	
1951	Gl 143.3		03 28 59	+14 09.7	sdM3	12.27	1.55	51.3	10.82	
1952	Gl 690.1		17 39 39	-16 36.5	M2.5	13.05	1.55	51.3	11.60	L 774-022
1953	Wo 9775		22 11 46	-08 59.1	K2	11.85		51.3	10.40	LTT 8920 LFT 1697 Wolf 1332
1954	Gl 874		22 45 25	-37 03.0	M3	11.92	1.48	51.3	10.47	L 501-038
1955	Gl 293.2		07 55 57	-25 29.2	K3 V	8.42	1.05	51.2	6.97	
1956	Gl 788.1		20 18 35	-58 26.4	m	10.59	1.46	51.2	9.14	Sm 54
1957	Gl 429.3		11 27 28	-51 23.3	F6 V	7.38	0.41	51.1	5.92	
1958	NN 3907		15 27 58	+43 03.5	m	14.17	1.73	51.1	12.71	double?? phot. cat.
1959	Gl 656.1	A	17 07 30	-15 39.9	A1 V	3.02	0.06	51.1	1.56	ETA Oph BS 6378 ADS 10374 V (AB) = 2.43 d (m) = 0.36
1960	Gl 656.1	BC	17 07 30	-15 39.9	A3 V	3.40		51.1	1.90	Comp C : V = 12.34, B-V = 0.83, U-B = 0.25 Woolley
1961	Gl 793.1		20 31 06	+41 43.2	G9 V	7.09	0.79	51.1	5.63	
1962	NN 3004		00 02 43	+48 12.0	G5	8.30		51.0	6.84	
1963	NN 3023		00 14 41	+28 54.0	M2	11.55		51.0	10.09	LTT 10100 LFT 29 Ross 680

1964	GI 31.4	wissenschaft in die schulen	00 42 31	+01 31.2	K2 V	8.01	1.00	51.0	6.55	
1965	NN 3098		01 30 05	-22 09.0	M1.5	11.21	1.50	51.0	9.75	LTT 838 LFT 138 L 654-28
1966	NN 3101		01 33 42	-27 02.0	m	13.33		51.0	11.87	PS 244
1967	GI 82.1		01 56 10	+32 58.3	dG7	7.14	0.78	51.0	5.68	
1968	Wo 9163	AB	04 38 06	-09 17.3	dM0	10.97	1.48	51.0	9.51	Wor 17 sep 2" d(m) = 0.1 , V(AB) = 10.27
1969	NN 3321		04 59 12	+03 41.7	M1	11.28	1.52	51.0	9.82	Steph 539
1970	NN 3353	A	05 31 30	+10 17.5	M3	12.32		51.0	10.86	LTT 11678 Ross 45
1971	NN 3354	B	05 31 30	+10 17.4	M3.5	13.62		51.0	12.16	LTT 11679 sep 6" 191d
1972	NN 3383		06 01 25	+18 41.9	G5	7.98		51.0	6.52	
1973	NN 3419		06 56 53	-10 11.2	m	13.50		51.0	12.00	LTT 2704 L 814-1 LP 721-2
1974	NN 3560		09 31 26	+61 28.0	M3	11.95	1.54	51.0	10.49	Steph 785
1975	NN 3600	A	10 22 57	+50 42.6	k-m	13.52		51.0	12.06	LP 127-371
1976	NN 3601	B	10 22 58	+50 42.8	m	13.68		51.0	12.22	LP 127-372 sep 16" 26d
1977	GI 397.2		10 29 25	-53 27.7	F6 V	4.89	0.50	51.0	3.43	
1978	GI 403.1		10 51 03	-19 52.1	F6 V	5.23	0.46	51.0	3.77	
1979	NN 3639		11 00 24	+36 55.3	m	13.67		51.0	12.21	LP 263-64
1980	GJ 1143	A	11 12 21	-22 49.6	K4 V	8.98	1.14	51.0	7.52	LTT 4150 DON 466A
1981	GJ 1143	B	11 12 21	-22 49.6		13.50		51.0	12.00	DON 466B
1982	NN 3677	AB	11 36 08	-12 55.6	F7 V	5.48	0.52	51.0	4.02	BS 4488 d (m) = 5.4 sep 1.4"
1983	NN 3719		12 14 28	+31 26.1	dM4-5e	14.15	1.62	51.0	12.69	San 39

1984	NN 3744		12 40 59	+78 09.4	m	15.84	1.86	51.0	14.40	LP 20-375
1985	NN 3802		13 40 33	+09 19.6	m	13.09		51.0	11.63	LTT 18350
1986	NN 3821		13 59 41	-20 45.9	M3.5	13.19	1.61	51.0	11.70	LTT 5475 L 691-8 LP 799-14
1987	NN 3830		14 10 10	-03 04.9	K1	7.03	0.74	51.0	5.57	LTT 5565
1988	NN 3858		14 30 32	+49 52.4	m	13.26		51.0	11.80	LP 174-355
1989	NN 3899		15 14 42	+03 21.4	DA wk	14.02		51.0	12.56	WD1514 +033
1990	NN 3911		15 32 02	+46 24.9	m	13.58		51.0	12.12	LP 176-55
1991	GI 639.2		16 47 00	-64 21.2	g	11.00	0.72	51.0	9.50	AC-64:N301- 65
1992	GI 654.1		17 02 44	+00 46.5	F9 V	6.00	0.58	51.0	4.54	
1993	NN 4001		17 15 45	-01 43.7	K7	10.59	1.44	51.0	9.13	BPM 78873
1994	GI 689		17 37 02	+71 54.4	dK8	8.62	1.10	51.0	7.16	
1995	NN 4017		17 37 14	+68 46.9	F5 V	4.80	0.43	51.0	3.34	LTT 15238
1996	GI 751		19 13 14	+24 48.3	dM0	9.72	1.35	51.0	8.26	
1997	NN 4119		19 39 19	-45 11.8	M1	10.01	1.34	51.0	8.55	LTT 7786 CFS 18799 CP-45:9776 Sm 42
1998	NN 4126		19 49 43	+11 30.2	G0 V	6.13	0.65	51.0	4.67	LTT 15805
1999	GI 773.6		19 58 50	-50 11.2	K5 V	8.66	1.12	51.0	7.20	optical double
2000	GI 779.1		20 02 04	+25 38.9	K3 V	7.88	0.91	51.0	6.42	
2001	GI 783.2	A	20 08 50	+16 02.0	K1 V	7.33	0.85	51.0	5.87	
2002	GI 783.2	B	20 08 57	+16 01.8	dM	13.94	1.62	51.0	12.48	
2003	NN 4151		20 33 51	+59 07.1	m	13.43		51.0	11.97	LTT 16016 Wolf 1074
2004	NN 4236		21 51 32	-01 31.2	DA6	14.41	0.26	51.0	12.95	LTT 8747 L 1003-16

2005	GI 850	wissenschaft in die schulen	22 09 01	+36 00.8	K0	7.24	0.79	51.0	5.78	
2006	NN 4310		23 00 27	-49 59.7	M3	10.64	1.41	51.0	9.18	BPM 28112 Sm 122
2007	NN 4324		23 14 25	+52 56.6	F7 V	5.54	0.52	51.0	4.08	LTT 16841
2008	GI 894.2	A	23 16 29	-13 43.9	G5 IV	5.20	0.79	51.0	3.70	Viln 82 no 43
2009	GI 894.2	B	23 16 29	-13 43.6	K2 V	7.61	0.91	51.0	6.15	Viln 82 no 44
2010	GJ 2155		23 23 39	+08 37.0	K7	10.54	1.50	51.0	9.08	LTT 16892 Rob 367
2011	NN 4347		23 33 37	-48 51.9	M0	10.09	1.37	51.0	8.63	CD- 49:14193 CFS 20397 Sm 139 BPM 45047
2012	NN 4348		23 33 37	-48 51.9		12.37	1.44	51.0	10.91	BPM 45048 sep 25" 150d Reid MN 201, 51 (1982)
2013	GI 91.3		02 13 46	+42 44.6	DC9	16.20	0.72	50.9	14.73	
2014	GI 165.1		04 11 20	+58 24.0	K3	8.67	1.00	50.9	7.20	
2015	GI 248		06 47 41	-61 53.2	A7 IV	3.27	0.21	50.9	1.80	ALF Pic
2016	GI 388.1		10 17 01	+19 43.5	F6 IV	4.81	0.45	50.9	3.30	
2017	GI 629.2	A	16 32 05	-04 07.0	G5 Ve	9.62	0.74	50.9	8.15	LFT 1290 LTT 6621
2018	GI 755.1		19 19 23	+14 34.9	DA5	13.01	0.06	50.9	11.54	BPM 94172 GD 219
2019	GJ 1261		21 17 23	+53 59.8	DA	12.33	0.07	50.9	10.86	
2020	NN 3016		00 11 42	-13 27.1	DC8	15.90	0.58	50.8	14.43	LP 704-001
2021	GI 46.1		00 57 36	+17 55.8	G5	7.33	1.07	50.8	5.90	probably no dwarf
2022	GI 221		05 50 34	-06 00.0	M0 V	9.70	1.33	50.8	8.23	
2023	NN 3504		08 29 58	-01 24.0	m	18.44		50.8	16.97	LP 605-23
2024	GJ 1219		17 25 27	+14 31.8	m	13.69	1.76	50.8	12.22	
2025	GI 705.2		18 06 48	+52 47.4	K5	12.51	1.50	50.8	11.00	Wolf 1409

2026	Gl 55.3	A	01 14 05	-69 08.5	F6 IV J	4.99	0.47	50.7	3.50	BS 377 KAP (2) Tuc V (AB) = 4.86 d (m) = 2.2 , cpm with Gl 55.1
2027	Gl 55.3	B	01 14 04	-69 08.4	G5	7.20		50.7	5.70	KAP(1) Tuc sep 5.5" 335d
2028	Gl 315		08 37 07	+11 42.4	K1 V	7.64	0.82	50.7	6.17	
2029	NN 3524		08 57 26	+48 38.0	k-m	14.13	1.70	50.7	12.66	
2030	GJ 1203		16 30 28	+12 43.1	k-m	12.18	1.46	50.7	10.71	
2031	Gl 781.1	A	20 04 38	-31 53.6	M3	12.25	1.55	50.7	10.78	LP 926-52 L 565-062
2032	Gl 781.1	B	20 04 35	-31 53.3	M3.5	12.50	1.63	50.7	11.03	LP 926-51 L 565-063 sep 41" 292d (NLTT)
2033	Gl 224.1		05 53 43	-63 06.3	K1 III/IV	4.65	1.05	50.6	3.20	
2034	Gl 247		06 45 27	+60 23.2	dM0 p	8.58	1.22	50.6	7.10	pi(t) Heintz AJ 94
2035	Gl 355.2		09 30 54	-20 53.6	K0 IV	5.01	1.02	50.6	3.50	
2036	Gl 507.1		13 17 22	+33 36.6	dM2	10.62	1.51	50.6	9.14	AC +33:38922 Ross 1007
2037	Gl 596.1	A	15 41 31	+02 40.4	G5 V	5.86	0.68	50.6	4.38	PSI Ser ADS 9763
2038	Gl 596.1	B	15 41 31	+02 40.4		12.00		50.6	10.50	sep 4"
2039	NN 3040		00 31 30	+70 55.5	k-m	13.52	1.65	50.5	12.04	LP 28-158
2040	Gl 365		09 40 17	+42 55.9	K5 V	8.12	1.15	50.5	6.64	
2041	GJ 1162		12 36 15	-04 02.8	m	13.52	1.60	50.5	12.04	
2042	NN 3771		13 11 26	+56 56.7	K2 II	7.97	1.17	50.5	6.50	
2043	GJ 1185		14 45 21	-02 57.5	m	13.28	1.63	50.5	11.80	
2044	Gl 678	A	17 27 49	-01 01.4	G8 IV-V	5.98	0.72	50.5	4.50	ADS 10598 V(AB) = 5.31 d(m) = 0.19

2045	Gl 678	wissenschaft in die schulen	17 27 49	-01 01.4	G8 IV-V	6.20		50.5	4.70	a = 1.017" P = 46.40 yr
2046	Gl 469.1		12 27 10	-03 03.0	G8 V	9.03	0.70	50.3	7.50	
2047	GJ 1178		13 44 59	+10 36.7	DA7	15.08	0.38	50.3	13.59	
2048	Gl 708.1		18 13 36	+64 22.8	F5 V	5.03	0.38	50.3	3.54	
2049	Gl 186		05 01 15	-23 19.3	K5 V	9.28	1.28	50.2	7.78	
2050	Gl 242		06 42 29	+12 57.1	F5 III	3.36	0.43	50.2	1.86	XI Gem BS 2484
2051	Gl 886.2		23 00 44	-35 01.2	F0 IV	5.11	0.29	50.2	3.60	PI Psa
2052	Gl 715		18 27 16	-01 51.0	dK5	8.05	1.10	50.1	6.55	
2053	Gl 725.2		18 43 31	+20 29.8	F6 V	4.19	0.46	50.1	2.69	
2054	NN 4076		18 44 47	+52 24.1	M1	15.11	1.85	50.1	13.61	LP 141-11
2055	NN 3018	A	00 13 26	-68 16.4	m	10.95		50.0	9.44	LFT 24 LTT 118 L 86-66
2056	NN 3019	B	00 13 17	-68 16.0	m	12.50		50.0	11.00	LFT 25 LTT 119 L 86-67 sep 48" 288d
2057	GJ 1020		00 42 58	-13 09.1	G0 V	6.15	0.61	50.0	4.64	LTT 421 BS 203
2058	NN 3084		01 15 18	+05 13.1	dM2	11.05		50.0	9.54	LTT 10470 Tou 23.198
2059	GJ 1048		02 33 45	-23 44.3	K2 V	8.43	1.08	50.0	6.92	
2060	NN 3350		05 29 08	-30 13.5	m	13.00		50.0	11.50	LP 892-51
2061	Gl 237		06 30 22	-43 29.8	g-k	10.59	1.48	50.0	9.08	
2062	NN 3480		08 04 06	+58 39.5	m	12.69		50.0	11.18	LP 89-101
2063	NN 3484		08 06 36	+22 03.2	m	11.81	1.53	50.0	10.30	LTT 12136 L 1321-40 LP 366-45
2064	Gl 307.1		08 24 08	+45 49.4	G5 V	6.32	0.62	50.0	4.81	
2065	NN 3531		09 03 31	+13 03.8	m	13.31		50.0	11.80	LTT 12392 L 1180-118 LP 486-49
2066	NN 3548	A	09 15 51	+26 58.1	k-m	11.77	1.50	50.0	10.30	LTT 12449

2067	NN 3549	S B	wissenschaft in die schulen 09 15 46	+26 58.8	m	16.00		50.0	14.00	LP 313-38 sep 76" 302d
2068	GJ 1127		09 34 22	+22 55.3	dM0	9.48	1.28	50.0	7.97	LTT 12540 Ross 89
2069	GJ 1130	A	09 51 17	-31 30.9	M0 V	10.21	1.38	50.0	8.70	LTT 3630 LDS 290
2070	GJ 1130	B	09 51 17	-31 30.9		14.42	1.70	50.0	12.91	
2071	NN 3574		09 54 38	+41 17.7	F6 Vas	5.14	0.46	50.0	3.63	
2072	NN 3606		10 27 32	+60 00.7	K4	8.77	1.15	50.0	7.26	LTT 12811 LFT 720
2073	NN 3632		10 53 05	-09 05.8	M4	13.54	1.63	50.0	12.00	LTT 4009 L 898-42 LP 671-10
2074	GJ 1142	A	11 05 34	-04 57.2	dM6	12.56	1.52	50.0	11.05	
2075	GJ 1142	B	11 05 28	-04 52.9	DA3	12.92	0.05	50.0	11.41	
2076	NN 3650		11 10 40	+00 30.7	K7	10.24	1.46	50.0	8.70	LTT 13023 Wolf 370
2077	GJ 429.4		11 28 18	-56 51.5	K4 Ve	8.33	1.06	50.0	6.82	
2078	NN 3675		11 34 43	+82 05.2	m	11.77	1.50	50.0	10.30	LTT 18178 AC+82:1874
2079	GJ 1147		11 36 03	-41 05.6	k	13.79	1.72	50.0	12.28	
2080	NN 3678		11 36 21	+42 36.0	K5 V	8.26	0.96	50.0	6.75	LTT 13186
2081	GJ 1153		11 56 36	-20 04.2	K2 V	7.94	0.98	50.0	6.43	LTT 4461
2082	NN 3700		11 59 07	-11 57.0	M5-6	12.34	1.46	50.0	10.83	LTT 4484 L 829-10 LP 734-14
2083	NN 3714		12 09 57	+39 57.3	M2 V	11.41	1.51	50.0	9.90	LTT 18204
2084	GJ 1165		12 45 54	-15 26.9	K2 V	7.94	0.96	50.0	6.43	
2085	NN 3766		13 09 00	+28 50.0	m	15.89	1.86	50.0	14.40	LP 322-936 San 232
2086	NN 3790		13 29 29	+23 38.7	m	12.26		50.0	10.75	LTT 13935 L 1338-13 LP 379-51
2087	NN 3795		13 36 19	+26 04.9	M3	12.56	1.52	50.0	11.10	LTT 13973 Ross 1022

2088	NN 3811	S	13 48 03	-53 17.1	m	12.90		50.0	11.40	LTT 5376 L 258-126
2089	GI 538.1		14 03 31	-26 26.5	K2 III	3.27	1.12	50.0	1.76	PI Hya
2090	NN 3853		14 27 50	+29 47.7	m	14.66		50.0	13.15	
2091	GI 578		15 05 06	+25 03.8	F5 V	4.93	0.43	50.0	3.42	
2092	NN 3896	A	15 10 29	+19 28.1	G5 V	6.68	0.68	50.0	5.17	LTT 14523 LFT 1183 ADS 9535
2093	NN 3897	B	15 10 30	+19 28.5	G7 V	7.53	0.73	50.0	6.02	LTT 14524 LFT 1184 sep 24" 10d
2094	GJ 1191		15 19 54	-10 28.8	K2 V	7.99	0.95	50.0	6.48	LTT 6139
2095	GI 627	A	16 26 41	+18 31.1	K3 V	7.68	0.85	50.0	6.17	ADS 10075 V(AB) = 7.01 d(m) = 0.17
2096	GI 627	B	16 26 41	+18 31.1	K3 V	7.85		50.0	6.34	a = 2.234" 236.07 yr
2097	NN 3970		16 39 25	-37 14.8	G8 V	7.13	0.77	50.0	5.62	
2098	NN 3987		17 00 09	-05 59.8	dM2	10.85	1.50	50.0	9.34	Steph 1422
2099	NN 4010		17 28 54	+47 26.3	G5	7.21		50.0	5.70	
2100	NN 4034		17 53 40	+36 11.7	G5	7.84		50.0	6.33	
2101	NN 4039	AB	17 55 10	+24 00.0	G2 V	6.30	0.64	50.0	4.79	BS 6697 SB: P = 2.41 yr, d (m) = 1.5
2102	GI 702.2		18 03 09	+04 39.4	G2 V	6.80	0.62	50.0	5.29	
2103	GJ 2135		18 21 15	-13 09.9	DA7	15.60	0.42	50.0	14.09	WD1821- 131
2104	GI 725.1		18 43 05	+43 46.8	K0	7.54	0.84	50.0	6.03	
2105	GJ 1239		19 29 14	-35 33.7	K5 V	8.71	1.11	50.0	7.20	LTT 7719
2106	GI 764.2		19 34 45	-14 24.8	F7 V	5.47	0.50	50.0	3.96	
2107	NN 4131		20 00 56	-31 49.7	m	14.50		50.0	13.00	LP 926-31

2108	NN 4149	S	wissenschaft in die schulen	20 32 11	+03 10.8	m	12.00	1.43	50.0	10.49	LTT 16006 USNO 762
2109	NN 4159			20 41 06	-00 21.8	K0	11.47	1.48	50.0	10.00	LTT 8204 L 999-6
2110	NN 4163			20 46 37	+19 32.1	m	13.38	1.54	50.0	11.87	
2111	NN 4166			20 48 13	+26 19.6	DC9	15.58	0.95	50.0	14.07	
2112	G1 812.1			20 54 22	-44 18.5	G0 V	6.53	0.58	50.0	5.02	
2113	NN 4290			22 38 28	+44 20.2	m	13.20		50.0	11.69	
2114	G1 872	A		22 44 12	+11 55.0	F6 IV-V	4.19	0.50	50.0	2.70	XI Peg
2115	G1 872	B		22 44 12	+11 55.0	M1	11.70		50.0	10.20	
2116	NN 4302			22 52 09	-05 44.7	m	13.90		50.0	12.40	
2117	NN 4311			23 04 36	+71 26.8	M2	11.78	1.48	50.0	10.27	LP 48-822
2118	NN 4316			23 09 35	-14 21.9	m	13.00		50.0	11.50	LP 762-3
2119	G1 894.4			23 19 11	+43 49.2	K1 V	7.36	0.80	50.0	5.85	
2120	NN 4353			23 35 37	-41 47.6	M3	11.93	1.46	50.0	10.42	LTT 9635 Sm 142
2121	NN 4361			23 43 52	-50 59.5	m	14.60		50.0	13.10	LFT 1824 LTT 9699 L 288-117
2122	GJ 2019			00 58 12	-26 54.3	K0	10.11	0.76	49.9	8.60	
2123	G1 176.3			04 44 23	-50 09.6	K0 V	7.59	0.89	49.9	6.08	
2124	G1 321.3	A		08 43 19	-54 31.5	A0 V	2.02	0.04	49.8	0.51	DEL Vel V (AB) = 1.96 d (m) = 3.0
2125	G1 321.3	B		08 43 19	-54 31.5		5.00		49.8	3.50	sep(AB) 2.6" 175d - 2.6" 153d (1894- 1952)
2126	G1 321.3	C		08 43 26	-54 30.9		11.00		49.8	9.50	sep(AC) 69.2" 61d (1879-1913)
2127	G1 321.3	D		08 43 26	-54 30.9		13.50		49.8	12.00	sep(CD) 6.2" 102d (1930- 1935)

2128	GI 459.3		12 16 56	+28 39.5	M2 V	10.63	1.44	49.8	9.12	LFT 896
2129	GI 612.1		16 04 48	+34 45.9	dM0	10.45	1.24	49.8	8.94	
2130	GI 797	A	20 38 29	+19 45.2	G5 V	6.45	0.63	49.8	4.94	
2131	GI 797	B	20 38 29	+19 43.1	m	11.88	1.55	49.8	10.37	L 1288-004
2132	GI 834	A	21 34 38	+39 14.0	dM0	10.34	1.42	49.8	8.83	LP 286-6 AC +39:60670 V (AB) = 10.18 d(m) = 2.0
2133	GI 834	B	21 34 38	+39 14.0		12.30		49.8	10.80	LP 286-5 sep 3" 295d (NLTT)
2134	GI 17.1		00 18 52	-46 00.7	M1	10.40	1.48	49.7	8.88	
2135	Wo 9175		05 05 23	-05 09.0	A3 III	2.79	0.13	49.7	1.27	
2136	GI 596.2		15 41 48	+06 34.9	K2 III	2.64	1.17	49.7	1.12	ALF Ser
2137	GI 11	A	00 10 26	+69 03.2	dM4 J	13.06	1.60	49.6	11.54	LTT 10070 LP 50-30 ppm(LHS), V (AB) = 12.49 d(m) = 0.4
2138	GI 11	B	00 10 26	+69 03.2		13.40		49.6	11.90	sep 0.7" 319d (NLTT)
2139	GJ 1122	A	09 16 12	+38 44.0	m	14.52	1.68	49.6	13.00	
2140	GJ 1122	B	09 16 12	+38 44.1	m	14.67	1.68	49.6	13.15	sep 9" 180d (Giclas)
2141	GI 660.1		17 10 11	-05 03.4	M0	11.62	1.46	49.6	10.10	AC-05:4400- 84
2142	NN 4237	A	21 53 27	+32 48.0		10.00		49.6	8.50	
2143	NN 4238	B	21 53 27	+32 48.0		10.20		49.6	8.70	sep 3.4"
2144	NN 3373	A	05 55 27	+68 09.7	k-m	12.90	1.56	49.5	11.37	LP 57-41 LDS 1201
2145	NN 3374	B	05 55 24	+68 08.8	m	13.31	1.59	49.5	11.78	LP 57-40 sep 56" 193d (NLTT)
2146	GI 412.2		11 05 31	-29 54.1	G2 V	6.54	0.60	49.5	5.01	
2147	GI 659	A	17 09 08	+54 33.4	dK8	8.85	1.16	49.5	7.32	

2148	Gl 659	wissenschaft in die schulen B	17 09 10	+54 33.1	dK8	9.34	1.25	49.5	7.81	
2149	Gl 171.1	A	04 33 03	+16 24.6	K5 III	0.85	1.54	49.4	-0.68	ALF Tau ADS 3321
2150	Gl 171.1	B	04 33 03	+16 24.6	dM2	13.50		49.4	12.00	sep 30.4" 110d
2151	Gl 173.1	A	04 36 58	+09 46.8	K3 V	9.20	1.02	49.4	7.67	
2152	Gl 173.1	B	04 36 59	+09 46.1	k-m	14.19	1.57	49.4	12.66	sep 34" 162d (NLTT)
2153	Gl 333.3		09 01 40	-66 11.8	A5 V	4.01	0.14	49.4	2.50	ALF Vol
2154	NN 3710		12 08 58	+57 41.1	DA9	15.79	0.58	49.4	14.26	
2155	NN 3756		12 53 41	+51 12.3	m	14.40	1.74	49.4	12.87	
2156	GJ 1257		20 38 45	-22 29.4	K5 V	9.70	1.11	49.4	8.17	LTT 8180 Wo 9704
2157	Gl 808.1		20 45 06	-44 10.3	F1 IV	5.10	0.35	49.4	3.57	IOT Mic
2158	Gl 160.2		04 04 23	-20 58.5	dM0	9.68	1.22	49.3	8.14	
2159	Gl 351.1		09 28 44	+20 30.8	M3	12.20	1.48	49.3	10.66	Ross 84
2160	Gl 455		11 59 48	+28 52.0	M3	12.84	1.75	49.3	11.30	L 1405-009
2161	Gl 464		12 21 21	+12 51.6	dM2	10.39	1.44	49.3	8.90	AC+13:1308- 25
2162	Gl 496.1		13 02 04	-52 09.8	K9 V	9.06	1.37	49.3	7.52	CD-51:7244 LFT 966
2163	Gl 695.1		17 44 39	-33 59.7	G8 V	7.19	0.71	49.3	5.65	
2164	Gl 156.2		03 54 49	+76 01.6	K4 V	8.26	1.15	49.2	6.72	
2165	GJ 1117		08 56 11	+33 08.8	DQ6	15.18	0.01	49.2	13.64	
2166	Gl 121.2		03 01 09	-05 51.5	dG5	8.09	0.67	49.1	6.55	
2167	Gl 891.1		23 10 15	+49 08.0	F0 V	4.52	0.29	49.1	2.98	
2168	NN 3002		00 02 16	+34 22.8	G2 V	6.11	0.62	49.0	4.56	LTT 10009 LFT 4
2169	Gl 22.2		00 32 05	-52 39.0	F3 IV-V	5.57	0.46	49.0	4.00	
2170	NN 3045		00 35 48	+51 11.4	m	12.60		49.0	11.05	
2171	Gl 31.5		00 42 32	-65 54.8	G3 V	6.54	0.65	49.0	4.99	LTT 416
2172	NN 3072		00 59 54	-10 41.0	K7 V	10.04	1.35	49.0	8.49	U 15

2173	NN 3115	S	01 45 52	+32 26.3	F8 V	5.79	0.55	49.0	4.24	LTT 10624
2174	NN 3137		02 05 55	+88 10.0	m	12.89		49.0	11.34	LP 1-52
2175	GI 85		02 05 56	-66 48.7	m	11.52	1.53	49.0	9.97	L 89-027
2176	GI 100	A	02 26 41	-20 12.3	K4 V	8.86	1.18	49.0	7.31	V(AB) = 8.76 d(m) = 2.5
2177	GI 100	B	02 26 41	-20 12.3		11.40		49.0	9.90	sep(AB) 0.6" 312d (1951)
2178	GI 100	C	02 26 12	-20 15.9	M3	12.85	1.61	49.0	11.30	LTT 1226
2179	GI 114		02 47 49	+15 30.6	dK6	8.90	1.20	49.0	7.35	
2180	GI 162.1		04 06 49	-64 21.5	G3 V	6.38	0.64	49.0	4.83	
2181	GI 198		05 16 37	-18 10.9	G0 V	5.96	0.57	49.0	4.41	dG0 (Wilson)
2182	GI 204.1		05 27 03	-60 27.3	G5 Ve	6.99	0.77	49.0	5.44	
2183	GI 209.1		05 35 47	-28 43.1	F5 V	5.30	0.46	49.0	3.75	NU(2) Col
2184	NN 3382		06 00 14	-20 20.1	m	13.25		49.0	11.70	LP 779-10
2185	GI 226.3		06 02 48	+35 23.8	G0 V	6.11	0.60	49.0	4.56	
2186	NN 3462		07 40 18	+18 18.3	k-m	11.34	1.40	49.0	9.79	LTT 12062 L 1249-13
2187	NN 3501	A	08 28 55	-05 51.8	M1.5	11.21	1.41	49.0	9.66	LTT 3154 L 891-16 LP 665-21
2188	NN 3502	B	08 29 00	-05 52.0	M3	12.36	1.47	49.0	10.81	LTT 3155 L 891-15 LP 665-22 sep 83" 97d
2189	NN 3527		08 58 36	+02 08.4	k	11.82	1.50	49.0	10.30	LTT 12366 Ross 625
2190	NN 3557		09 25 12	+13 58.1	G5	7.81		49.0	6.26	
2191	GI 346		09 26 24	-09 02.8	dM0	10.52	1.43	49.0	8.97	
2192	NN 3610	A	10 31 32	+46 33.8	m	13.13		49.0	11.58	LP 167-64 L 1617-7
2193	NN 3611	B	10 31 28	+46 34.0	m+	15.50		49.0	14.00	LP 167-63 sep 46.5" 285d

2194	NN 3636	S	wissenschaft in die schulen!	10 58 12	+12 20.0	M5 e	15.96		49.0	14.41	IE 1058.2 +1220 V-R (kc) = 1.48, R-I(kc) = 1.87 FLGM
2195	NN 3687			11 45 33	-34 56.8	G5/6 V	7.09	0.77	49.0	5.54	
2196	GJ 2096			12 36 40	-77 34.4	K5 V	9.05	1.20	49.0	7.50	CP-77: 859
2197	NN 3781	A		13 21 06	+02 58.9	G5 V	7.06	0.77	49.0	5.51	LTT 13889 ADS 8883
2198	NN 3782	B		13 21 08	+02 59.0	G5 V	7.36	0.83	49.0	5.81	LTT 13890 sep 27" 76d
2199	GI 509.1			13 21 26	+58 10.0	M0 V	9.75	1.26	49.0	8.20	
2200	GI 534.2			13 54 01	+79 05.7	dM1	10.61	1.45	49.0	9.06	AC+79:4347
2201	GI 539.1			14 03 48	-74 36.9	G1 V	6.02	0.58	49.0	4.47	
2202	NN 3842			14 18 02	+39 16.7	M0:e:	12.31	1.51	49.0	10.76	Steph 1145
2203	NN 3888			15 02 08	-20 55.2	m	14.70		49.0	13.20	LP 801-53
2204	NN 3934			15 59 24	-24 57.2	m	13.20		49.0	11.70	LP 861-12
2205	NN 4045			18 12 05	-77 03.6	m	14.10		49.0	12.60	LTT 7245 L 44-59
2206	GI 708.4			18 14 06	+45 11.6	G2 V	6.29	0.62	49.0	4.74	
2207	NN 4067			18 38 09	+33 21.8	m	13.12		49.0	11.57	LTT 15504 L 1498-10 LP 280-9
2208	NN 4081			18 47 35	-60 49.6	m	13.40		49.0	11.90	LTT 7469 L 159-20
2209	GJ 1244			19 50 37	-72 29.5	K5 V	8.45	1.06	49.0	6.90	LTT 7857
2210	NN 4136			20 05 21	-01 41.2	k-m	13.55	1.62	49.0	12.00	LTT 7959 L 997-68 LP 634-18
2211	NN 4152			20 34 54	+38 40.1	m	13.35		49.0	11.80	LTT 16018 L 1575-70 LP 284-7
2212	NN 4189	A		21 15 05	+20 41.0	M3	12.47		49.0	10.92	LTT 16245 Ross 773 V (AB) = 12.23 d(m) = 1.5

2213	NN 4190	S B	21 15 05	+20 41.0	M4	14.00		49.0	12.00	LTT 16246 sep 4" 173d (NLTT)
2214	NN 4193		21 23 00	-42 39.0	M7	12.67	1.53	49.0	11.12	Sm 79 BPM 43997
2215	NN 4217		21 42 48	-06 07.7	M3.5	13.54	1.65	49.0	12.00	LTT 8681 Wolf 939
2216	NN 4229	A	21 49 35	-77 34.3	K3/4 V	8.24	1.00	49.0	6.69	LTT 8736 CD-77: 1092
2217	NN 4230	B	21 49 35	-77 34.3		10.50		49.0	9.00	sep 7.85" 306d (1980.8)
2218	G1 840		21 52 32	+32 05.7	dK0 e	7.78	0.92	49.0	6.23	
2219	NN 4253		22 02 53	-38 30.3	M3.5	12.45		49.0	10.90	LTT 8846 L 499-75 LP 983-87
2220	G1 871	A	22 39 39	-47 28.1	G1 V	6.00	0.57	49.0	4.45	
2221	G1 871	B	22 39 39	-47 28.1	M1	11.10	1.41	49.0	9.55	
2222	NN 4291		22 40 46	-06 39.6	K0	8.12	0.97	49.0	6.57	LTT 9164
2223	NN 4329		23 15 01	+06 07.3	dM4	12.53	1.55	49.0	11.00	LTT 16844 Viln 82 no 35
2224	GJ 1283		23 16 10	-60 47.6	K4 V	8.97	1.15	49.0	7.42	
2225	NN 4359		23 41 32	+64 27.8	M1.5	11.30	1.40	49.0	9.75	LTT 16992 LFT 1821 Ross 676 AC +64:8806
2226	GJ 1064	A	03 43 37	+41 17.4	K1 V	8.15	0.78	48.9	6.60	LTT 11256 Wolf 225 ADS 2757
2227	GJ 1064	B	03 43 37	+41 17.5	K2 V	8.75	0.90	48.9	7.20	LTT 11257 sep 8" 50d (NLTT)
2228	G1 339	AB	09 12 17	+04 39.0	dK5	8.04	1.02	48.9	6.49	orb Heintz AJ 94: sep 0.7": d(m) = 3. ., V(AB) = 7.97
2229	G1 297.2	A	08 08 21	-13 39.1	F7 V	5.54	0.49	48.8	3.98	

2230	GI 297.2		08 08 15	-13 39.9	M3	11.82	1.51	48.8	10.26	L 818-040
2231	NN 3493		08 16 26	-15 02.7	K3 V	9.84	1.13	48.8	8.28	U182 SB? pos(BDX)
2232	GI 321.1		08 42 37	-42 28.0	G5 III	4.06	0.87	48.8	2.50	
2233	GI 804		20 42 06	+19 34.5	dM1.5e	10.31	1.45	48.8	8.75	
2234	GI 828.5		21 26 43	+73 25.9	DA4	12.80	0.02	48.8	11.24	LTT 18524 AC+73:8031
2235	GI 53.3		01 06 55	+35 21.4	M0 IIIe	2.05	1.57	48.7	0.49	BET And
2236	GI 217.1		05 44 41	-14 50.4	A3 V	3.55	0.10	48.7	1.99	ZET Lep
2237	NN 3925	A	15 51 11	+34 54.5	M3	11.75	1.51	48.7	10.19	LTT 14715 LFT 1231 Ross 806
2238	NN 3926	B	15 51 11	+34 54.0	m	13.18	1.53	48.7	11.62	LTT 14716 LFT 1232 L 1489-3 LP 274-21 sep 26" 174d
2239	GI 609.1		16 00 57	+58 41.9	F8 IV-V	4.01	0.52	48.7	2.45	THE Dra
2240	Wo 9131		03 44 06	+23 50.5	F0 V	8.38	0.29	48.6	6.80	HZ 1284 TR365
2241	GI 334.1		09 05 22	+73 36.9	K7	10.17	1.26	48.6	8.60	
2242	NN 3602		10 25 21	+48 29.8	m	13.25	1.67	48.6	11.68	USNO 717
2243	GI 563.4		14 47 55	-15 47.4	F5 IV-V	5.15	0.41	48.6	3.58	
2244	Wo 9615	A	18 04 59	+09 33.3	A4 V	3.73	0.12	48.6	2.16	BDS 8359
2245	Wo 9615	B	18 04 59	+09 33.3		14.00		48.6	12.00	sep 25.4" 299d (1934)
2246	GI 762.1		19 30 18	+58 29.0	K1 V	6.59	0.87	48.6	5.02	
2247	GI 895.3		23 26 49	-47 18.6	K7 V	10.21	1.31	48.6	8.64	CD- 47:14591 Sm 137
2248	GJ 1034		01 13 40	+24 04.2	m	15.04	1.84	48.5	13.47	
2249	Wo 9125		03 41 17	+24 37.6	G0	10.81	0.70	48.5	9.20	HZ 293 TR 98
2250	GJ 1078		05 20 47	+22 30.2	m	15.52	1.83	48.5	13.95	
2251	GI 249.1		06 48 30	-46 33.6	F5 III	5.13	0.45	48.5	3.60	
2252	GJ 1193		15 32 13	+14 26.3	M3.5	13.83	1.57	48.4	12.25	Ross 512

2253	Gl 672.1	wissenschaft in die schulen!	17 20 35	-32 11.8	M2	11.64	1.50	48.4	10.06	LP 920-1 L 557-068
2254	Gl 761.1		19 27 26	+31 30.6	G7 IV	6.96	0.71	48.4	5.38	
2255	Gl 4.2	A	00 03 44	-49 21.2	G1 IV	5.71	0.52	48.3	4.13	
2256	Gl 4.2	B	00 03 44	-49 21.2		11.50		48.3	9.90	sep 5.4" 176d
2257	Wo 9099		02 42 14	+09 54.3	F0 IV	4.27	0.31	48.3	2.70	LTT 10901
2258	Gl 273.1		07 25 49	+32 05.7	dK8	7.74	0.94	48.3	6.16	
2259	NN 3552		09 17 22	+26 56.9	m	15.56	1.92	48.3	13.98	LP 313-42 USNO 714
2260	Wo 9448	A	13 29 41	+31 23.4	M0 V	11.11	1.44	48.3	9.53	WOR 24 V (AB) = 10.45 d(m) = 0.2
2261	Wo 9448	B	13 29 41	+31 23.4		11.30		48.3	9.70	WOR 24 sep 0.26" 335.9d (1961.39)
2262	NN 3826		14 08 15	+76 05.0	M1	11.60		48.3	10.00	LTT 14140 AC+76:4935
2263	Gl 580.2		15 14 03	+67 32.2	F8 V	5.13	0.53	48.3	3.55	
2264	Gl 717		18 30 42	-11 40.3	K7 V	10.00	1.28	48.3	8.42	
2265	GJ 1275		22 48 56	+29 23.7	DA9	15.52	0.63	48.3	13.94	
2266	Gl 893.3	A	23 14 00	-41 03.6	g-k	11.57	0.90	48.3	10.00	LP 1034-092 L 431-25
2267	Gl 893.3	B	23 14 01	-41 03.9		17.40		48.3	15.80	LP 1034-093 sep 19" 160d (NLTT)
2268	Gl 677	A	17 27 24	+29 26.0	dM0 J	9.55	1.15	48.2	7.97	ADS 10585 V(AB) = 8.97 d(m) = 0.38
2269	Gl 677	B	17 27 24	+29 26.0		9.93		48.2	8.35	a = 0.60" P = 60.0 yr
2270	GJ 1021		00 43 25	-47 49.6	G5 IV	5.80	0.64	48.1	4.20	BS 209
2271	Gl 97.1		02 20 51	-68 53.2	A3 Vn	4.08	0.03	48.1	2.50	DEL Hyi
2272	GJ 1205		16 39 50	+53 47.0	DC7	15.06	0.33	48.1	13.47	LP 137-43 GD356 PG
2273	NN 4120		19 40 06	+71 45.5	M0.5	10.96	1.48	48.1	9.37	LTT 18490 AC+71:8595

2274	Wo 9771		22 07 41	+05 57.1	A2 V	3.53	0.08	48.1	1.94	LTT 16484
2275	GJ 1274		22 48 14	+34 35.2	m	11.72	1.53	48.1	10.13	LP 289-11
2276	Wo 9832		23 35 06	+46 11.2	G8 III-IV	3.82	1.01	48.1	2.23	LTT 16964
2277	NN 3050		00 41 36	+75 39.9	G8	7.19	0.75	48.0	5.60	LTT 10255
2278	NN 3059		00 46 43	-50 24.9	M2	10.75	1.43	48.0	9.16	LTT 464 L 219-8 CFS 223 Sm 174
2279	GJ 39		00 48 43	+18 28.3	dK6	9.24	1.21	48.0	7.65	
2280	NN 3134		02 03 23	+64 03.1	m	14.31		48.0	12.72	
2281	NN 3166		02 32 30	+23 21.0	M3 e	13.71	1.58	48.0	12.12	X-ray src: Fleming et al 1988
2282	Wo 9087		02 34 09	-03 22.4	K3	8.10	0.95	48.0	6.51	LTT 1274
2283	NN 3171		02 34 24	+06 41.0	M5 e	16.00		48.0	14.41	IE 02344 +0641 R-I (KC) = 1.85, V-R(KC) = 1.49
2284	NN 3196	A	03 01 17	-13 02.1	k-m	13.37		48.0	11.78	LP 711-43
2285	NN 3197	B	03 01 24	-13 02.9	k-m	13.50		48.0	11.91	LP 711-44 sep 114" 115d
2286	NN 3204		03 06 33	+58 15.0	M3	11.72	1.50	48.0	10.13	
2287	NN 3206		03 07 48	+61 21.0	dK8	10.12	1.32	48.0	8.53	SpT K5 III OP
2288	Wo 9120		03 36 40	+25 19.6	M3.5	13.10		48.0	11.50	LTT 11207 Wolf 205 LFT 300 cpm to Wolf 204
2289	GJ 1063		03 42 05	+11 45.7	dK8	9.15	1.18	48.0	7.56	
2290	GJ 154.1	A	03 43 19	-28 01.2	K5 V	8.25	1.00	48.0	6.66	ADS 2756 V (AB) = 8.22 d (m) = 3.30

2291	GI 154.1		03 43 19	-28 01.2	M3 V	11.60		48.0	10.00	sep 1.8" 78d (1959)
2292	GI 155.1		03 45 23	+02 38.5	M1	11.04	1.50	48.0	9.45	AC+02:2282- 51
2293	NN 3335		05 06 18	+15 24.3	M3	12.48	1.50	48.0	10.89	LTT 11591 LFT 392 Ross 388
2294	NN 3341		05 13 51	-31 21.2	m	12.15		48.0	10.56	LTT 2219 L 521-2 LP 892-26
2295	NN 3363		05 41 35	+32 22.3	G5	8.15		48.0	6.56	
2296	NN 3418		06 55 22	+14 17.3	G5	8.28		48.0	6.69	
2297	GI 279		07 31 55	-22 11.2	F6 IV	4.45	0.51	48.0	2.86	
2298	NN 3456		07 35 18	+85 06.0	m	12.80		48.0	11.21	LP 4-258
2299	NN 3461		07 39 15	+05 09.6	m	12.71		48.0	11.12	LTT 12058
2300	NN 3468	A	07 55 41	+15 38.5	m	14.24		48.0	12.65	LDS 3768
2301	NN 3469	B	07 55 40	+15 38.3	m	15.09		48.0	13.50	LDS 3768
2302	NN 3505		08 30 34	+18 42.5	m	14.75		48.0	13.16	LTT 12227
2303	GI 342		09 21 35	+76 09.1	dK5 e	9.03	1.19	48.0	7.44	
2304	NN 3556		09 24 07	+50 52.4	m	11.93		48.0	10.34	
2305	NN 3580		09 57 13	+24 47.6	K0 V	7.90	0.88	48.0	6.31	LTT 12668
2306	Wo 9326		10 19 13	+41 29.0	F7 V	5.77	0.53	48.0	4.18	
2307	NN 3607		10 27 35	+33 06.0	M6 e:	12.72	1.45	48.0	11.13	
2308	NN 3615		10 41 08	-28 48.0	K1 V	7.74	0.89	48.0	6.15	LTT 3932
2309	NN 3638		10 58 47	+15 17.0	G8	7.66	0.94	48.0	6.07	LTT 12950
2310	GJ 2085		11 21 13	+08 50.1	dM1	11.18	1.48	48.0	9.59	

2311	GI 430	wissenschaft in die schulen	11 28 22	+63 26.0	dM0	10.02	1.33	48.0	8.43	
2312	GI 441		11 43 08	+72 22.3	dK8	9.02	1.17	48.0	7.43	
2313	Wo 9381		11 52 36	+01 15.1	M1.5	11.50	1.44	48.0	9.91	LTT 13296 LFT 862 Ross 129 comp. B: G8: opt.
2314	NN 3695		11 55 01	+12 06.2	M2.5	11.86	1.45	48.0	10.27	LFT 846 LTT 13307 Ross 122
2315	NN 3738		12 36 41	+47 18.9	m	12.14		48.0	10.55	
2316	GJ 1164	A	12 45 32	-24 32.2	K4/5 V	9.02	1.12	48.0	7.43	LTT 4898
2317	GJ 1164	B	12 45 31	-24 32.0	K7	10.04	1.38	48.0	8.45	LTT 4899
2318	GJ 1173		13 32 51	-00 08.2	K7 V	10.28	1.44	48.0	8.69	LTT 5259 U324
2319	GI 522		13 39 22	+00 07.7	M0 V	9.74	1.30	48.0	8.15	
2320	NN 3810		13 47 58	-21 26.3	M2.5	12.72	1.56	48.0	11.13	LTT 5375 L 691-20 LP 798-44
2321	NN 3814		13 50 36	-09 01.6	DA6	14.60	0.21	48.0	13.01	LTT 5410 L 907-37 LP 678-4
2322	NN 3819		13 56 21	-23 18.9	f-g	14.93	0.32	48.0	13.34	LTT 5453 L 691-60 LP 856-2
2323	GI 540.3		14 12 28	-44 46.0	G4 V	6.31	0.60	48.0	4.72	
2324	GI 550.3		14 26 03	-46 14.3	K5	10.35	1.44	48.0	8.76	
2325	GI 563.2	A	14 46 42	-25 53.8	M3	11.66	1.49	48.0	10.07	LTT 5883
2326	GI 563.2	B	14 46 40	-25 54.0	M3	12.06	1.52	48.0	10.47	LTT 5884
2327	GI 586	C	15 25 03	-08 51.0	k-m	15.41	1.84	48.0	13.82	
2328	NN 3920		15 48 14	+51 11.7	M3:	12.05	1.53	48.0	10.46	
2329	NN 3962		16 32 10	+03 24.2	k	11.57	1.48	48.0	10.00	LTT 14922
2330	NN 3975		16 48 17	-04 45.4	k	13.40		48.0	11.80	
2331	NN 3989		17 07 05	+03 59.7	G5	7.95		48.0	6.36	

2332	NN 3999	A	17 14 57	-11 46.6	M3	12.83	1.49	48.0	11.24	LTT 6883 L 845-15 LP 747-20
2333	NN 4000	B	17 14 56	-11 46.1	M3	12.91	1.49	48.0	11.32	LTT 6882 L 845-16 LP 747-19 sep 30" 338d
2334	NN 4012		17 33 12	-54 24.0	DA8	15.80	0.46	48.0	14.20	LTT 6999 BPM 24960 L 270-137
2335	NN 4016		17 36 27	+08 03.3	M4	12.28	1.57	48.0	10.69	
2336	NN 4046		18 13 33	+18 55.5	M0	10.84	1.50	48.0	9.25	LTT 15403 Wolf 835
2337	NN 4052		18 17 19	-09 36.9	G8 V	6.92	0.70	48.0	5.33	LTT 7289
2338	NN 4088		18 54 45	+07 30.5	m	11.20		48.0	9.61	LP 571-80
2339	NN 4103		19 09 18	+32 35.0	m	10.48		48.0	8.89	LP 336-6
2340	GJ 755		19 18 12	-35 04.6	G5 V	6.48	0.62	48.0	4.89	
2341	GJ 1237		19 25 02	+49 21.2	K3 V	8.01	0.93	48.0	6.42	
2342	NN 4114	A	19 32 41	+08 21.0	dM1	10.38	1.46	48.0	8.79	AC+08:147- 294
2343	NN 4115	B	19 32 41	+08 21.0		12.52	1.52	48.0	10.93	sep 6.2" 9d
2344	NN 4162		20 42 44	-29 38.1	m	13.40		48.0	11.80	LP 928-7
2345	NN 4164		20 47 04	-00 32.2	M3.5	13.06	1.53	48.0	11.50	LTT 8247 Wolf 882
2346	Wo 9714		20 58 35	-32 43.2	K5 V	9.40	1.24	48.0	7.81	LTT 8325
2347	GJ 1262		21 20 19	-68 26.7	G5 V	6.97	0.73	48.0	5.38	LTT 8497
2348	NN 4258	AB	22 04 25	+65 23.9	M1.5	11.62	1.55	48.0	10.03	LTT 16470 J??
2349	NN 4264		22 11 16	+25 43.3	m	13.62		48.0	12.03	L 1436-28 LP 399-165
2350	GJ 851.4		22 12 13	+56 52.3	K0	9.83	0.72	48.0	8.20	
2351	NN 4351		23 35 30	+45 55.4	G5	6.58	0.66	48.0	4.99	LTT 16967 BS 8964

2352	GI 908.1		23 47 55	+30 04.5	dK8	9.34	1.26	48.0	7.75	
2353	GI 226.1		06 00 47	+26 09.4	M3.5	13.67	1.65	47.9	12.07	Ross 60
2354	GI 611.1		16 03 51	-70 55.9	G8 V	7.22	0.72	47.9	5.62	
2355	Wo 9652	A	19 12 30	+19 13.4	M3	11.55		47.9	9.95	LTT 15634 LFT 1463 Ross 733 double?
2356	Wo 9652	B	19 12 30	+19 12.7	M3.5	13.27		47.9	11.67	LTT 15635 LFT 1464 Ross 734 sep 45" 178d
2357	Wo 9015	A	00 30 28	-63 18.4	A0 V	5.75	0.04	47.8	4.15	BS 136 V (AB) = 5.09 d (m) = 0.2
2358	Wo 9015	B	00 30 28	-63 18.4	A	6.00		47.8	4.40	sep 0.1" 143d
2359	GI 378.3		10 04 29	+35 29.4	A7 V	4.48	0.18	47.8	2.90	
2360	GJ 1052		02 43 58	-02 39.6	DA7	15.53	0.36	47.7	13.92	
2361	NN 3857		14 30 01	+05 59.6	dM0	10.64	1.23	47.7	9.03	LTT 14280
2362	GI 854		22 15 08	+68 05.4	dK6	9.23	1.15	47.7	7.62	
2363	NN 4108		19 20 42	+29 20.6	m	15.37	1.82	47.6	13.76	
2364	GI 826.1		21 17 25	-20 03.3	K5 V	9.12	1.35	47.6	7.51	
2365	GI 857.1	A	22 22 24	+22 17.9	dK7 e	8.86	1.19	47.6	7.25	ADS 15915 V(AB) = 8.82 d(m) = 3.5
2366	GI 857.1	B	22 22 24	+22 17.9		12.40		47.6	10.80	sep 1.3" 204d (1959)
2367	GI 54.3		01 12 51	-65 01.4	K0 IV/V	9.05	0.76	47.5	7.43	
2368	GI 105.3		02 36 56	-26 31.8	G2 V-VI	8.76	0.60	47.5	7.10	
2369	GI 240.1		06 37 44	+79 37.4	F8 V	5.45	0.50	47.5	3.83	
2370	GI 616.2		16 15 59	+55 23.8	dM1.5e	9.96	1.48	47.5	8.34	CR DRA possible binary: Heintz AJ 101, 1071
2371	GI 825.3		21 15 28	-00 02.8	dK6	8.22	0.98	47.5	6.60	

2372	GJ 1045		02 12 14	+17 11.5	m+	14.44	1.62	47.4	12.82	
2373	Gl 224		05 53 12	+13 55.5	G5 IV	6.61	0.65	47.4	5.00	
2374	Gl 469.2	A	12 27 30	-13 07.0	G0 V J	6.46	0.58	47.4	4.84	V(AB) = 6.37 d(m) = 2.73
2375	Gl 469.2	B	12 27 30	-13 07.0		9.20		47.4	7.60	a = 1.510" P = 180.0 yr
2376	Gl 490	A	12 55 19	+35 29.8	M0 Ve	10.68	1.44	47.4	9.06	BF Cvn
2377	Gl 490	B	12 55 18	+35 29.6	dM4 e	13.20	1.64	47.4	11.58	
2378	Gl 600		15 49 46	+11 01.6	dM0	9.36	1.42	47.4	7.74	
2379	Gl 757		19 21 36	-22 09.3	K4	10.92	1.41	47.4	9.30	
2380	Gl 773	A	19 54 33	-12 41.7	K4 V	9.30	1.33	47.4	7.68	
2381	Gl 773	B	19 54 37	-12 41.5	m	15.36		47.4	13.74	LP 754-5 sep. 62" 75d (LHS)
2382	Gl 518.2	A	13 34 55	+30 20.3	G8 V	9.30	0.64	47.3	7.70	
2383	Gl 518.2	B	13 34 57	+30 20.4		10.51	0.83	47.3	8.90	
2384	Gl 748.1		19 11 01	+76 28.7	F2 V	5.13	0.31	47.3	3.50	
2385	NN 4158		20 40 23	-52 06.1	A7 III-IV	4.51	0.27	47.3	2.90	BS 7920 other SpT: A6 - A9 var
2386	NN 4286		22 34 34	-00 53.2		10.50		47.3	8.90	VVO 271
2387	Gl 29.1		00 40 05	+35 16.4	dM0 e	10.52	1.50	47.2	8.90	FF And
2388	Gl 318.1		08 39 58	+44 40.6	M1.5:	14.11	1.63	47.2	12.48	Wolf 321
2389	Gl 336		09 06 29	+33 01.9	dM2	9.96	1.39	47.2	8.33	COU 1561
2390	Gl 454.1		11 58 35	-01 27.4	K4	10.96	1.12	47.2	9.30	LTT 4483 AC-01:240- 110
2391	NN 3035		00 24 22	+49 25.5	m	14.25		47.1	12.62	
2392	Gl 187.2	A	05 02 45	+51 32.0	F0 V	5.00	0.33	47.1	3.40	
2393	NN 3408	A	06 42 51	+32 36.5	K3 V	8.77	0.96	47.1	7.14	LTT 11914
2394	NN 3409	B	06 42 53	+32 36.4	M0.5	12.17	1.53	47.1	10.54	LTT 11915 Ross 419 sep 31" 101d

2395	NN 3005	S	wissenschaft in die schulen	00 02 54	-50 20.0	M5	11.95	1.50	47.0	10.31	BPM 16002 SM 152 R-I = 1.23 Weistrop
2396	NN 3008			00 05 53	+17 08.8	dM0	10.79	1.47	47.0	9.15	
2397	G1 52.1			01 04 35	-51 15.5	K1 V	8.85	0.94	47.0	7.21	
2398	G1 53.1	A		01 04 56	+22 41.7	K4 V	8.41	1.12	47.0	6.77	
2399	G1 53.1	B		01 04 56	+22 41.7	M3	13.60		47.0	11.96	
2400	NN 3080			01 10 13	+41 23.4	G5	7.28	0.78	47.0	5.64	LTT 10444
2401	NN 3102			01 35 15	-49 26.7	K7	10.50		47.0	8.90	CFS 445 CP- 49:211 LFT 141 LTT 886 L 294-102
2402	G1 84.1	A		02 03 07	-28 18.8	M0.5	10.92	1.40	47.0	9.28	L 583-53
2403	G1 84.1	B		02 03 08	-28 17.9	M3.5	12.80	1.50	47.0	11.16	LP 885-12 L 583-52 sep 58" 13d
2404	GJ 1044			02 10 50	-21 25.6	K7 V	9.88	1.36	47.0	8.24	LTT 1141
2405	NN 3150			02 16 11	+23 39.1	m	14.17		47.0	12.53	LTT 10787
2406	NN 3178	A		02 42 20	+44 44.4	K6	10.85	1.40	47.0	9.21	LTT 17413 Pulk 22-59
2407	NN 3179	B		02 42 22	+44 44.6	m	15.00		47.0	13.00	LTT 17412 LP 197-48 sep 18" 65d
2408	GJ 1056			03 07 13	-60 21.9	K5 V	9.35	1.22	47.0	7.71	BPM 2877
2409	NN 3236			03 32 18	+69 01.1	m	14.17		47.0	12.53	LP 54-19
2410	NN 3255			03 51 37	+16 28.3	G5	6.81		47.0	5.17	LTT 11292 comp B: G5 optical
2411	NN 3257			03 52 03	+59 29.7	G0	6.54		47.0	4.90	LTT 11294
2412	GJ 2041			05 20 12	+00 09.8	K5 V?	8.82	1.11	47.0	7.18	AG+00: 531
2413	NN 3362			05 37 27	+12 37.6	M3	11.36	1.46	47.0	9.72	

2414	Wo 9188	S wissenschaft in die schulen!	05 39 07	+15 18.8	dM0	10.61	1.46	47.0	8.97	AC+16:777-164
2415	Gl 256		06 56 07	-12 55.3	K4 V	9.15	1.16	47.0	7.51	
2416	NN 3507		08 31 59	-00 33.2	G5	7.32		47.0	5.68	
2417	NN 3551		09 16 44	-57 34.0	K7 V	9.52	1.19	47.0	7.88	CP-57:1976 LTT 3433
2418	NN 3562		09 33 57	+40 48.2	m	14.03		47.0	12.39	LP 211-22
2419	NN 3579		09 56 35	+47 26.8	m	14.09		47.0	12.45	
2420	NN 3671		11 32 09	-23 35.6	M1	11.17	1.53	47.0	9.53	LTT 4281 comp B: K: opt
2421	GJ 1149		11 43 03	+63 22.9	DC9	16.39	0.66	47.0	14.75	LP 63-267
2422	NN 3705		12 07 01	-03 16.5	DA4	13.50		47.0	11.90	WD1207-032 y = 13.53 b-y = +0.05 u-b = +0.04 -> Mv = 11.88
2423	NN 3734		12 29 56	+20 40.0	M4	12.90	1.56	47.0	11.26	Steph 1021
2424	NN 3739		12 37 16	+25 47.4	m	14.81	1.63	47.0	13.17	LTT 13593 LP 377-36 San 111
2425	NN 3746		12 43 55	-11 32.4	G5 V	6.87	0.70	47.0	5.23	LTT 4887
2426	NN 3788		13 29 08	-02 03.8	G9 V	7.36	0.78	47.0	5.72	LTT 5229
2427	Gl 525.1		13 42 50	-32 47.5	F3 IV	4.23	0.38	47.0	2.59	
2428	Gl 545.1		14 18 20	-40 09.9	K3/4 V	9.02	1.10	47.0	7.38	K3 (Kui)
2429	Gl 563.1		14 46 03	+38 40.6	dM2	9.71	1.32	47.0	8.07	
2430	Gl 591		15 34 10	+39 59.7	K3 V	7.60	0.96	47.0	5.96	ADS 9716C
2431	Gl 593	A	15 34 15	+39 58.0	K2 V	7.43	0.91	47.0	5.79	ADS 9716A V(AB) = 6.77 d(m) = 0.21

2432	GI 593	wissenschaft in die schulen	15 34 15	+39 58.0		7.60		47.0	6.00	ADS 9716B a = 0.785" P = 55.88 yr
2433	GJ 1196		15 51 38	-25 51.6	K5 V	9.28	1.24	47.0	7.64	LTT 6348
2434	NN 3933		15 59 08	+40 28.3	m	13.12		47.0	11.48	
2435	NN 3946		16 12 17	+04 59.6	m	13.53		47.0	11.89	LTT 14839 L 1130-104 LP 564-54
2436	NN 3984		16 58 39	+08 16.9	m	13.43		47.0	11.79	
2437	NN 4009		17 26 47	+37 29.6	m	13.35		47.0	11.71	LTT 15193 Wolf 750
2438	NN 4011		17 30 54	+50 27.4	m	12.74	1.47	47.0	11.10	
2439	NN 4015		17 35 30	+22 07.8	m	14.08		47.0	12.44	
2440	GI 692.1		17 41 09	+21 38.4	K0 V	7.49	0.77	47.0	5.85	
2441	GI 698		17 53 34	+18 30.4	dK8	9.22	1.18	47.0	7.58	
2442	NN 4084		18 49 37	+24 23.8	m	12.76		47.0	11.12	LTT 15549 L 1354-11 LP 391-10
2443	NN 4089		18 55 00	+46 18.6	m	13.95		47.0	12.31	
2444	NN 4111		19 26 38	+07 03.2	K7	10.71	1.41	47.0	9.10	LTT 15688 L 1140-40 LP 572-18
2445	NN 4141		20 12 37	-39 38.5	K1 V	7.77	0.86	47.0	6.13	LTT 8014 V, B-V from Geneva, CPC
2446	NN 4167		20 49 02	+52 42.4	K5	9.74	1.32	47.0	8.10	LTT 16100
2447	NN 4179		21 02 56	-17 06.8	K7	10.33	1.42	47.0	8.69	Steph 1853
2448	NN 4196		21 25 28	+33 48.5	m	11.15		47.0	9.51	LTT 16275 L 1506-10 LP 286-3
2449	NN 4208		21 36 06	+52 51.3	M0	10.60	1.41	47.0	8.96	LTT 16322

2450	NN 4218	S	21 43 24	+20 33.0	m	14.39	1.68	47.0	12.75	
2451	NN 4249		21 59 52	-50 52.8	M4	12.09	1.57	47.0	10.45	LTT 8822 L 283-3 Sm 100
2452	NN 4268	A	22 14 01	+54 25.3	K1 V	7.51	0.81	47.0	5.87	LTT 16519 ADS15797
2453	NN 4269	B	22 14 10	+54 24.9	m	14.00		47.0	12.00	sep 78" 106d
2454	NN 4297		22 45 32	+31 36.2	m	12.91		47.0	11.27	L 1509-40 LP 344-44
2455	NN 4299	1	22 48 17	+35 55.7	m	12.00		47.0	10.00	LP 289-12
2456	NN 4308	A	22 57 51	-24 13.0	M1:	11.57	1.53	47.0	9.93	LTT 9310 L 718-71 Steph 1681 is comp B (NLTT) !?
2457	NN 4309	B	22 57 54	-24 14.0	M2	11.61	1.55	47.0	9.97	LTT 9315 L 718-70 Steph 1682 sep 75" 324d
2458	GI 894.1		23 15 56	+46 00.8	M0.5	10.90	1.45	47.0	9.26	
2459	NN 4336		23 23 59	+11 52.8	m	12.63		47.0	10.99	LTT 16893 L 1223-62 LP 522-49
2460	NN 4342		23 32 56	+29 47.4	m	13.21		47.0	11.57	LTT 16945 L 1440-32 LP 346-49
2461	NN 4363		23 46 42	+09 49.3	dM4 :	13.57		47.0	11.93	LTT 17016 Rob 379
2462	NN 4365		23 47 23	+29 17.8	DA9	15.72	0.58	47.0	14.08	
2463	NN 4377		23 53 35	-39 19.7	K3 V	8.21	0.96	47.0	6.57	LTT 9795
2464	NN 4382		23 55 34	+50 10.0	dG2	6.64	0.66	47.0	5.00	LTT 17065
2465	GI 106.1	A	02 40 42	+03 01.6	A3 V	3.56	0.09	46.9	1.92	BS 804 ADS 2080 GAM Cet V(AB) = 3.47 d(m) = 2.73

2466	Gl 106.1	B	02 40 42	+03 01.6	dF3	6.30		46.9	4.70	sep 2.8"
2467	Gl 147.1		03 37 49	-03 22.5	F9 V	6.68	0.54	46.9	5.04	LTT 1734
2468	Gl 225.1		05 58 12	-37 03.6	G5 V	8.60	0.63	46.9	6.96	
2469	Gl 501.1		13 08 18	+36 12.0	F5 IV	8.16	0.58	46.9	6.50	RS Cvn
2470	Gl 503.3		13 13 16	-19 40.7	K1 IV	5.22	1.03	46.9	3.60	
2471	GJ 1198		16 05 31	-10 17.3	M2	14.70	1.70	46.9	13.06	
2472	Gl 747.1		19 06 29	-14 49.4	M3	12.02	1.50	46.9	10.38	Ross 727
2473	GJ 1027		01 01 14	+04 48.3	DA6	13.96	0.31	46.8	12.31	
2474	Gl 120		02 54 43	+10 35.8	dM4	13.03	1.56	46.8	11.38	AC+10:22- 181 Ross 791 LFT 242
2475	Gl 402.1		10 49 29	+00 06.5	dK8	10.20	0.90	46.8	8.60	
2476	GJ 1250		20 06 21	+33 09.0	m	14.88	1.82	46.8	13.23	
2477	GJ 1100		07 44 46	-13 48.6	M1	11.50	1.41	46.7	9.85	Ross 391
2478	Gl 379.1	A	10 07 22	-35 36.7	F8 V	6.15	0.60	46.7	4.50	
2479	Gl 379.1	B	10 07 22	-35 36.7		10.90		46.7	9.20	
2480	Gl 540.1		14 09 54	-27 01.6	K2 III	5.09	1.15	46.7	3.40	
2481	Gl 699.2		17 57 50	-03 41.3	F3 V	4.62	0.38	46.7	3.00	ZET Ser
2482	NN 3024		00 14 54	-09 01.0	M0	12.49	1.57	46.6	10.83	LTT 137 L 866-24 LP 704-74
2483	Gl 84.3		02 04 21	+23 13.6	K2 IIIab	2.00	1.15	46.6	0.34	ALF Ari
2484	NN 3437		07 14 35	+19 39.9	m	12.80	1.56	46.6	11.14	LTT 17957
2485	Gl 291.1		07 49 42	-50 10.7	K2	10.06	1.22	46.6	8.40	
2486	Wo 9473		14 13 23	-05 45.8	F6 III	4.08	0.52	46.6	2.42	LTT 5603
2487	NN 4030		17 48 12	+23 46.2	M4.5-5	13.50	1.61	46.6	11.84	LTT 15285 LFT 1379 LP 389-21 L 1351-12
2488	Gl 825.1		21 14 47	-61 33.4	G5 V	6.60	0.68	46.6	4.94	
2489	Gl 4.1	A	00 03 38	+58 09.5	G5 V	6.43	0.64	46.5	4.77	ADS 61AB V (AB) = 5.99 d (m) = 0.83

2490	GI 4.1	B	00 03 38	+58 09.5	dG8	7.20	0.78	46.5	5.54	a = 1.432" P = 106.83 yr
2491	Wo 9127		03 41 23	+24 36.6	G3	11.09	0.86	46.5	9.43	HZ 320 TR113
2492	GI 458.1	AB	12 09 57	-02 48.7	G4 V	7.43	0.71	46.5	5.77	faint comp. 2" in 5d, m = 12, C&L Rv = + 14.11 +- .18 (4)
2493	NN 4037		17 54 48	+58 24.0	m	17.98		46.5	16.32	LP 102-320
2494	GI 694.2		17 44 11	+46 52.4	dM1.5	10.72	1.49	46.4	9.05	
2495	GI 709		18 15 05	+45 32.0	dM0	10.28	1.47	46.4	8.61	
2496	GI 31.3		00 42 16	-22 16.8	F2 V	5.23	0.34	46.3	3.60	
2497	GJ 1047	A	02 17 59	+36 39.8	m	14.05	1.68	46.3	12.38	V(AB) = 13.30 d(m) = 0.0
2498	GJ 1047	B	02 17 59	+36 39.8	m	14.05		46.3	12.38	sep(AB) 1"
2499	GJ 1047	C	02 17 57	+36 39.5	m	14.26	1.70	46.3	12.59	sep 32" 233d
2500	GI 301.1		08 15 05	+30 46.1	K4 V	8.85	1.14	46.3	7.18	
2501	Wo 9343		10 58 50	+56 39.1	A1 V	2.37	-0.02	46.3	0.70	
2502	GI 6		00 06 06	+36 21.0	F8 IV	6.21	0.49	46.2	4.53	
2503	NN 3329		05 03 39	-17 27.3	DC9?	15.97	0.74	46.2	14.29	LP 777-1
2504	GI 624.1	A	16 23 18	+61 37.6	G8 III	2.74	0.91	46.2	1.10	ETA Dra
2505	GI 624.1	B	16 23 18	+61 37.6	K2	8.80		46.2	7.10	
2506	GI 268.1		07 11 08	-46 40.5	F0 IV	4.48	0.32	46.1	2.80	I Pup
2507	GI 611.2		16 03 58	+80 45.8	K0	7.57	1.06	46.1	5.89	giant (Tokovinin Sov. Astr. Lett 16, p 24, 1990)
2508	Wo 9661		19 31 39	+07 16.3	K3 IIIb	4.45	1.17	46.1	2.77	LTT 15709
2509	NN 3012		00 08 42	+58 04.5	K7	9.48	1.22	46.0	7.79	LTT 10057
2510	GJ 1008		00 16 33	-10 14.3	K7 V	9.94	1.33	46.0	8.25	

2511	NN 3043		00 33 49	+08 36.0	G5	7.87		46.0	6.18	
2512	GJ 1022		00 47 18	-61 17.7	M6	12.16	1.46	46.0	10.47	LTT 471 L 123-30 Sm 176
2513	NN 3090		01 19 37	-46 58.5	M3	11.36	1.44	46.0	9.67	BPM 30654 SM 186 CFS 383
2514	NN 3091	A	01 19 46	-27 09.1	K2 V	8.30		46.0	6.60	LTT 751
2515	NN 3092	B	01 19 48	-27 10.0	m	14.85		46.0	13.16	LP 883-221 PS 187 sep 57" 147d 3
2516	NN 3132		02 01 57	-02 06.8	m	13.90		46.0	12.20	
2517	Gl 113	AB	02 45 12	+26 51.7	K1 Ve	7.61	0.83	46.0	5.92	
2518	Gl 113	C	02 45 12	+26 52.0	m	16.50		46.0	14.80	LP 354-414 sep(AB-C) 20" 20d (NLTT)
2519	GJ 1054	A	03 05 49	-28 24.4	K7 V	10.24	1.41	46.0	8.55	LTT 1479
2520	GJ 1054	B	03 05 47	-28 25.5	m+	13.09	1.64	46.0	11.40	LTT 1477
2521	GJ 1069		04 12 40	-04 32.5	K5 V	9.39	1.22	46.0	7.70	
2522	NN 3272		04 16 37	-49 10.5	M4	13.20		46.0	11.50	LTT 1935 L 302-94
2523	NN 3273		04 18 46	+51 49.6	G5	7.73		46.0	6.04	
2524	GJ 1071		04 32 26	-43 37.6	K5 V	8.86	1.11	46.0	7.17	BPM 31946
2525	NN 3324		05 00 48	+24 54.3	G8 V	7.44	0.80	46.0	5.75	
2526	Gl 189.2		05 06 15	-04 31.2	F2 V	5.11	0.44	46.0	3.42	
2527	GJ 2043	A	05 26 35	+15 32.3	dM2	10.63	1.47	46.0	8.94	LP 412-213 BPM 85872
2528	GJ 2043	B	05 26 34	+15 32.4	m	14.68		46.0	12.99	LP 417-212
2529	NN 3390		06 11 54	+19 10.5	F6 V	5.20	0.44	46.0	3.51	LTT 11815 ADS 4842 optical

2530	NN 3399	S	06 36 56	+28 38.2	k-m	11.93	1.50	46.0	10.20	LTT 11891 L 1389-16 LP 307-8
2531	NN 3400	A	06 37 28	-61 29.3	G0 V	6.34	0.62	46.0	4.65	BS 2468 V (AB) = 6.18 d (m) = 2.0
2532	NN 3401	B	06 37 28	-61 29.3		8.30		46.0	6.60	sep = 2.1"
2533	NN 3432		07 08 16	+52 21.7	M0	11.29	1.48	46.0	9.60	
2534	Wo 9231	A	07 15 13	+16 37.9	A3 V	3.58	0.11	46.0	1.89	
2535	Wo 9231	B	07 15 13	+16 37.9		10.00		46.0	8.00	sep 9.6" 33d d(m) = 6.24
2536	NN 3449	A	07 29 42	-08 46.3	F9 V	5.90	0.54	46.0	4.21	BS 2883
2537	NN 3450	B	07 29 42	-08 46.3		8.60		46.0	6.90	cpm with ADS 6158 ? sep 23.4"
2538	NN 3464		07 49 45	+26 03.5	K4	8.60	1.04	46.0	6.91	Steph 665
2539	NN 3515		08 47 13	+53 05.1	m	15.40	1.78	46.0	13.70	
2540	NN 3525		08 57 34	-27 37.2	G5 V	6.87	0.69	46.0	5.18	
2541	NN 3576		09 55 19	+12 02.9	m	14.66		46.0	12.97	LTT 12663
2542	GJ 2077		09 59 08	+14 55.9	DC7	15.37	0.36	46.0	13.68	LTT 12680
2543	NN 3583		10 00 58	+06 12.4	m	13.17		46.0	11.48	LTT 12693
2544	NN 3589		10 11 45	+21 25.1	F9 V	6.03	0.55	46.0	4.34	
2545	NN 3593		10 15 50	+44 18.2	G5 V	6.65	0.66	46.0	4.96	LTT 12759
2546	NN 3594		10 16 06	-26 14.9	K0 V	7.94	0.94	46.0	6.25	
2547	G1 398.1		10 34 03	-11 57.7	F7 V	5.71	0.52	46.0	4.02	
2548	NN 3631		10 49 41	+06 11.1	m	14.40		46.0	12.70	

2549	NN 3646		11 08 03	+48 13.7	m	14.52		46.0	12.83	
2550	GI 454.3		11 59 47	+43 25.1	K0 V	8.38	1.15	46.0	6.70	
2551	NN 3706		12 07 07	+40 31.9	K0 V	7.47	0.79	46.0	5.78	LTT 13378
2552	GJ 1155	A	12 14 20	+03 14.6	sdM3	13.28	1.62	46.0	11.59	LP 554-64
2553	GJ 1155	B	12 14 20	+03 14.6	DA s	15.32	0.38	46.0	13.63	
2554	GI 468		12 25 55	-18 01.1	K4 V	9.22	1.24	46.0	7.53	uncertain comp 35" (Worley)
2555	NN 3730		12 26 58	+23 16.4	dM5	14.18	1.60	46.0	12.49	LP 377-100 San 85
2556	NN 3745		12 43 32	+53 11.7	m	14.42		46.0	12.73	LP 13-055
2557	Wo 9428		13 05 57	+17 14.3	M0	11.80	1.55	46.0	10.11	AC+17:478- 60
2558	NN 3772		13 11 36	+04 09.8	m	13.48	1.64	46.0	11.79	LTT 18300
2559	GJ 1170		13 15 41	+36 34.0	dM2	11.29	1.41	46.0	9.60	
2560	NN 3787		13 27 23	-51 47.7	m	13.10		46.0	11.40	LTT 5212 L 257-54
2561	GI 535		13 57 00	+23 06.7	dM0 p	9.03	1.16	46.0	7.34	
2562	NN 3850		14 26 37	+12 20.6	G5	8.38		46.0	6.69	
2563	NN 3917		15 45 38	+01 43.6	G8 V	7.43	0.81	46.0	5.74	LTT 14685
2564	NN 3922		15 48 57	+74 34.2	K5	9.31	1.18	46.0	7.62	LTT 14698
2565	NN 3964		16 32 35	-30 44.5	M3.5	12.68	1.54	46.0	11.00	LTT 6625 L 555-14 LP 918-1
2566	GI 635.1		16 40 41	+79 00.8	gG9	6.32	1.14	46.0	4.60	
2567	NN 4035		17 53 44	+04 50.4	dK8	8.00		46.0	6.30	AG+04:2218
2568	GI 747.2		19 07 04	+33 58.8	dK6	9.43	1.24	46.0	7.74	
2569	NN 4127		19 51 39	+34 00.4	m	11.63		46.0	9.94	LTT 15815 L 1501-20 LP 282-7
2570	GJ 1246		19 53 26	-31 28.2	K4 V	8.43	0.98	46.0	6.74	LTT 7876

2571	NN 4223	S	wissenschaft in die schulen	21 45 58	+50 00.3	M4	13.00		46.0	11.30	LTT 16375 Wolf 945
2572	Gl 839			21 51 55	+41 32.8	dM1	10.35	1.36	46.0	8.66	AC+41:915- 440
2573	Gl 851.5			22 12 14	+27 35.9	dM0.5	10.35	1.46	46.0	8.66	AC +27:66379
2574	NN 4275			22 20 30	+27 46.7	m	14.06		46.0	12.37	
2575	Wo 9784			22 26 21	+18 40.6	dM0	10.75	1.48	46.0	9.06	LTT 16590
2576	Wo 9802			22 50 41	-48 51.8	G3 IV	6.03	0.62	46.0	4.30	LTT 9249
2577	GJ 1282			23 13 58	-62 16.4	F7 V	5.66	0.51	46.0	3.97	BS 8843
2578	NN 4325			23 14 57	-48 35.0	m	13.70		46.0	12.00	LFT 1779 LTT 9467 L 359-91
2579	NN 4332			23 17 24	-60 20.0	M2	10.99	1.45	46.0	9.30	LTT 9494 BPM 15510 L 168-9 Sm 133 R-I = 1.03 Weistrop
2580	GJ 1121			09 06 14	+40 18.7	m	14.55	1.82	45.9	12.86	
2581	GJ 1159	A		12 26 58	+53 49.2	m	14.21	1.55	45.9	12.52	LP 130-225
2582	GJ 1159	B		12 26 58	+53 49.5	M5.5-6	18.00		45.9	16.30	LP 130-226 sep 21" 356d (NLTT)
2583	Gl 748.2	A		19 12 26	+02 04.3	K4	10.20	1.19	45.9	8.51	
2584	Gl 748.2	B		19 12 26	+02 04.3	k-m	11.17	1.36	45.9	9.48	Ross 651 sep 9" 176d (NLTT)
2585	Gl 634.1			16 38 31	-02 45.3	dG2	7.22	0.64	45.8	5.52	
2586	Gl 816.1	A		21 00 53	+45 41.1	K25 V	7.68	0.97	45.8	5.98	
2587	Gl 816.1	B		21 00 53	+45 41.1		13.00		45.8	11.30	
2588	Gl 863.1	A		22 30 50	+53 32.1	dM1 J	10.84	1.36	45.8	9.14	V(AB) = 10.09 d(m) = 0.0

2589	GJ 863.1	B	22 30 50	+53 32.1		10.84		45.8	9.14	sep 0.5" 296d (1962); comp C optical
2590	GJ 1017		00 39 45	-52 38.5	m	12.25		45.7	10.50	
2591	GJ 838.5		21 50 34	-13 47.3	F1 III	5.08	0.37	45.7	3.38	MU Cap
2592	GJ 276		07 28 18	+14 43.5	dK8	8.98	1.10	45.6	7.27	
2593	GJ 337	A	09 09 34	+15 11.9	K0 V J	7.25	0.73	45.6	5.54	V(AB) = 6.50 d(m) = 0.0
2594	GJ 337	B	09 09 34	+15 11.9		7.30		45.6	5.60	a = 0.126" P = 2.65 yr
2595	GJ 419		11 11 27	+20 47.9	A4 V	2.56	0.12	45.6	0.90	DEL Leo
2596	Wo 9429		13 06 19	+05 29.0	G5 IV	6.80	0.67	45.6	5.10	LFT 969
2597	NN 3862		14 35 54	+18 30.9	gK2	5.91	1.10	45.6	4.20	
2598	GJ 1197		16 05 09	+26 58.6	m	13.33	1.64	45.6	11.62	
2599	Wo 9674		19 54 30	+51 08.1	M2	12.00		45.6	10.30	LFT 1505 LTT 15835 Wolf 1122
2600	GJ 268.4		07 14 19	-40 56.6	G3 V	9.09	0.66	45.5	7.40	
2601	GJ 392.1		10 25 10	+82 48.9	F2 V	5.26	0.37	45.5	3.60	
2602	Wo 9491		14 40 25	-05 26.5	F2 III	3.88	0.38	45.5	2.17	LTT 5845
2603	NN 4388		23 59 21	-37 30.5	K1 III	7.06	1.06	45.5	5.40	
2604	GJ 155.2		03 50 44	+61 01.4	K0 V	7.86	0.83	45.4	6.15	
2605	GJ 1112		08 27 32	+32 52.4	DA7	15.72	0.30	45.4	14.01	
2606	GJ 836.1		21 36 15	-27 31.9	G4 IV-V	6.73	0.62	45.4	5.02	
2607	GJ 575.1		15 02 15	+29 40.4	k-m	12.75	1.53	45.3	11.03	
2608	NN 3952		16 19 32	+01 08.7	F0 V	4.82	0.34	45.3	3.10	
2609	NN 3230	A	03 27 37	+19 56.0	G5	8.32	0.74	45.2	6.60	Hy 3

2610	NN 3231	S	wissenschaft in die schulen	03 27 37	+19 56.0	dK6	10.75	1.42	45.2	9.03	sep 20.2" 147d (IDS), identical with YPC 727.01 ?
2611	NN 3351			05 29 12	+79 31.0	m	18.40		45.2	16.68	LP 16-36 see Dawson & de Roberts AJ 98 p 1472 (1989)
2612	Gl 336.2	A		09 09 03	-45 06.2	K0 V	9.78	0.78	45.2	8.06	V(AB) = 9.26 d(m) = 0.5
2613	Gl 336.2	B		09 09 03	-45 06.2	K0 V	10.30	0.91	45.2	8.58	L 317-002 sep 9.0" 281d (1913- 1955)
2614	Gl 56.1			01 15 47	-13 09.2	M3	11.76	1.47	45.1	10.03	AC-14:789- 106
2615	NN 3158			02 25 30	+02 58.0	m	17.46	2.06	45.1	15.73	LP 590-137
2616	NN 3245			03 39 42	+12 22.9	M0.5	12.91	1.54	45.1	11.18	LTT 11223 Wolf 1057
2617	Wo 9132			03 45 08	+23 59.4	F6 V	9.24	0.54	45.1	7.50	HZ 1726
2618	NN 3797			13 38 13	+47 28.1	m	15.30	1.73	45.1	13.57	USNO 735
2619	GJ 1290			23 41 48	+21 19.3	m	13.30	1.59	45.1	11.57	
2620	NN 3022			00 14 21	+19 47.2	m	13.77		45.0	12.04	LTT 10097 L 1226-7 LP 404-66
2621	NN 3030			00 19 16	+48 56.0	m	12.84		45.0	11.11	LP 149-56
2622	GJ 1016			00 39 05	-33 53.9	k	10.60	1.40	45.0	8.87	BPM 46556
2623	NN 3068			00 57 38	+66 40.8	m	13.28		45.0	11.55	LP 51-17
2624	NN 3096			01 20 24	-26 04.0	m	13.05		45.0	11.32	PS 190
2625	NN 3111			01 41 29	-24 06.3	m	13.28		45.0	11.55	GR 316 PS 279

2626	NN 3144	S	wissenschaft in die schulen	02 13 12	+39 37.6	DA6	14.54	0.23	45.0	12.81	GD 25
2627	GI 92.2			02 15 00	+44 02.4	M3	13.49	1.53	45.0	11.80	L 1592-001
2628	GI 100.1			02 27 39	+05 02.6	DA3	12.79	-0.04	45.0	11.06	AC+05:19- 98 Feige 22
2629	NN 3174			02 36 37	+07 15.5	m	14.27		45.0	12.54	LTT 17400
2630	NN 3175			02 37 46	-09 40.0	F8 V	5.78	0.52	45.0	4.05	
2631	NN 3176			02 40 55	-39 08.8	M3.5	13.10		45.0	11.40	LTT 1323 L 442-72
2632	NN 3189			02 55 46	-13 05.5	M2.5	12.67	1.73	45.0	10.90	LTT 1415 L 802-6 LP 711-32
2633	NN 3194	A		03 00 03	+61 31.2	G4 V	6.62	0.63	45.0	4.89	LTT 10990 LFT 252
2634	NN 3195	B		03 00 37	+61 33.1	M3	12.60		45.0	10.90	LTT 10995 LFT 253 V Ma sep 266" 65d (NLTT)
2635	NN 3219	A		03 19 27	+26 58.7	K7	11.03	1.43	45.0	9.30	LP 355-64
2636	NN 3220	B		03 19 48	+26 58.0	a	18.00		45.0	16.00	LP 355-65 sep 278" 98d
2637	GI 150.2			03 41 16	+45 52.8	K0	7.71	0.86	45.0	5.98	
2638	NN 3251			03 46 07	+63 18.5	M3	11.39	1.42	45.0	9.66	
2639	NN 3287			04 23 23	+59 28.8	m	14.45		45.0	12.72	
2640	NN 3310			04 41 28	+29 43.9	k-m	13.45	1.60	45.0	11.70	LTT 11503
2641	NN 3352			05 30 13	+51 11.1	M3	11.07	1.46	45.0	9.34	
2642	NN 3368			05 45 41	+07 44.9	m	14.19		45.0	12.46	LTT 17868
2643	NN 3381			05 59 43	+47 48.8	M3.5	13.94		45.0	12.21	LTT 11766 LFT 446 Wolf 261
2644	NN 3394			06 22 47	-28 45.0	G0 V	6.39	0.62	45.0	4.66	BS 2318 LTT 2547

2645	NN 3486		08 10 10	-83 05.1	m	12.55		45.0	10.82	LTT 3077 L 15-97
2646	Wo 9258		08 10 25	-07 03.1	K0	7.93	0.90	45.0	6.20	
2647	GI 308.1		08 25 39	+61 54.2	dM0	10.33	1.37	45.0	8.60	AC +62:18836
2648	Wo 9273		08 35 24	-06 37.9	G0	6.75	0.66	45.0	5.02	LTT 3193
2649	NN 3513		08 41 57	-10 12.9	m	14.00		45.0	12.30	LP 726-6
2650	GJ 1115		08 50 40	+35 25.0	dM0	9.30	1.14	45.0	7.57	
2651	NN 3534		09 05 21	+51 48.5	A m	4.48	0.27	45.0	2.75	BS 3619
2652	NN 3539		09 09 02	+49 24.9	G5	7.68		45.0	5.95	
2653	Wo 9299		09 27 07	-05 09.2	K7	9.74	1.31	45.0	8.01	LTT 3488
2654	GJ 1126	A	09 28 20	-31 53.2	K3 V	8.38	0.98	45.0	6.65	LTT 3494 L 534-025
2655	GJ 1126	B	09 28 20	-31 53.2	g	13.08	1.46	45.0	11.35	LP902-30
2656	GI 368.1	A	09 47 02	-52 23.1	K1 V	7.93	0.90	45.0	6.20	V(AB) = 7.92 d(m) = 4.1
2657	GI 368.1	B	09 47 02	-52 23.1		12.00		45.0	10.30	sep 1.4" 277d (1929- 43)
2658	NN 3577	A	09 56 13	+44 05.0	m	13.89		45.0	12.16	
2659	NN 3578	B	09 56 15	+44 05.0	m	14.16		45.0	12.43	sep 23" 91d
2660	NN 3588		10 10 52	-35 29.8	M3.5	12.95		45.0	11.22	LTT 3742 L 464-6 comp B: G opt.
2661	NN 3598		10 21 40	+12 12.5	M0	12.46	1.57	45.0	10.73	Steph 852
2662	NN 3629		10 48 33	+36 23.4	m	13.46		45.0	11.73	LP 263-35
2663	NN 3648		11 09 33	-25 51.8	G8/K0 V	7.05	0.77	45.0	5.32	LTT 4131

2664	NN 3674	S	wissenschaft in die schulen	11 34 00	+39 28.3	K5	10.03	1.35	45.0	8.30	LTT 13171
2665	G1 433.1			11 34 28	+30 04.6	DA3	12.50	-0.06	45.0	10.77	AC +30:27225 GD140 LB10276 PG CBS 46
2666	G1 435.1			11 39 14	+05 25.5	K5	9.60	1.25	45.0	7.87	
2667	GJ 1150			11 44 23	+51 15.4	dM0 p	9.62	1.26	45.0	7.89	zero parallax: Heintz AJ 99
2668	G1 444	A		11 44 32	-11 32.7	dK8	9.02	1.12	45.0	7.29	
2669	G1 444	B		11 44 32	-11 32.7		14.20		45.0	12.50	
2670	NN 3694			11 53 09	-18 37.6	m	14.30		45.0	12.60	LP 793-44
2671	NN 3713			12 09 40	+49 06.0	m	12.91		45.0	11.18	
2672	GJ 1176			13 39 53	-01 25.9	K7 V	9.28	1.19	45.0	7.55	
2673	NN 3824			14 00 32	+15 12.9	G5	7.12		45.0	5.39	
2674	NN 3851			14 26 40	+46 07.8	M5.5:	16.99	2.22	45.0	15.26	LP174-340 USNO 738
2675	NN 3863			14 36 37	-74 55.5	G5 V	6.73		45.0	5.00	
2676	NN 3867			14 44 45	+02 54.8	G8 V	7.78	0.90	45.0	6.05	LTT 14377
2677	NN 3883			14 57 02	+59 46.9	dK5	10.16	1.38	45.0	8.43	uncertain comp. sep 30" (Worley)
2678	NN 3902			15 18 53	+68 01.8	m	13.44		45.0	11.71	LP 68-73
2679	NN 3915			15 44 01	-58 01.6	M2-3	11.65		45.0	9.92	LTT 6300 L 201-97
2680	NN 3935	A		15 59 54	+30 35.8	m	13.37		45.0	11.64	LP 329-20
2681	NN 3936	B		15 59 46	+30 35.9	m	15.17		45.0	13.44	LP 329-19 sep 112" 273d
2682	NN 3979			16 51 15	+40 10.2	m	13.44		45.0	11.71	

2683	GI 642	wissenschaft in die schulen	16 51 54	+11 59.5	dM1.5	10.74	1.45	45.0	9.01	AC+12:1155-87
2684	NN 3986		16 59 50	+77 47.2	m	12.67		45.0	10.94	
2685	NN 3993		17 10 14	+56 43.2	G5	6.98	0.70	45.0	5.25	
2686	NN 4008		17 26 05	-23 47.7	K5 V	9.66	1.29	45.0	7.93	CP-23: 6597 LTT 6946 V- R = 0.78 Weis
2687	NN 4018	A	17 37 32	+27 47.5	M1	11.12	1.45	45.0	9.39	LTT 15241 L 1422-16 LP 332-45
2688	NN 4019	B	17 37 33	+27 48.3	M5	12.72	1.53	45.0	10.99	LTT 15242 L 1422-15 LP 332-46 sep 57" 21d
2689	NN 4057		18 23 01	+24 36.6	M0	10.79		45.0	9.06	LTT 15449
2690	NN 4061		18 29 49	+79 23.0	K5	9.28	1.18	45.0	7.55	LTT 15472
2691	GI 718		18 31 12	+22 16.9	K4 V	8.89	1.12	45.0	7.16	V774 Her
2692	NN 4077		18 45 11	-14 38.1	k	12.13	1.51	45.0	10.40	LTT 7452 L 850-59 LP 751-15
2693	NN 4082		18 48 35	-57 09.8	M2	12.14	1.47	45.0	10.41	LTT 7481 L 207-33 Sm 23
2694	GI 775.1		20 00 17	+15 27.6	G8 V	7.16	0.71	45.0	5.43	
2695	NN 4137		20 07 54	-25 43.4	m	14.98		45.0	13.25	LP 870-45
2696	NN 4144		20 17 13	+07 51.0	m	12.92		45.0	11.19	LTT 15948 L 1142-58 LP 575-38
2697	NN 4148		20 31 31	+23 11.8	m	12.93		45.0	11.20	LTT 16001 L 1359-22 LP 395-15
2698	GI 811		20 53 49	-26 29.3	F8 V	5.70	0.50	45.0	3.97	

2699	NN 4191	S	wissenschaft in die schulen	21 15 48	-56 03.0	DA6	14.28	0.26	45.0	12.55	LTT 8452 L 212-19 BPM 27273 WD2115- 560
2700	GI 836.3			21 39 02	-41 21.0	K5 V	8.82	1.04	45.0	7.09	
2701	NN 4244			21 55 57	-61 10.3	K7	9.55	1.25	45.0	7.82	CP-61: 6606 Sm 95
2702	NN 4272			22 16 31	-28 38.2	m	14.80		45.0	13.07	LP 931-40
2703	GI 862.1			22 28 41	-06 48.6	F7 V	6.14	0.56	45.0	4.41	
2704	NN 4283			22 32 14	+03 47.0	dM4 :	12.68		45.0	10.95	LP 580-33 BPM 97396 Rob 324 ident. with LTT 16621 = L 1077-11 ?
2705	NN 4304	A		22 53 24	+05 29.5	dM0	11.26	1.45	45.0	9.53	LTT 16738 L 1150-65 LP 581-36 BPM 97728 Rob 348
2706	NN 4305	B		22 53 23	+05 29.6	DB	15.70		45.0	14.00	LP 581-35 sep 17" 286d
2707	NN 4344			23 33 00	-16 34.3	DA	13.34	0.13	45.0	11.61	GD 1192 BPM 82958
2708	NN 4369			23 48 23	+38 13.1	m	14.18		45.0	12.45	LP 291-24
2709	NN 4373			23 51 38	+51 24.4	m	13.52		45.0	11.79	
2710	GI 85.1			02 07 07	+35 12.0	M3	13.74	1.48	44.9	12.00	Ross 17
2711	GI 176.2			04 40 29	+27 35.9	K3	8.00	0.90	44.9	6.26	other SpT: K5 III OP
2712	GI 200.1			05 16 48	-53 43.6	k	13.19	1.16	44.9	11.45	L 233-030
2713	NN 3393			06 21 39	+56 12.5	m	14.55	1.76	44.9	12.81	
2714	GI 683.1			17 34 18	-42 32.0	G5 V	7.17	0.65	44.9	5.43	
2715	GI 119	A		02 52 50	+55 14.5	M1	10.48	1.39	44.8	8.74	AC +55:19224 Ross 364 LFT 240

2716	Gl 119	B	02 52 50	+55 14.8	M3	11.65	1.42	44.8	9.91	AC +55:19225 Ross 365 LFT 241 sep 17" 22d (LHS)
2717	Gl 148		03 38 34	+03 27.3	dM0 p	9.59	1.37	44.8	7.85	
2718	Gl 174.1	A	04 38 57	-41 57.5	F2 V	4.44	0.34	44.8	2.70	ALF Cae
2719	Gl 174.1	B	04 38 57	-41 57.5		12.50		44.8	10.80	
2720	NN 3392		06 18 05	+06 46.7	DA9	16.37	0.55	44.8	14.63	
2721	GJ 1110		08 25 20	+20 18.9	g-k	13.08	1.48	44.8	11.34	
2722	NN 3798		13 39 00	+30 17.0	m	15.83	1.75	44.8	14.09	LP 323-239 USNO 736
2723	Gl 524.1		13 42 30	-04 22.1	dM1	10.53	1.34	44.8	8.79	
2724	Gl 794.1		20 34 04	-47 28.0	K0 III	3.11	1.00	44.8	1.40	ALF Ind
2725	Gl 375.1		09 57 02	-49 45.8		11.68	0.91	44.7	9.90	CF 7007
2726	NN 3635		10 56 24	+30 31.5	m	15.36	1.75	44.7	13.61	
2727	Gl 457		12 09 36	+59 12.3	dM0	10.04	1.28	44.7	8.29	
2728	GJ 1255	-	20 52 04	+74 34.9	G8 V	7.80	0.70	44.7	6.05	
2729	Wo 9720		21 05 42	-21 23.7	A0 V	5.30	0.00	44.7	3.60	
2730	GJ 1152		11 49 02	+35 28.1	G7 IV	9.64	0.78	44.6	7.90	a parallax of 0.4" not confirmed by Heintz AJ 101, 1071
2731	Gl 550.2	A	14 25 37	-02 00.3	G2 IV	4.83	0.72	44.6	3.08	PHI Vir ADS 9273 V(AB) = 4.81 d(m) = 4.15
2732	Gl 550.2	B	14 25 37	-02 00.3	G4 V	9.00		44.6	7.20	sep 4.8" 110d (1829- 1958)
2733	Gl 756		19 19 49	+28 34.0	M1	11.53	1.41	44.6	9.78	AC +28:53670
2734	Gl 761.2		19 30 04	+00 28.2	dM0.5	10.43	1.45	44.6	8.68	

2735	Wo 9721	A	21 06 08	-04 37.8	dM2	9.44	1.13	44.6	7.69	BDS10765A
2736	Wo 9721	B	21 06 08	-04 37.8		13.40	1.63	44.6	11.65	BDS10765B sep. 25"
2737	Gl 52.2		01 04 56	+33 56.1	M3	13.35	1.59	44.5	11.59	Ross 322
2738	Wo 9124		03 41 17	+24 38.6	F8	10.66	0.66	44.5	8.90	HZ 314 TR108
2739	Gl 539.2		14 06 34	-30 41.5	M0	11.81	1.50	44.5	10.05	
2740	Wo 9518		15 15 47	-18 26.4	K5 p	10.35	1.22	44.5	8.59	LTT 6099 LFT 1190
2741	GJ 1266		22 15 04	+70 41.5	k	12.12	1.47	44.5	10.36	
2742	Gl 114.1	A	02 48 31	-53 21.3	k-m	10.72	1.51	44.4	8.96	comp B is optical
2743	Gl 167.1		04 14 43	-51 36.7	F4 III	4.25	0.30	44.4	2.50	BS 1338 GAM Dor
2744	Wo 9533		15 56 32	+27 52.7	K0 V	8.01	0.77	44.4	6.25	LFT 1237
2745	Gl 615.2	A	16 12 48	+33 59.0	F8 V	5.64	0.51	44.4	3.88	SIG Crb ADS 9979
2746	Gl 615.2	B	16 12 48	+33 59.0	G1 V	6.72		44.4	4.96	
2747	Gl 615.2	C	16 12 03	+33 53.9	M3.5	12.31	1.40	44.4	10.55	L 1490-024
2748	Gl 767.1	A	19 44 32	+33 36.6	F5 IV-V	4.99	0.47	44.4	3.23	ADS 12913 common motion: Gl 765.4
2749	Gl 767.1	B	19 44 34	+33 36.8	dK6	8.56	1.04	44.4	6.80	sep 25.8" 73d - 26.0" 70d (1832- 1953)
2750	Gl 784.2	A	20 11 32	+06 32.5	dM5	13.19	1.54	44.4	11.43	LTT 15922 L 1142-088
2751	Gl 784.2	B	20 11 29	+06 34.0	DA7	15.72	0.37	44.4	13.96	LTT 15921
2752	NN 4260		22 07 34	+40 47.1	k-m	12.57	1.49	44.4	10.81	
2753	NN 3375		05 55 52	+44 56.7	A2 IV	1.90	0.03	44.3	0.13	
2754	GJ 1091		06 45 27	+37 12.0		13.34	1.35	44.3	11.57	"near G87-8"
2755	GJ 1201		16 25 30	+09 19.3	DA s	16.13	0.38	44.3	14.36	

2756	NN 4174	S	wissenschaft in die schulen	20 57 17	+37 44.1	K5	8.00	1.67	44.3	6.20	
2757	Wo 9779			22 19 04	-01 38.4	A0 V	3.84	-0.05	44.3	2.07	
2758	Gl 336.1			09 08 11	+46 49.4	dM0	10.94	1.44	44.2	9.17	AC+47:2368-79
2759	Gl 604.1			15 56 52	-45 18.6	G5 IV	7.54	0.74	44.2	5.80	
2760	Gl 673.1			17 23 19	-24 07.9	A9 V	4.17	0.28	44.2	2.40	
2761	GJ 1104			07 50 22	+30 45.7	G2 VI	8.30	0.61	44.1	6.52	
2762	Wo 9578			16 44 21	+56 52.2	F2 V	4.85	0.38	44.1	3.10	
2763	Wo 9735			21 17 23	-51 15.4	G5	10.64	0.81	44.1	8.90	LTT 8473
2764	NN 3007			00 05 26	+07 44.0	M3.5	13.07	1.52	44.0	11.29	LTT 10037 LP 524-65 L 1082-25
2765	NN 3013			00 09 12	-35 24.8	F4 V	5.25	0.44	44.0	3.47	LTT 79
2766	NN 3044			00 35 28	+52 03.6	M0	10.48	1.42	44.0	8.70	
2767	NN 3073			01 00 28	+31 24.9	m	13.64		44.0	11.86	LP 294-40
2768	Gl 57.1	A		01 20 33	-13 13.6	K0 IV	7.85	0.90	44.0	6.07	
2769	Gl 57.1	B		01 20 31	-13 13.1	dK7 J	10.38	1.38	44.0	8.60	LP 707-104 L 795-25 sep (A-BC) 42" 316d; V(BC) = 10.29 d(m) = 2.7
2770	Gl 57.1	C		01 20 31	-13 13.1		13.10		44.0	11.30	sep (BC) 1.6" (1942)
2771	NN 3145			02 13 22	-12 54.5	M3	13.00	1.50	44.0	11.20	LTT 1159 LFT 197 L 800-18 LP 709-62
2772	Gl 91.2	A		02 13 25	-18 28.2	K3 V	8.42	1.02	44.0	6.64	ADS 1733 V (AB) = 7.95 d (m) = 0.64
2773	Gl 91.2	B		02 13 25	-18 28.2	K	9.10		44.0	7.30	a = 2.01" 173 yr

2774	NN 3161		02 30 10	+14 48.9	F8 V	6.02	0.54	44.0	4.24	
2775	NN 3184		02 49 11	+06 01.5	dM3	13.19	1.58	44.0	11.40	LTT 17424
2776	Gl 120.1	A	02 55 02	-25 10.1	K1/2 V	8.03	0.87	44.0	6.25	ADS 2242 V (AB) = 7.36 d (m) = 0.17
2777	Gl 120.1	B	02 55 02	-25 10.1		8.20		44.0	6.40	a = 1.548" P = 137.0 yr
2778	Gl 120.1	C	02 55 01	-25 10.5	K2 V	7.83	0.95	44.0	6.05	sep(AB-C) 28.6" 224d (1954)
2779	Gl 140.1	A	03 21 43	-50 10.5	K5 V	8.47	1.13	44.0	6.69	CD-50:1015 V(AB) = 8.36 d(m) = 2.4
2780	Gl 140.1	B	03 21 42	-50 10.6	k	10.32	1.39	44.0	8.54	CD-50:1014 sep 14.7" 234d
2781	Wo 9205		06 10 18	+70 48.2	dG7	7.43	0.77	44.0	5.65	LTT 11803
2782	Wo 9209	A	06 15 37	-59 11.4	G3 V	6.43	0.59	44.0	4.65	LTT 2510 CD-59:1274
2783	Wo 9209	B	06 15 37	-59 11.4	DB4	14.09	-0.09	44.0	12.31	LTT 2511 L 182-61 BPM 18164 sep 41" 302d (NLTT)
2784	NN 3427		07 04 06	+69 56.1	m	12.54		44.0	10.76	
2785	NN 3433		07 08 34	-14 21.5	K5	9.94	1.35	44.0	8.16	LTT 2755 Ross 55 NSV 3445
2786	NN 3440		07 21 30	-82 54.8	m	11.75		44.0	9.97	LTT 2823 L 15-86
2787	Wo 9234		07 26 09	+49 46.7	F6 V	5.36	0.45	44.0	3.58	
2788	NN 3446		07 28 56	-37 14.0	G4 V	6.64	0.63	44.0	4.86	
2789	NN 3494		08 18 08	+14 14.0	K5	9.82	1.29	44.0	8.04	LTT 12180

2790	NN 3538	S	wissenschaft in die schulen	09 07 16	+05 24.5	K4	8.38	1.01	44.0	6.60	Steph 753
2791	G1 340.3			09 18 16	-05 32.4	dK8	9.09	1.16	44.0	7.31	
2792	G1 343.1			09 24 20	+39 43.5	dK8 e	9.84	1.29	44.0	8.06	
2793	NN 3613			10 35 30	+48 47.4	m	13.49		44.0	11.71	LP 167-71
2794	GJ 1137			10 42 02	-33 18.7	K2 V	8.30	0.95	44.0	6.52	BPM 54316
2795	NN 3616	A		10 42 06	+32 40.5	m	13.55		44.0	11.77	LP 316-604
2796	NN 3617	B		10 42 08	+32 40.2	m	15.50		44.0	13.70	LP 316-605 sep 40" 123d
2797	NN 3640			11 01 29	+40 16.5	K5	10.74	1.40	44.0	9.00	LP 214-26
2798	G1 417			11 09 49	+36 05.3	G0 V	6.41	0.61	44.0	4.63	
2799	NN 3651			11 11 53	+25 58.9	K1 V	7.76	0.84	44.0	5.98	
2800	G1 423.1			11 15 47	-04 47.5	G8 V	7.29	0.73	44.0	5.51	
2801	NN 3660	A		11 22 13	+78 32.6	M2.5	12.15		44.0	10.37	LTT 13090 AC+78:3815
2802	NN 3661	B		11 22 01	+78 33.7	M3	12.65		44.0	10.87	LTT 13091 sep 74" 327d
2803	NN 3662			11 22 18	+40 16.7	dM0	10.33	1.36	44.0	8.55	AC+40:477- 39
2804	G1 439			11 42 04	+31 14.5	dK8	8.96	1.13	44.0	7.18	
2805	NN 3688			11 45 49	-11 00.5	k	12.90	1.46	44.0	11.12	LP 733-24
2806	Wo 9390	A		12 06 53	-11 34.6	G2 V	6.81	0.66	44.0	5.03	LTT 4545 NSV 5478
2807	Wo 9390	B		12 06 55	-11 34.5	K5	9.20		44.0	7.40	LTT 4546 ADS 8440 sep 11" 90d (NLTT)
2808	Wo 9393			12 08 26	+41 20.0	M2 V	10.67	1.35	44.0	8.89	AC+41:509- 35
2809	NN 3711	A		12 08 59	+53 42.1	K2	8.03	0.88	44.0	6.25	LTT 13391 ADS 8450
2810	NN 3712	B		12 08 58	+53 41.9	K3	8.23		44.0	6.45	LTT 13390 sep 12" 222d
2811	G1 459.2			12 14 14	+44 40.8	K4 V	9.18	1.50	44.0	7.40	

2812	GJ 1160	wissenschaft in die schulen!	12 28 57	+55 23.7	K2 V	8.12	0.93	44.0	6.34	
2813	NN 3741	A	12 39 16	+48 31.0	m	11.66		44.0	9.88	
2814	NN 3742	B	12 39 17	+48 31.0	m	14.80		44.0	13.00	LP 171-46 sep 6.5" 90d
2815	NN 3743		12 39 27	+55 59.9	K3 V	8.29	0.95	44.0	6.51	
2816	NN 3774		13 14 28	+23 26.0	M2	11.69		44.0	9.91	LTT 13855 L 1337-15 LP 378-924
2817	NN 3778		13 19 05	+04 01.7	m	11.90		44.0	10.10	LTT 13881 L 1049-18 LP 557-59
2818	G1 520	A	13 35 49	+48 23.6	dM0.5	10.17	1.40	44.0	8.39	ADS 8980 V (AB) = 9.77 d (m) = 0.8 ::
2819	G1 520	B	13 35 49	+48 23.6		11.00		44.0	9.20	sep 2.6" 272d - 2.6" 297d (1908- 1965)
2820	G1 520	C	13 35 38	+48 23.6	m	14.46	1.66	44.0	12.68	
2821	GJ 2108		14 25 24	-81 07.0	DA6	13.75	0.25	44.0	11.97	LTT 5712 L 19-2 BPM 784
2822	G1 554		14 28 42	+35 40.3	dK5	8.70	1.04	44.0	6.92	
2823	NN 3906		15 25 15	+10 46.3	K5	9.86	1.30	44.0	8.08	LTT 14593
2824	NN 3930		15 56 38	+25 42.8	K2 V	8.33	1.00	44.0	6.55	
2825	NN 3957		16 28 06	-03 52.9	K5	9.58	1.25	44.0	7.80	Steph 1347
2826	G1 637.1		16 42 44	+68 11.3	K1 V	7.56	0.79	44.0	5.78	
2827	NN 3974		16 47 43	+39 21.8	K4	9.75	1.27	44.0	7.97	LTT 14979
2828	NN 4064		18 33 41	+41 26.8	M2	11.78		44.0	10.00	
2829	GJ 1247		19 54 35	-55 04.3	K3 V	8.60	1.08	44.0	6.82	BPM 26450
2830	NN 4155		20 38 13	-10 17.5	M0 e	11.94	1.51	44.0	10.16	Steph 1806

2831	NN 4246	S	21 57 18	+41 37.4	m	12.76		44.0	10.98	
2832	NN 4251		22 02 01	+67 15.6	m	13.41		44.0	11.63	
2833	NN 4256		22 03 53	+39 03.7	m	12.69		44.0	10.91	
2834	G1 863.2		22 31 58	-20 57.9	F3 V	5.20	0.44	44.0	3.42	UPS Aqr
2835	Wo 9809		23 04 00	+63 39.0	dM0	10.82	1.42	44.0	9.04	AC +63:32399
2836	G1 889	A	23 04 26	-23 25.6	K5 V	9.62	1.30	44.0	7.84	LTT 9360 dM0 Wil
2837	G1 889	B	23 04 34	-23 23.8	k-m	13.65	1.65	44.0	11.87	LTT 9361 LP 877-061
2838	GJ 1280		23 07 08	-69 06.9	K4 V	8.78	1.02	44.0	7.00	LTT 9387
2839	GJ 2154	A	23 11 32	-19 55.1	K7 V	10.62	1.46	44.0	8.84	LTT 9423
2840	GJ 2154	B	23 11 32	-19 55.2	m	13.80	1.60	44.0	12.02	LP 822-105
2841	NN 4341		23 32 34	+24 58.2	M3	12.92		44.0	11.14	LTT 16939 Ross 298
2842	NN 4346		23 33 14	+41 41.3	M0	11.20	1.43	44.0	9.42	LTT 16947 LFT 1807
2843	G1 907.1	AB	23 45 50	-13 15.9	dM0	9.86	1.26	44.0	8.08	RST 4134 sep 1.5" d(m) = 1.5 , V (AB) = 9.62
2844	NN 3067		00 53 54	-28 24.5		10.96	0.96	43.9	9.20	
2845	NN 3569		09 46 55	+53 29.2	DQ6	15.20	0.13	43.9	13.41	PG
2846	G1 431.1	A	11 29 32	+61 21.6	F6 V	5.74	0.50	43.9	3.95	ADS 8197 BS 4439 V (AB) = 5.48 d (m) = 1.43
2847	G1 431.1	B	11 29 32	+61 21.6	G3 V	7.10		43.9	5.30	a = 0.813" P = 72.87 yr
2848	G1 765.4	A	19 43 39	+33 29.1	K3 V	8.35	0.99	43.9	6.56	ADS 12889 V(AB) = 7.68 d(m) = 0.19 , cpm: G1 767.1 sep 13'

2849	Gl 765.4	B	19 43 39	+33 29.1	K3 V	8.54		43.9	6.75	a = 2.048" P = 224.68 yr
2850	Gl 157.1		03 56 49	+25 57.2	dM4	12.62	1.49	43.8	10.83	Wolf 1322
2851	NN 4047		18 15 48	+26 39.0	K3	9.59	1.02	43.8	7.80	LTT 15414
2852	GJ 1249		20 03 20	+38 20.0	G5 IV	6.17	0.65	43.8	4.38	BS 7683 LTT 15881 ADS 13348 6.6-12.8 sep 12" 230d
2853	Wo 9706		20 44 07	+57 24.0	F8 IV-V	4.51	0.54	43.8	2.72	LTT 16071
2854	Wo 9787		22 30 38	-35 42.1	G8 V	7.79	0.72	43.8	6.00	LTT 9071
2855	Gl 154.2		03 43 34	-64 57.8	K0 IV	3.85	1.13	43.7	2.10	BET Ret
2856	Wo 9256		08 08 31	+32 36.9	G4 V	6.81	0.69	43.7	5.01	LFT 567
2857	Gl 310.1	A	08 33 12	+06 47.7	F8 V	5.99	0.52	43.7	4.19	
2858	Gl 310.1	B	08 33 12	+06 47.9	G5 IV-V	7.25	0.71	43.7	5.45	
2859	Wo 9574		16 38 41	-17 38.8	G7.5 II CN	4.96	1.11	43.7	3.20	
2860	Wo 9112		03 12 04	+08 48.1	K1 V	7.83	0.86	43.6	6.03	LFT 264
2861	Wo 9666		19 40 42	-15 35.3	F5 IV	5.49	0.46	43.6	3.70	LTT 7797
2862	Wo 9791		22 34 59	-65 38.5		14.00		43.6	12.00	near Gl 865; sep 13" 185d
2863	Gl 499.1		13 03 57	+22 53.0	M5 III	5.60	1.59	43.5	3.80	FS Com
2864	Wo 9648	A	19 10 48	+49 45.7	G6 V	6.57	0.65	43.5	4.76	LFT 1459
2865	Wo 9648	B	19 10 47	+49 45.6	G6 V	6.75	0.65	43.5	4.94	LFT 1460
2866	Wo 9691		20 18 04	-50 09.3	G2 IV-V	6.27	0.55	43.5	4.46	LTT 8055
2867	Wo 9713		20 57 35	-42 13.4	K4	12.30		43.5	10.50	LTT 8318
2868	Wo 9207		06 13 38	+12 17.3	F5 IV-V	5.04	0.42	43.4	3.20	LTT 11823

2869	Wo 9006	S	wissenschaft in die schulen	00 13 46	+15 38.5	m	14.80		43.3	13.00	LTT 10091 MW 412-30
2870	GJ 1015	A		00 38 28	+55 33.6	m	14.02	1.55	43.3	12.20	
2871	GJ 1015	B		00 38 29	+55 33.7	DQ5	14.08	0.02	43.3	12.26	
2872	Gl 893.2	A		23 13 16	-09 21.6	K0 III	4.22	1.11	43.3	2.40	BS 8841 PSI (1) Aqr sep (A-BC) 49.6" 312d (1836- 1938)
2873	Gl 893.2	B		23 13 14	-09 21.1	K3 V J	9.62	1.05	43.3	7.80	ADS 16633 V(BC) = 9.16 d(m) = 0.7
2874	Gl 893.2	C		23 13 14	-09 21.1		10.30		43.3	8.50	sep 0.2" 108d (1961)
2875	NN 3436			07 13 33	-12 57.8	G2 V	7.75	0.61	43.2	5.93	LTT 2776
2876	Wo 9493			14 42 54	+17 10.5	K0 III	4.60	0.98	43.2	2.78	
2877	Wo 9503			14 54 34	-04 08.6	F0 V	4.49	0.32	43.2	2.67	
2878	Wo 9531			15 53 58	+38 05.4	F0 IV	5.45	0.33	43.2	3.63	
2879	Gl 836.6	A		21 41 54	+28 31.0	F4 V	4.78	0.48	43.2	2.96	MU(1) Cyg ADS 15270 V(AB) = 4.50 d(m) = 1.33
2880	Gl 836.6	B		21 41 54	+28 31.0	G2 V	6.09		43.2	4.27	MU(2) Cyg a = 4.278" P = 507.5 yr
2881	NN 4250			22 01 00	+01 21.8		10.34	0.73	43.2	8.52	no 18 in AJ 84 p567: AC +01:2189-92
2882	NN 3037			00 29 34	-03 10.7	g-k	17.34		43.1	15.51	LP 645-46
2883	Wo 9143			04 03 34	-27 47.2	F1 IV	5.58	0.32	43.1	3.80	LTT 1864

2884	NN 3301	S	wissenschaft in die schulen 04 33 03	+16 24.6	K	11.20		43.1	9.40	ADS 3321CD sep (AC) 121.7" 33.5d; sep (CD) 1.7" 273.8d d(m) = 2.4	
2885	Gl 618.4			16 19 01	-48 31.9	M3	11.83	1.48	43.1	10.00	L 338-152
2886	NN 4023			17 39 30	-08 47.3	M3	13.52	1.61	43.1	11.69	LTT 7048 LFT 1367 Wolf 1471
2887	Wo 9641			19 01 41	-21 49.0	K0 III	3.77	1.01	43.1	1.90	
2888	Wo 9643			19 03 49	-27 44.7	K1 III	3.32	1.19	43.1	1.50	LTT 7571
2889	NN 4180			21 03 26	+04 13.8	m	12.18	1.49	43.1	10.35	LP 576-34
2890	NN 3011			00 08 31	-06 03.7	dM2	10.86	1.47	43.0	9.03	LTT 74
2891	GJ 2004			00 20 46	-33 26.8	K3/4 V	8.75	1.07	43.0	6.92	LTT 198
2892	Gl 27.1			00 37 34	-44 31.5	M0.5	11.40	1.49	43.0	9.57	
2893	NN 3054			00 43 12	-51 54.0	M3	11.91	1.48	43.0	10.08	BPM 16228 Sm 173
2894	NN 3057			00 46 06	+26 45.0	M4	12.38	1.52	43.0	10.50	LTT 17156
2895	NN 3064			00 53 20	-11 44.1	DA7	15.25	0.35	43.0	13.42	LTT 524 L 796-10 LP 706-65
2896	NN 3071			00 59 48	+04 47.4	K0	8.20	1.00	43.0	6.37	LTT 10369
2897	NN 3081			01 11 48	-37 12.9	dM2.5	13.85	1.66	43.0	12.02	
2898	GJ 1043			02 10 00	+20 58.6	F5 V	5.27	0.43	43.0	3.44	BS 646 ETA Ari
2899	NN 3159			02 25 42	+01 13.2	m	13.05		43.0	11.22	LTT 17373
2900	Gl 105.5			02 38 07	+00 58.9	dM0 p	9.52	1.20	43.0	7.69	
2901	Gl 118.1	A		02 52 00	-36 06.3	K3 V	8.23	0.93	43.0	6.40	
2902	Gl 118.1	B		02 52 00	-36 06.9	M3 :	13.10	1.52	43.0	11.27	L 442-013

2903	GJ 2028	wissenschaft in die schulen	02 55 54	-70 34.0	DA6	14.08	0.23	43.0	12.25	LTT 1419 LFT 245 L 54-005
2904	NN 3228	A	03 26 19	-15 47.7	m	14.28		43.0	12.45	LP 772-72
2905	NN 3229	B	03 26 19	-15 47.9	m	14.37		43.0	12.54	LDS 3498? LP 772-73 sep 16" 172d
2906	NN 3239	A	03 34 41	+17 41.7	g-k	12.74		43.0	10.91	LP 413-18 LDS 3512
2907	NN 3240	B	03 34 42	+17 41.5	g-k	13.29		43.0	11.46	LP 413-19
2908	NN 3260		03 58 31	-23 13.2	M0	11.47	1.48	43.0	9.64	Steph 442
2909	GI 161.1		04 05 16	+37 54.6	F7 V	5.52	0.46	43.0	3.69	
2910	NN 3265		04 07 30	+49 24.5	M3.5	13.45		43.0	11.62	LTT 11358 Ross 27
2911	NN 3288		04 23 40	+04 26.3	DC9	17.11	1.10	43.0	15.28	LP 535-11
2912	NN 3291		04 25 06	+11 40.7	k	13.85		43.0	12.02	LTT 11432
2913	NN 3297		04 30 59	+34 43.5	g-k	13.13	1.57	43.0	11.30	LTT 11455 L 1455-1 LP 250-2
2914	NN 3300		04 32 50	-35 45.4	G8 V	7.58	0.81	43.0	5.75	LTT 2036 V, B-V from CPC
2915	GJ 2035		04 50 04	+22 09.3	K5 V	8.77	1.01	43.0	6.94	AG+22:478
2916	NN 3319		04 52 15	-35 29.2	K0 V	7.60	0.77	43.0	5.77	LTT 2120 V, B-V from CPC
2917	NN 3337		05 08 03	+18 34.5	m	14.20		43.0	12.40	LTT 17752
2918	NN 3345		05 16 59	+55 43.1	m	13.01		43.0	11.18	
2919	GJ 2057		07 20 59	+13 04.1	K2	8.20	0.94	43.0	6.37	LTT 12011
2920	NN 3445		07 28 32	+39 20.2	m	13.08		43.0	11.25	
2921	GI 287		07 42 25	+02 15.7	dM0	10.20	1.37	43.0	8.37	
2922	GI 292.2		07 52 03	-01 16.8	G8 V	7.43	0.73	43.0	5.60	

2923	NN 3470	S	07 56 17	+15 31.7	m	12.33		43.0	10.50	LP 424-4
2924	NN 3475		08 00 53	+44 06.2	K5	9.83	1.27	43.0	8.00	
2925	NN 3483		08 06 24	-66 09.0	DQ5	13.92	0.05	43.0	12.09	LTT 3059 L 97-3 BPM 4834
2926	NN 3496		08 20 10	+84 34.1	m	13.42	1.62	43.0	11.59	LP 5-110
2927	NN 3516		08 47 52	+35 00.7	G0	7.60		43.0	5.77	
2928	NN 3532		09 04 24	+66 47.8	m	12.96		43.0	11.13	LP 60-205
2929	NN 3565		09 41 18	-06 49.7	DA9	16.41	0.56	43.0	14.58	
2930	NN 3597		10 21 37	-29 23.6	G5 V	6.94	0.65	43.0	5.11	
2931	NN 3608	AB	10 28 39	-21 23.1	K7 V	10.68	1.38	43.0	8.85	U235 LTT 3856 L 681- 21 DON 414 sep(AB) < 1" d(m) = 0.3 V (J) = 10.07
2932	NN 3609	C	10 28 39	-21 23.1		13.13	1.57	43.0	11.30	DON 414C sep 6" 189d
2933	NN 3619		10 43 27	+09 57.9	m	13.55		43.0	11.72	LTT 12870
2934	GI 415		11 08 43	-10 41.2	K4	9.24	1.10	43.0	7.41	
2935	NN 3656		11 19 21	+47 11.1	K6	9.80		43.0	7.97	LTT 13073
2936	NN 3664		11 25 04	+04 15.2	dM0	10.68	1.42	43.0	8.85	
2937	NN 3665		11 26 08	+48 30.3	G5	7.89		43.0	6.06	
2938	NN 3736		12 33 50	-04 06.1	M3: V	13.10	1.60	43.0	11.30	LTT 4796 L 975-27 LP 675-19 M3 Kui
2939	GI 498		13 03 29	+49 44.2	dK8	9.30	1.17	43.0	7.47	
2940	NN 3773		13 12 38	-72 52.0	m	13.05		43.0	11.22	LTT 5075 L 69-70

2941	NN 3799	S	wissenschaft in die schulen	13 39 07	+15 04.5	k-m	12.09	1.50	43.0	10.30	LTT 18344
2942	NN 3827			14 09 05	-12 22.5	K1 V	7.93	0.86	43.0	6.10	LTT 5553
2943	NN 3835			14 12 32	+10 38.9	M2	12.37	1.52	43.0	10.50	LTT 14175 L 1196-40 LP 499-54
2944	NN 3844			14 18 51	+27 49.1	m	12.62		43.0	10.79	LTT 14214 L 1412-31 LP 325-26
2945	NN 3845			14 20 19	-22 03.2	m	15.00		43.0	13.20	LP 857-29
2946	NN 3868	A		14 48 37	+09 55.7	dG5	7.40	0.76	43.0	5.57	LTT 14397
2947	NN 3869	B		14 48 37	+09 55.6	k	8.90		43.0	7.10	LTT 14398 ADS 9410 sep 8" 227d
2948	NN 3886			14 59 11	+35 39.3	M2	12.05		43.0	10.22	LTT 14457 Ross 1042
2949	NN 3908			15 28 39	-26 44.8	M3.5	13.70		43.0	11.90	LTT 6205 L 624-20 LP 860-50
2950	Wo 9541	A		16 01 41	-11 18.8	G8 V	7.46	0.74	43.0	5.63	
2951	Wo 9541	B		16 01 41	-11 18.8	K2 V	8.03	0.84	43.0	6.20	
2952	NN 3939			16 05 02	+06 06.1	m	13.46		43.0	11.63	LTT 14801 L 1130-80 LP 564-39
2953	Wo 9554			16 16 05	-50 02.1	G8 III	4.02	1.08	43.0	2.20	
2954	NN 3969			16 39 06	-05 43.5	g-k	12.06	1.50	43.0	10.20	LTT 6674 L 915-5 LP 685-43
2955	GJ 1208			16 55 01	+21 31.8	DA6	14.06	0.25	43.0	12.23	
2956	Wo 9582	A		17 02 37	+59 39.0	K4 V	8.65	1.04	43.0	6.82	LTT 15047
2957	Wo 9582	B		17 02 38	+59 39.2	K4	10.31	1.40	43.0	8.48	LTT 15048 sep 17" 44d

2958	Wo 9584	S A	wissenschaft in die schulen 17 04 17	+54 32.1	F7 V	5.63	0.47	43.0	3.80	BS 6370 ADS 10345 V(AB) = 4.93 d(m) = 0.10
2959	Wo 9584	B	17 04 17	+54 32.1	F7 V	5.73		43.0	3.90	BS 6369 a = 3.945" P = 672 yr
2960	Wo 9584	C	17 04 17	+54 32.1	M3 :	13.50		43.0	11.70	sep(AB-C) 14"
2961	Gl 665.1		17 15 04	-24 01.2	G3 V	6.59	0.62	43.0	4.76	
2962	NN 4031		17 49 15	+14 46.0	m	13.71		43.0	11.88	
2963	NN 4050		18 16 29	-45 56.5	G5 V	7.32	0.76	43.0	5.49	CP-45:9234
2964	NN 4092		18 57 13	+07 55.1	M2	10.86	1.42	43.0	9.03	LTT 15574 L 1138-44
2965	NN 4096		19 05 18	-42 30.4	K1 V	7.88	0.86	43.0	6.05	CP-42:8610
2966	Gl 756.1		19 20 14	-66 34.3	K5 V	8.40	1.04	43.0	6.57	
2967	Gl 765.1	A	19 40 29	+50 24.5	G2 V	5.96	0.64	43.0	4.13	
2968	Gl 765.1	B	19 40 32	+50 24.0	G5 V	6.20	0.66	43.0	4.37	
2969	NN 4140		20 11 47	-07 25.8	K7 V	10.20	1.34	43.0	8.37	LTT 8005 U494
2970	NN 4146		20 24 50	+27 20.9	m	12.27		43.0	10.44	LTT 15978 L 1431-22 LP 339-7
2971	NN 4150		20 33 18	+64 08.9	m	13.08		43.0	11.25	
2972	NN 4153		20 35 08	+21 46.5	M2	11.44	1.50	43.0	9.61	LTT 16019 Wolf 1351
2973	NN 4157		20 40 14	-29 36.1	G5 V	6.95	0.67	43.0	5.12	LTT 8195
2974	NN 4170		20 51 32	+68 58.7	M3	11.70	1.54	43.0	9.87	LTT 18506 AC+68:8102
2975	GJ 1259		20 52 42	+12 58.8	K3 V	8.81	1.05	43.0	6.98	
2976	Gl 825.2		21 15 11	-43 32.7	G5 V	6.75	0.63	43.0	4.92	
2977	NN 4212		21 39 46	+27 27.6	m	13.97		43.0	12.14	LP 342-14

2978	NN 4271	S	22 14 58	-36 25.9		14.20		43.0	12.40	LP 984-2
2979	G1 869		22 38 06	-32 15.1	G8 V	7.39	0.80	43.0	5.56	
2980	NN 4314		23 07 04	-02 14.5	k-m	12.66	1.54	43.0	10.80	LTT 9381 L 1007-39 LP 642-82
2981	G1 893.4		23 14 11	+19 21.0	dM0	11.16	1.49	43.0	9.33	AC+19:1079- 115
2982	NN 4321	A	23 14 14	-67 11.2	K5 V	8.73	1.05	43.0	6.90	LTT 9452 CD-67:2594 SB !?
2983	NN 4322	B	23 14 10	-67 12.3	K5 V	9.04	1.11	43.0	7.21	LTT 9451 CD-67:2593 sep 71" 199d
2984	NN 4331		23 15 50	-61 31.7	M3	11.20	1.41	43.0	9.37	Sm 132 R-I = 1.05 Weistrop
2985	Wo 9835		23 39 38	-02 50.9	dM0	10.32	1.38	43.0	8.49	LTT 9665
2986	NN 4374		23 51 54	+07 53.0	M3:	13.01	1.50	43.0	11.18	LTT 17044 LP 583-82 LE 31 Rob 382
2987	NN 3940		16 05 10	+47 38.1	dK8	9.90	1.17	42.9	8.06	
2988	Wo 9747		21 38 47	+53 46.6	M3.5	14.10		42.9	12.30	LTT 16338 LFT 1653
2989	Wo 9796		22 45 33	-51 34.8	A2 V	3.48	0.08	42.9	1.64	
2990	Wo 9423		12 52 11	-43 52.7	G1 V	5.88	0.64	42.8	4.00	LTT 4935
2991	NN 4080		18 46 42	-20 23.0	K2 III	5.24	1.41	42.8	3.40	
2992	NN 4284		22 32 17	-01 20.8	dM4	14.83	1.70	42.8	12.99	LP 640-43
2993	G1 105.6		02 39 05	+39 59.0	F9 V	4.92	0.59	42.7	3.07	
2994	GJ 1217		17 19 52	-14 54.4	K5 V	10.84	1.41	42.7	8.99	LTT 6914
2995	G1 686.2		17 36 32	-49 23.2	F2 V	4.77	0.40	42.7	2.92	LAM Ara
2996	NN 4066		18 36 26	+20 35.1	F9	9.34	0.65	42.7	7.50	LTT 15494

2997	GJ 1242	wissenschaft in die schulen!	19 39 24	+03 02.5	m	12.88	1.60	42.7	11.03	
2998	Wo 9086		02 34 06	-47 52.9	G0	11.99	0.55	42.6	10.10	LTT 1273 CFS 676
2999	Wo 9468		14 06 27	-61 16.6	G9 V	9.68	0.78	42.5	7.82	LFT 1069
3000	GI 608		15 59 53	+61 48.0	dM0	9.99	1.29	42.5	8.13	
3001	Wo 9085		02 32 49	-03 46.3	G5 IV	6.82	0.67	42.4	4.96	LTT 1267
3002	NN 3364		05 42 00	+69 44.0	m	16.47	1.69	42.4	14.61	LP 33-436
3003	NN 4171		20 55 03	+42 44.2	A2	9.00		42.4	7.10	AG+42:1955 SAO 50268
3004	Wo 9724		21 08 29	-43 48.0	M1	12.01	1.56	42.4	10.15	LFT 1610 LTT 8406 Sm 74
3005	Wo 9800	A	22 49 45	-33 08.5	A0 III	4.50	-0.04	42.4	2.60	BS 8695 V (AB) = 4.46 d (m) = 3.6 , pi (uvby) = 0.012
3006	Wo 9800	B	22 49 45	-33 08.5		8.60		42.4	6.70	sep 4.2"
3007	NN 3048		00 41 02	+23 36.9	dM0	10.97	1.34	42.3	9.10	
3008	NN 3895		15 09 40	+18 09.0	m	13.45	1.51	42.3	11.58	LTT 14519 L 1271-41 LP 442-17
3009	NN 4345		23 33 07	+05 54.3	m	16.10	1.78	42.2	14.23	LP 583-11
3010	Wo 9037		01 02 22	-39 44.9	G3 IV	7.72	0.60	42.1	5.84	LTT 610
3011	NN 3927		15 53 08	+34 00.0	m	15.95	1.76	42.1	14.07	LP 274-24 USNO 746
3012	Wo 9763		21 56 42	-04 19.6	M2 :	14.17	1.59	42.1	12.30	LTT 8788
3013	Wo 9821		23 16 08	-32 48.3	G8 III	4.41	1.13	42.1	2.50	
3014	Wo 9008		00 15 25	-13 44.0	G2 V	6.50	0.59	42.0	4.62	LTT 145

3015	NN 3031	S	wissenschaft in die schulen	00 19 37	+42 20.3	DC9	16.50	0.72	42.0	14.62	
3016	NN 3063			00 50 06	-41 31.0	M3	11.92	1.49	42.0	10.04	Sm 177
3017	NN 3074			01 04 52	-32 41.6	m	10.76	1.38	42.0	8.88	L 509-35
3018	Wo 9046			01 12 11	-42 09.5	G0 V	8.47	0.56	42.0	6.60	
3019	GI 55.2			01 13 54	+25 04.2	dK5	10.08	1.36	42.0	8.20	AC+25:4674
3020	NN 3099			01 31 17	-44 09.5	K0/1 V	7.84	0.83	42.0	5.96	LTT 851
3021	NN 3122			01 50 22	+65 55.9	G5	8.48	1.01	42.0	6.60	
3022	NN 3127			01 58 21	-10 35.5	m	14.10		42.0	12.20	LP 709-16
3023	NN 3133			02 02 35	-15 55.0	K0 V	7.78		42.0	5.90	
3024	NN 3168			02 32 55	+55 15.8	m	13.22		42.0	11.34	
3025	GI 106.1	C		02 39 54	+03 09.9	K5	10.16	1.36	42.0	8.28	
3026	NN 3188			02 51 58	+61 19.1	F4 V	5.59	0.45	42.0	3.71	BS 860
3027	GI 120.2			02 59 28	+26 24.9	G8 V	6.62	0.72	42.0	4.74	
3028	NN 3202			03 05 04	-04 09.6	dK7	10.87	1.43	42.0	8.99	LTT 1471 L 947-30
3029	NN 3216			03 15 30	+32 28.0	m	11.33	1.47	42.0	9.45	LTT 11085 LP 299-53
3030	NN 3238			03 34 21	-41 09.4	M3	13.05		42.0	11.17	LTT 1704 L 372-18 LP 995-48
3031	Wo 9119	A		03 36 39	+33 18.7	dK5	9.07	1.06	42.0	7.19	ADS 2662A
3032	Wo 9119	B		03 36 38	+33 18.8		12.87	1.49	42.0	10.99	ADS 2662B sep 15.2"
3033	NN 3246			03 40 20	-51 35.1	K4 V	9.07	1.10	42.0	7.19	CP-51:438
3034	NN 3262			04 03 26	+82 47.4	dM0	10.82	1.44	42.0	8.94	LTT 11332 AC+82:779
3035	NN 3264			04 07 15	-08 01.5	G2 IV-V	7.04		42.0	5.16	

3036	NN 3274	S	04 18 52	+21 12.9	k-m	13.03	1.56	42.0	11.10	LTT 11407 L 1310-30 LP 415-18
3037	NN 3276		04 19 24	+15 23.9	m	17.00		42.0	15.00	LP 415-1446 No 190 in Leggett & Hawkins MN 234, p 1065 (1988)
3038	NN 3282	A	04 22 32	+07 56.1	m	12.63		42.0	10.75	LDS 3584A
3039	NN 3283	B	04 22 34	+07 57.2	m	14.97		42.0	13.09	LDS 3584B
3040	NN 3359		05 35 20	+45 25.3	G5	8.08		42.0	6.20	
3041	NN 3367		05 44 44	-00 01.8	M0	10.99	1.45	42.0	9.11	Steph 578
3042	NN 3369		05 45 57	-11 09.3	M0.5	11.00	1.42	42.0	9.12	LTT 2376 L 810-58
3043	NN 3391		06 17 34	+44 16.2	m	12.27		42.0	10.39	
3044	NN 3397		06 32 45	-69 55.2	m	13.00		42.0	11.10	LTT 2392 L 59-3
3045	G1 266		07 04 32	+03 31.8	dM0	9.84	1.29	42.0	7.96	AC+03:2350- 326
3046	NN 3439		07 19 33	+30 46.5	k-m	13.34	1.50	42.0	11.46	LTT 17963
3047	NN 3471		07 56 37	+20 59.3	K0 V	7.70	0.82	42.0	5.82	LTT 12105
3048	G1 319.1	A	08 40 22	-42 44.9	K1 V	8.12	0.90	42.0	6.24	LDS 230
3049	G1 319.1	B	08 40 22	-42 45.6	M1 :	12.68	1.52	42.0	10.80	L 387-60 sep 45" 188d NLTT
3050	G1 333.2	A	08 58 11	+05 26.6	dM4	12.34	1.45	42.0	10.46	Ross 686
3051	G1 333.2	B	08 58 13	+05 26.4	dM4	12.68	1.47	42.0	10.80	Ross 687
3052	NN 3537		09 07 00	+06 54.0	M4 e	13.35	1.57	42.0	11.47	
3053	NN 3547		09 15 29	+62 16.2	m	11.28		42.0	9.40	LP 91-14

3054	NN 3584	S	wissenschaft in die schulen	10 01 56	+05 48.5	M0	12.66	1.50	42.0	10.78	Steph 823
3055	NN 3587			10 08 48	+35 33.6	M4	14.50		42.0	12.62	LTT 12734 Wolf 351
3056	Wo 9329			10 23 18	-44 38.2		11.19	0.94	42.0	9.30	
3057	NN 3623			10 45 51	+19 25.0	m	13.45		42.0	11.57	LTT 12881 L 1258-7 LP 431-69
3058	NN 3626			10 47 39	+33 22.3	m	13.07	1.52	42.0	11.19	
3059	NN 3641			11 02 43	+45 16.9	m	11.11	1.48	42.0	9.23	
3060	NN 3653			11 13 01	+55 36.2	M0	11.22	1.41	42.0	9.34	Steph 932
3061	NN 3676			11 34 55	+58 59.5	m	12.57		42.0	10.69	LTT 13176 Ross 112
3062	Gl 452.4			11 52 22	+29 01.2	M0 Ve	10.52	1.39	42.0	8.64	
3063	NN 3697			11 56 27	+42 56.3	m	12.07		42.0	10.19	
3064	Gl 455.1			12 03 17	-18 35.4	K5 V	9.99	1.34	42.0	8.11	
3065	NN 3725	AB		12 24 44	+27 18.3	K3 V	8.89	1.02	42.0	7.01	Wolf 412 ADS 8553 sep 2.3" 18d d(m) = 0.3 V (AB) = 8.28
3066	NN 3726	C		12 24 27	+27 17.8	dM5 e	14.88	1.73	42.0	13.00	San 76 sep 222" 260d
3067	NN 3735			12 31 25	-14 21.8	K3/4 V	9.05	1.11	42.0	7.17	LTT 4772 U300
3068	Gl 491	A		12 56 28	-09 34.0	K0 V	7.56	0.79	42.0	5.68	V(AB) = 7.55 d(m) = 5.2
3069	Gl 491	B		12 56 28	-09 34.0		12.50		42.0	10.60	sep 1.5" 326d - 1.6" 300d (1945- 1960)
3070	Gl 496	A		13 01 05	-20 18.9	F7 V J	6.27	0.56	42.0	4.39	BS 4935 ADS 8757 V (AB) = 5.57 d (m) = 0.1

3071	GI 496	wissenschaft in die schulen	13 01 05	-20 18.9		6.40		42.0	4.50	sep 0.6" (1876- 1947)
3072	Wo 9427		13 05 15	+34 40.1	dK8	9.34	1.18	42.0	7.46	SpT: K3 III OP
3073	NN 3793		13 32 25	+20 27.1	m	13.77		42.0	11.89	LP 379-62
3074	NN 3794		13 34 33	+23 13.4	m	12.66		42.0	10.78	LTT 13962 Ross 1021
3075	NN 3805		13 44 15	+57 15.3	DA3	13.30		42.0	11.42	LTT 14019
3076	GI 533.1		13 51 29	+65 52.5	M1.5	11.83	1.50	42.0	9.95	LTT 14056
3077	NN 3823		13 59 59	-24 17.7	M0.5	12.15	1.70	42.0	10.30	LTT 5477 LP 856-36 L 391-74
3078	NN 3834		14 12 09	+23 41.9	m	13.50		42.0	11.62	LTT 14173 L 1340-16 LP 381-17
3079	NN 3847		14 22 45	-20 02.4	m	14.70		42.0	12.80	LP 800-6
3080	NN 3874		14 52 29	+10 09.1	M0.5	11.30	1.40	42.0	9.42	LTT 14422 L 1198-67 LP 501-40
3081	GJ 1192		15 20 11	+01 36.1	K3 V	8.30	1.00	42.0	6.42	
3082	NN 3903	A	15 22 36	+37 33.1	F0 V	4.31	0.31	42.0	2.43	BS 5733 ADS 9626
3083	NN 3904	B	15 22 36	+37 33.4	G1 V	6.50	0.59	42.0	4.62	BS 5734 sep 108.9" d(m) = 2.2
3084	NN 3905		15 23 02	-26 31.9	K3/4 V	8.84	1.05	42.0	6.96	LTT 6168
3085	GI 587.1		15 25 53	+25 57.8	dM0	11.12	1.46	42.0	9.24	AC +26:37030
3086	NN 3941		16 07 11	+77 02.9	M1.5	12.35		42.0	10.50	LTT 18432 AC+77:5457
3087	NN 3947		16 13 26	+24 35.0	M2	11.99	1.51	42.0	10.11	LTT 14849 L 1346-3 LP 385-58
3088	NN 3980		16 55 04	+13 32.9	m	14.35		42.0	12.47	LP 506-37

3089	NN 3996	S	wissenschaft in die schulen!	17 13 31	-12 07.4	dM0	10.33	1.37	42.0	8.45	BPM 78844
3090	NN 4042			18 06 45	-12 02.8	K7 V	10.47	1.38	42.0	8.59	LTT 7218 L 847-61 dM2
3091	NN 4075			18 44 11	-61 40.1	m	12.80		42.0	10.90	LTT 7442 L 158-46
3092	G1 736			18 53 12	+04 12.1	G8 V	8.03	0.90	42.0	6.15	
3093	NN 4090	A		18 55 13	+54 28.1	dM0	10.44	1.38	42.0	8.56	
3094	NN 4091	B		18 55 15	+54 26.1	m	12.04	1.56	42.0	10.16	sep 120" 169d
3095	NN 4093			19 02 54	+70 21.0	m	12.54		42.0	10.66	LP 045-128
3096	G1 765.3			19 42 16	+57 53.8	F8	6.23	0.55	42.0	4.35	
3097	NN 4125			19 48 19	+31 39.0	m	12.88		42.0	11.00	LTT 15794 L 1501-69 LP 338-4
3098	GJ 1252			20 23 46	-56 35.7	m	12.23	1.45	42.0	10.35	
3099	NN 4156			20 40 12	+57 14.5	K7	10.29	1.36	42.0	8.41	LTT 16050
3100	NN 4173			20 56 40	+34 04.8	M2	11.06	1.46	42.0	9.18	LTT 16135 L 1504-126 LP 285-5
3101	NN 4187	A		21 14 55	-09 06.7	M1	12.11	1.52	42.0	10.23	Steph 1876
3102	NN 4188	B		21 14 58	-09 07.4		13.33		42.0	11.45	
3103	NN 4242	A		21 55 56	-32 42.3	m	14.65		42.0	12.77	LP 930-70
3104	NN 4243	B		21 55 55	-32 40.5	m	15.80		42.0	13.90	LP 930-69 sep 112" 354d
3105	NN 4245			21 55 58	-47 00.1	M4	11.80	1.47	42.0	9.92	CP-47: 9805 Sm 97
3106	NN 4301			22 49 37	+23 09.0	dK8	9.78	1.20	42.0	7.90	
3107	NN 4303			22 52 30	-52 34.0	M4	11.49	1.45	42.0	9.61	BPM 28050 Sm 119
3108	NN 4320			23 13 51	+30 23.8	K2 V	8.09	0.88	42.0	6.21	LTT 16838

3109	Wo 9826	S	wissenschaft in die schulen	23 23 26	+28 55.5	K3	11.05	0.94	42.0	9.20	LTT 16891 LFT 1791 AC +28:68304
3110	NN 4335			23 23 54	-47 07.0	m	15.75		42.0	13.87	L 360-133
3111	NN 4354			23 36 14	+38 53.2	m	13.58		42.0	11.70	V-R = 1.36 Weis
3112	NN 3070			00 59 29	-26 01.9		11.84	1.23	41.9	10.00	RGO 2913
3113	Wo 9433			13 10 04	+74 07.2	G2	9.34	0.58	41.9	7.50	LTT 13822
3114	Wo 9733	A		21 16 19	-53 39.6	A5 V	4.50	0.19	41.9	2.60	BS 8140 V (AB) = 4.39 d (m) = 2.40
3115	Wo 9733	B		21 16 18	-53 39.6	A7 V	6.90		41.9	5.00	sep 6.0" 275d (1957)
3116	Wo 9111			03 10 58	+52 10.1	dM0	10.24	1.26	41.8	8.35	LTT 11048 Ross 345
3117	Wo 9247			07 56 45	-34 48.7	G6 V	7.95	0.74	41.8	6.06	LTT 3016
3118	Wo 9309			09 57 28	-50 21.3	g-k	12.10		41.8	10.20	CFS 7030
3119	Wo 9327			10 20 33	+65 49.2	A0 p	4.97	-0.06	41.8	3.10	
3120	Gl 429.2			11 25 26	-08 53.7	M2	12.37	1.46	41.8	10.48	AC-09:1823- 108
3121	Gl 542.2			14 16 20	-06 22.1	K5	9.10	1.30	41.8	7.21	
3122	Wo 9581			16 54 28	-55 54.8	K5 III	3.12	1.60	41.8	1.20	
3123	Gl 799.1			20 39 41	-20 15.3	DA3	12.38	-0.08	41.8	10.49	LTT 8189 L 711-10
3124	Wo 9259			08 11 10	-40 23.0	G8 (IV)	9.39	0.82	41.7	7.50	LTT 3084
3125	Wo 9340			10 51 50	-30 53.3	G2 V	8.35	0.60	41.7	6.50	LTT 4001
3126	Gl 818.1	A		21 04 11	-73 22.3	G3 IV J	6.40	0.59	41.7	4.50	V(ABC) = 5.68 d(m) = 0. ?

3127	Gl 818.1	B	21 04 11	-73 22.3		6.40		41.7	4.50	comp B uncertain, sep 0.2"?
3128	Gl 818.1	C	21 04 11	-73 22.3		13.50		41.7	11.60	sep(AB-C) 8.1" 136d - 7.9" 131d (1901-1931)
3129	Wo 9722		21 06 44	+59 32.1	sdM1	13.30	1.55	41.7	11.40	LFT 1608
3130	Gl 338.1	A	09 11 57	+77 27.2	K5 J	10.67	1.38	41.6	8.77	Kui 39 V (AB) = 10.06 d(m) = 0.24
3131	Gl 338.1	B	09 11 57	+77 27.2		11.00		41.6	9.10	a = 0.58" P = 70.0 yr
3132	GJ 2152		21 11 00	+07 13.7	f	16.17	0.45	41.6	14.27	LTT 16218 pos (NLTT??)
3133	NN 3430	A	07 06 51	+37 45.3	sdM6	14.67	1.65	41.5	12.76	
3134	NN 3431	B	07 06 52	+37 45.3	DQ8	15.68	0.30	41.5	13.77	sep 13" 226d (NLTT)
3135	NN 3509		08 36 29	+67 50.3	m	14.68	1.68	41.5	12.77	LP 60-100 USNO 711
3136	Wo 9286		09 05 51	+26 50.2	G5 IV	5.99	0.65	41.5	4.08	LTT 12402
3137	GJ 1184		14 29 48	+11 34.2	K5	9.69	1.21	41.5	7.78	Wo 9485
3138	Gl 732.1		18 50 28	+52 54.6	G9 IVa	5.50	0.84	41.5	3.59	
3139	Wo 9219		06 51 34	-28 28.2	G5 IV	6.03	0.72	41.4	4.12	LFT 496
3140	Gl 406.1		10 54 21	+69 51.8	dM0.5	10.28	1.40	41.4	8.37	LTT 12927
3141	Wo 9394		12 09 29	+13 32.7	F6 V-VI	10.18	0.47	41.4	8.30	LTT 13394
3142	NN 3783	A	13 21 55	+55 11.2	dA1 p	2.25	0.02	41.4	0.34	BS 5054 ADS 8891 Aa: a = 0.012" P = 0.056 yr, d (m) = 0.0

3143	NN 3784	S	13 21 56	+55 10.9	A1 m	3.95	0.13	41.4	2.04	BS 5055 a = 0.13", P = 57 yr, AB: sep = 14.4" d(m) = 1.71
3144	Wo 9630		18 34 07	-25 42.6	G5 V	7.44	0.69	41.4	5.53	LTT 7388
3145	NN 4266		22 13 12	+56 47.9	F0 IV	4.19	0.28	41.4	2.28	LTT 16515
3146	Wo 9187		05 36 28	-07 14.4	A4 IV	4.80	0.14	41.3	2.90	
3147	NN 3575		09 55 00	+24 47.5	DA6	15.09	0.25	41.2	13.16	LTT 12661
3148	NN 3422		06 59 56	-67 50.9	K3 III	5.17	1.40	41.1	3.20	LTT 2717 CD-67: 492
3149	NN 3803	AB	13 42 35	+51 56.1	M3	12.30		41.1	10.40	LTT 14009 Ross 492 d (m) = 0.5 , sep 1.3" 33d (LTT)
3150	Wo 9540	A	16 01 37	-11 14.2	F6 IV-V	4.84	0.45	41.1	2.91	BS 5978 ADS 9909 V (AB) = 4.16 d (m) = 0.16
3151	Wo 9540	B	16 01 37	-11 14.2	F6 IV-V	5.00		41.1	3.10	BS 5977 a = 0.720" P = 45.69 yr
3152	Wo 9540	C	16 01 37	-11 14.1	G8 V	7.30	0.75	41.1	5.37	sep (AC) 7.6" 53d (1959)
3153	Wo 9782	A	22 24 05	+04 08.3	F7 V	5.75	0.52	41.1	3.82	LTT 16573 BS 8548 ADS 15935
3154	Wo 9782	B	22 24 05	+04 08.3	K4:	11.70		41.1	9.80	sep 3" 218d (NLTT)
3155	GJ 2003		00 17 36	-17 20.3	M1	11.69	1.55	41.0	9.75	BPM 70147 GR7
3156	Gl 31.2	A	00 42 07	-19 13.4	dM2	10.78	1.44	41.0	8.84	

3157	GI 31.2	wissenschaft in die schulen	00 42 05	-19 13.7	m	16.30		41.0	14.40	LP 766-10 sep 34" 239d d(pg) = 5.3, d (R) = 4.9 (NLTT)
3158	NN 3085		01 17 00	-26 40.0	m	13.46		41.0	11.52	PS 176
3159	NN 3104		01 36 55	+04 48.2	M5	12.83		41.0	10.89	Rob 72
3160	NN 3107		01 40 18	-24 53.0	m	12.02		41.0	10.08	PS 274
3161	NN 3123		01 56 57	+43 31.2	m	13.01		41.0	11.07	
3162	GI 92.1		02 14 52	+56 20.0	K1 V	8.27	0.92	41.0	6.33	
3163	NN 3153		02 18 10	+02 45.0	m	14.78	1.69	41.0	12.80	LTT 17354
3164	NN 3154		02 18 39	-39 15.7	K3/4 V	8.74	1.04	41.0	6.80	CP-39:190 LTT 1190
3165	NN 3164		02 30 48	+41 33.6	m	13.62		41.0	11.68	LTT 17383
3166	NN 3167		02 32 37	-72 54.5	K4 V	8.90	1.04	41.0	6.96	CD-73:110 LTT 1263
3167	NN 3169	A	02 33 49	+31 51.4	M3	13.63		41.0	11.69	LTT 10854 LE 7A LP 298-7 V(AB) = 13.02 d(m) = 0.3
3168	NN 3170	B	02 33 49	+31 51.4	M3.5	13.90		41.0	12.00	LTT 10855 LE 7B LP 298-8 sep 3" 25d d(R) = 0.2, d(pg) = 0.4
3169	NN 3215		03 14 45	+25 04.5	k	11.85	1.45	41.0	9.91	LTT 11081 LP 355-51 L 1307-8
3170	GI 149	A	03 40 36	-24 37.2	K4	9.20	1.13	41.0	7.26	
3171	GI 149	B	03 40 38	-24 36.9	m	15.60		41.0	13.70	LP 832-45 sep 36" 65d

3172	NN 3249	S	03 44 21	-11 27.0	M2.5	12.70	1.53	41.0	10.76	LTT 1777 L 805-8 LP 713-28
3173	NN 3254		03 50 33	+28 00.1	G8 V	7.84	0.84	41.0	5.90	
3174	GJ 1067		04 07 26	+70 04.4	dM0	9.69	1.23	41.0	7.75	
3175	NN 3298		04 31 22	-37 03.0	K3/5 V	8.79	0.99	41.0	6.85	CP-37:540
3176	NN 3303		04 34 55	-29 09.6	M3.5	13.70		41.0	11.80	LTT 2047 L 591-70 LP 890-46
3177	Wo 9160	A	04 35 53	-14 24.0	K2 IIIb	3.91	1.10	41.0	1.97	BS 1481 Kpr 18 V(AB) = 3.87 d(m) = 3.44
3178	Wo 9160	B	04 35 53	-14 24.0		7.30		41.0	5.40	sep 0.8"
3179	NN 3314		04 45 39	-11 01.2	K7 V	9.53	1.14	41.0	7.59	
3180	NN 3315		04 46 35	+45 53.9	k-m	11.79	1.47	41.0	9.90	LTT 11515 L 1672-41 LP 157-32
3181	NN 3330		05 03 51	+14 23.0	K0 V	7.75	0.80	41.0	5.81	LTT 11580
3182	NN 3355		05 31 51	+28 04.2	K7	10.08	1.27	41.0	8.14	LTT 11681 Ross 411
3183	NN 3384		06 03 54	+33 33.3	M3	12.44	1.45	41.0	10.50	LTT 11782 Ross 70
3184	GJ 245.1		06 43 31	-31 44.1	F6 V	5.92	0.49	41.0	3.98	dF6 (Wil)
3185	NN 3429		07 05 28	+30 47.6	M0	11.36	1.49	41.0	9.42	Steph 626
3186	NN 3473	A	07 59 47	+03 29.1	k-m	13.70		41.0	11.80	
3187	NN 3474	B	07 59 45	+03 28.5	m+	17.00		41.0	15.00	LP 544-12 sep 49" 223d
3188	GJ 305.1		08 20 34	+22 00.9	dM0 e	9.54	1.18	41.0	7.60	
3189	NN 3519		08 53 47	-54 46.3	F6 V	5.71	0.48	41.0	3.77	
3190	NN 3521		08 55 10	-71 24.4	m	14.50		41.0	12.60	LTT 3305 L 63-18

3191	NN 3529	S	09 00 26	+73 27.1	DC9	16.97		41.0	15.03	LP 36-115
3192	Wo 9315		10 04 48	-14 03.7	K7 V	10.19	1.32	41.0	8.25	U227
3193	Wo 9333		10 30 35	-41 12.4		11.12	0.90	41.0	9.20	
3194	NN 3645		11 07 26	-10 00.9	M0 V	10.54	1.40	41.0	8.60	Steph 922
3195	NN 3658		11 20 37	+45 05.2	m	12.74		41.0	10.80	
3196	NN 3669	A	11 29 10	+14 38.6	G0 V	6.20	0.57	41.0	4.26	LTT 13145 Wolf 401 ADS 8196
3197	NN 3670	B	11 29 10	+14 38.6	K6 IV	9.22	1.14	41.0	7.28	LTT 13146 sep 15" 326d
3198	NN 3683		11 41 04	-57 44.0	K1 V	8.21	0.91	41.0	6.27	LTT 4350 CD-57:4096
3199	NN 3717		12 11 54	+24 52.4	m	12.16	1.48	41.0	10.22	LTT 13409 L 1406-34 LP 376-34
3200	NN 3733		12 29 54	+31 52.3	m	13.22		41.0	11.28	LTT 13537 LP 321-35
3201	NN 3749		12 45 50	+47 30.3	m	13.65		41.0	11.71	
3202	NN 3767		13 09 24	+25 36.5	m	15.75	1.79	41.0	13.80	LP 378-688 San 236
3203	NN 3785		13 23 14	+55 14.9	A5 V	4.01	0.16	41.0	2.07	
3204	NN 3872		14 51 03	+28 42.6	K0 V	7.96	0.86	41.0	6.02	
3205	NN 3875		14 53 03	+41 20.8	m	14.67		41.0	12.73	LP 222-015
3206	NN 3880		14 54 43	+49 49.9	F8 V	5.63	0.50	41.0	3.69	LTT 14437 BS 5581
3207	NN 3887		15 02 05	-18 23.7	K4 V	9.59	1.20	41.0	7.65	LTT 6010
3208	Wo 9543	A	16 02 29	-32 43.5	G9 V	8.34	0.82	41.0	6.40	LTT 6409 V (AB) = 7.85 d (m) = 0.59
3209	Wo 9543	B	16 02 29	-32 43.5	K1 V	9.00		41.0	7.10	a = 0.820" P = 134.00 yr

3210	Wo 9543	S wissenschaft in die schulen	16 02 29	-32 43.5	K5	11.10		41.0	9.20	sep (AC) 9.6" 8d (1957)
3211	NN 3948		16 14 05	+35 56.5	K5	9.62	1.23	41.0	7.68	LTT 14853 L 1562-52 LP 275-83 H 32
3212	NN 3955		16 25 46	+15 40.8	m	13.18		41.0	11.24	LTT 14899 L 1274-24 LP 445-22
3213	NN 3956		16 25 52	+25 18.3	G5	8.19		41.0	6.25	
3214	NN 3958		16 28 48	-87 19.0	DA6	14.58	0.22	41.0	12.64	L 8-61 BPM 890 WD1628- 873
3215	NN 4020	A	17 38 07	+61 15.8	dK8	10.28	1.23	41.0	8.34	AC +61:27026
3216	NN 4021	B	17 38 08	+61 15.6		14.70		41.0	12.76	GSC 036B- 821 sep 19.1" 152d (GSC 1983.29)
3217	NN 4025		17 42 25	-07 59.4	g	11.48	1.45	41.0	9.50	LTT 7069 Wolf 1472
3218	NN 4043		18 09 42	+49 57.8	K7	9.96	1.29	41.0	8.00	LTT 15383 Wolf 1414
3219	NN 4074		18 42 48	-28 59.0	k	12.65	1.53	41.0	10.70	LTT 7434 L 633-165 LP 923-15
3220	NN 4087		18 51 54	-37 33.5	K1 V	8.11	0.88	41.0	6.17	LTT 7499
3221	NN 4100		19 08 07	+01 27.4	g	12.18	1.50	41.0	10.20	LTT 15613
3222	NN 4116		19 33 02	+51 07.7	F7 V	5.73	0.48	41.0	3.79	
3223	NN 4118		19 36 07	+33 46.7	G5	7.47		41.0	5.53	
3224	NN 4121		19 41 45	-71 12.2	m	13.90		41.0	12.00	LTT 7809 L 79-24
3225	NN 4128		19 52 06	+32 25.8	m	12.43		41.0	10.49	LTT 15818 L 1501-51 LP 338-6

3226	NN 4138	S	wissenschaft in die schulen	20 09 36	+38 14.9	G8 V	7.95	0.86	41.0	6.01	SpT: K1 IV OP, mod = 1.94 Olsen
3227	NN 4194			21 24 40	+70 15.6	G5	7.28		41.0	5.34	
3228	NN 4221			21 45 37	+01 12.8	m	13.87		41.0	11.93	LP 638-040
3229	GI 838.1	A		21 46 40	+05 29.4	K3 V	8.65	1.04	41.0	6.71	
3230	GI 838.1	B		21 47 04	+05 25.0	m	14.90	1.75	41.0	12.96	
3231	NN 4235			21 51 06	-43 50.3		15.35		41.0	13.41	LP 1032-23
3232	NN 4252			22 02 34	+04 53.5	M3	13.60	1.51	41.0	11.70	LTT 16456 Wolf 983
3233	NN 4263			22 10 48	-14 59.6	M3.5	13.34	1.51	41.0	11.40	LTT 8914 Wolf 1556
3234	NN 4265			22 11 22	+05 01.7	dM2	11.79	1.49	41.0	9.85	LTT 16505 Wolf 1019 Rob 314 V-I = 1.99 Robertson
3235	NN 4293			22 43 18	-63 34.0	M3	11.40	1.46	41.0	9.46	LTT 9181 BPM 15055 L 166-104 Sm 114
3236	Wo 9801	A		22 49 52	+09 34.1	F7 IV	5.16	0.48	41.0	3.22	LFT 1743
3237	Wo 9801	B		22 49 58	+09 38.1	M3:	13.52	1.66	41.0	11.58	LTT 16722 LFT 1744 sep 248" 20d
3238	GI 883			22 57 16	-11 38.9	dM1	10.60	1.42	41.0	8.66	
3239	Wo 9818			23 14 31	-58 30.6	F1 III	3.99	0.40	41.0	2.10	
3240	NN 4349			23 33 59	+55 13.2	M1	11.70	1.46	41.0	9.76	LTT 16952 Ross 303
3241	NN 4356	A		23 36 23	+20 44.6	m	14.24		41.0	12.30	
3242	NN 4357	B		23 36 24	+20 44.5	g	17.90		41.0	16.00	LP 463-28 sep 10" 108d (NLTT)
3243	Wo 9142			04 01 57	+00 06.9	G8	8.33	0.77	40.9	6.39	LTT 11337

3244	Wo 9168	S	wissenschaft in die schulen!	04 48 03	+45 45.5	G1 IV-V	6.97	0.58	40.9	5.00	LFT 375
3245	NN 3624			10 46 29	+05 18.7	m	19.11		40.9	17.17	LP 551-13
3246	NN 3663			11 23 33	-63 41.8	F7 V +F7V	5.17	0.50	40.9	3.23	LTT 4227 CD-63:650
3247	NN 3882			14 55 01	+15 10.8	m	14.73	1.68	40.9	12.79	USNO 741
3248	Wo 9557	A		16 18 12	+39 49.6	F3 IV-V	5.46	0.40	40.9	3.50	
3249	Wo 9557	B		16 18 12	+39 49.6		11.00		40.9	9.00	
3250	Wo 9638			18 53 47	+23 29.7	K2	8.09	0.91	40.9	6.15	LTT 15564 V775 Her
3251	NN 4295			22 44 07	+23 18.1	G8 IIIa CN	3.96	1.07	40.9	2.00	
3252	G1 893.1			23 11 51	-06 49.1	DQ6	15.42	0.22	40.9	13.48	LTT 9427 LP 702-48 L 935-050
3253	Wo 9057			01 31 35	+34 25.4	F8	9.56	0.52	40.8	7.60	
3254	NN 3837			14 14 29	+46 19.0	A0 p	4.18	0.08	40.8	2.23	LTT 14190 LAM Boo
3255	Wo 9848			23 59 22	+25 44.0	K3	11.30	0.94	40.8	9.40	LTT 17087 LFT 1847 Ross 679 AC +26:41
3256	Wo 9029	A		00 45 08	-37 12.5	F7/8 V	7.85	0.54	40.7	5.90	LTT 449
3257	Wo 9029	B		00 45 07	-37 13.4	m	15.50		40.7	13.50	L 938-2 sep 57" 193d
3258	NN 3201			03 05 03	+42 51.0	m	14.70	1.50	40.7	12.70	LTT 17467
3259	NN 3451			07 30 50	+22 30.6	m	16.46	1.60	40.7	14.51	LP 365-22
3260	NN 3541			09 12 36	+54 13.8	A5 V	4.83	0.19	40.7	2.90	FK 2734
3261	NN 3950	A		16 18 56	+75 52.3	F3 V	4.95	0.37	40.7	3.00	LTT 14869 ETA UMi

3262	NN 3951	S	16 19 50	+75 50.1	m	14.51		40.7	12.56	sep 227" 125d (NLTT)
3263	NN 4199		21 28 45	+23 07.0	dK8	9.25	1.05	40.7	7.30	
3264	Gl 890		23 05 41	-15 40.8	dM2.5e	10.88	1.42	40.7	8.93	
3265	NN 3075		01 06 04	-10 26.8	K1.5 III	3.45	1.16	40.6	1.49	FK 40 LTT 645 ETA Cet
3266	NN 3100		01 32 39	+41 47.2	dM0	10.99	1.30	40.6	9.03	
3267	NN 3172		02 34 54	+00 08.5	m	15.16	1.67	40.6	13.20	
3268	NN 3434		07 09 27	-48 51.1	K2 III	5.12	1.26	40.6	3.20	LTT 2758
3269	NN 3949		16 15 40	-04 34.3	G9.5 IIIb	3.24	0.96	40.6	1.28	
3270	Gl 686.1	A	17 35 44	+22 59.1	dM0 eJ	10.00	1.33	40.6	8.04	
3271	Gl 686.1	B	17 35 44	+22 59.1		10.22	1.38	40.6	8.26	
3272	Gl 773.3		19 57 04	-10 05.4	G0 V	5.88	0.58	40.6	3.92	
3273	Wo 9350		11 07 20	-42 11.2	K1	9.74	0.78	40.5	7.80	LTT 4109
3274	NN 3302		04 33 52	+11 07.0	k-m	14.30	1.62	40.4	12.33	LTT 17665
3275	NN 3447	A	07 29 11	+17 25.7	dM0	11.02	1.38	40.4	9.05	
3276	NN 3448	B	07 29 10	+17 25.7	m	12.95		40.4	10.98	Wor 27 sep 11"
3277	Gl 355.1		09 30 06	+70 03.1	G4 III-IV	4.56	0.77	40.4	2.59	
3278	NN 3703		12 02 40	+09 00.6	G8 IIIa CN	4.13	0.98	40.4	2.16	BS 4608 LTT 13353 OMI Vir
3279	NN 3841		14 16 51	+13 14.0	dF1	5.41	0.38	40.4	3.40	
3280	NN 4072		18 40 57	+04 17.3	DA6	14.92	0.14	40.4	12.95	GD 215

3281	GJ 1255	AB	20 38 03	+75 25.0	K0 V	8.00	0.86	40.4	6.00	Wo 9703 VW Cep Hei 7 a = 0.51" P = 30.45 yr, V (AB) = 7.08 d (m) = 0.
3282	GJ 1255	C	20 38 03	+75 25.0		10.40		40.4	8.40	sep(AC) 0.64" 223.3d (1974.64), d (m) = 2.9
3283	G1 838.4		21 49 53	+02 09.4	DA3	12.75	0.01	40.4	10.78	
3284	NN 3308		04 40 31	+18 54.7		13.40		40.3	11.40	AC+19:1513- 210 Ann Shanghai Obs. Vol. 10, p 57 (1989)
3285	NN 3642	AB	11 02 55	-27 01.4	F3 IV J	5.63	0.37	40.3	3.70	BS 4314 a = 0.140" P = 7.40 yr, V (AB) = 4.93 d (m) = 0.10
3286	Wo 9629		18 32 50	-44 20.7	G0	10.23	0.62	40.3	8.30	LTT 7379
3287	NN 4168		20 49 59	+26 54.5	G7 III CN	4.58	0.83	40.3	2.60	BS 7995
3288	NN 4195		21 25 19	+07 05.4	M0.5	11.60	1.56	40.3	9.63	LTT 16274 Ross 778
3289	NN 4334		23 23 16	+52 51.3	m	14.59	1.66	40.3	12.62	
3290	Wo 9035		00 59 04	+81 50.0	dG2	8.45	0.60	40.2	6.50	
3291	NN 3334		05 04 54	+09 24.7	G1 IV	6.17	0.62	40.2	4.19	LTT 11585
3292	Wo 9200		06 03 02	-45 02.1	G0 IV-V	6.35	0.52	40.2	4.40	LTT 2450 cmp with CD-45:2302
3293	NN 3754		12 47 56	+55 04.5	DC9+	17.82	1.50	40.2	15.84	LP 131-66 V- I = 1.46 (USNO) see also ApJ 346, 456

3294	Wo 9600	S	wissenschaft in die schulen	17 40 22	-18 29.7	M2	12.15	1.43	40.2	10.17	LFT 1369
3295	NN 4307			22 54 19	+67 59.2	m	14.68	1.70	40.2	12.70	USNO 778
3296	Gl 27.2			00 38 02	-24 04.4	G3 V	6.15	0.71	40.1	4.17	LTT 357
3297	Wo 9470			14 08 07	+25 19.7	F8 IV	4.83	0.53	40.1	2.80	
3298	NN 3041			00 33 18	-48 16.5	F6 V	5.51	0.44	40.0	3.52	CP-48: 51
3299	NN 3055			00 44 27	-26 24.6	M3 :	13.98	1.64	40.0	12.00	LTT 442 L 580-29 LP 826-59
3300	NN 3065			00 53 23	-29 56.9	K5 V	9.48	1.18	40.0	7.49	CP-30:90 LTT 525 RGO 8349 Mich : K4 III ??
3301	NN 3083			01 15 06	+28 24.7	M0.5	11.56		40.0	9.57	LTT 10468 Ross 324 LHS.
3302	NN 3088			01 17 28	-27 42.5	m	14.20		40.0	12.21	LTT 734 L 581-64 LP 883-185 PS 179 TS 389
3303	NN 3110			01 40 45	-42 27.2	M0	11.25		40.0	9.26	LFT 157 LTT 927
3304	Gl 74			01 43 58	+12 09.8	dK8	8.90	1.05	40.0	6.91	
3305	Wo 9061	A		01 47 08	-10 56.0	F3 III	4.67	0.33	40.0	2.68	
3306	Wo 9061	B		01 46 56	-10 57.0	dG1	6.77	0.62	40.0	4.78	
3307	Gl 81.3			01 55 06	-52 00.8	F8 V	6.10	0.48	40.0	4.11	
3308	NN 3124			01 57 09	+36 25.4	m	13.93		40.0	11.94	
3309	NN 3138			02 06 46	-16 34.9	K7	10.95		40.0	8.96	LTT 1117
3310	Gl 88			02 10 27	-17 55.4	M0	11.09	1.47	40.0	9.10	LP 769-90 L 728-16 AC- 18:3546

3311	NN 3151	A	02 17 21	+37 33.8	m	12.68		40.0	10.69	LTT 17347 V (AB) = 12.65 d(m) = 4.
3312	NN 3152	B	02 17 21	+37 33.8	k	16.70		40.0	14.70	LP 245-18 sep 2" 90d d (R) = 5, d (pg) = 4.3 (NLTT)
3313	NN 3155		02 19 14	-07 06.5	K0	8.98	1.08	40.0	6.99	LTT 1192
3314	Wo 9083		02 28 55	+02 02.8	K3 III	5.25	1.27	40.0	3.30	
3315	NN 3163		02 30 20	+07 40.1	G5	8.89	1.15	40.0	6.90	
3316	NN 3191		02 56 14	+31 34.3	m	13.41		40.0	11.42	LP 298-52
3317	NN 3199	AB	03 03 38	+40 10.1	K5	9.71	1.19	40.0	7.72	LTT 11010 ADS 2343 V (AB) = 9.66 d (m) = 3.4 , sep 3" 214d
3318	NN 3200		03 04 57	-13 57.0	G5 V	6.97	0.65	40.0	4.98	LTT 1469
3319	NN 3212		03 12 12	-09 51.2	M0	11.63	1.55	40.0	9.64	Steph 350
3320	NN 3214		03 14 36	+60 25.8	M3.5	13.33	1.51	40.0	11.30	LTT 11079 Ross 371
3321	NN 3226		03 24 55	+09 45.7	K7	10.45	1.39	40.0	8.46	Steph 367 = AC+09:26- 25 not BD +09:440!
3322	NN 3268		04 11 26	-54 00.1	m	13.87	1.56	40.0	11.88	LTT 1901 L 230-205
3323	NN 3277		04 20 15	+09 17.2	G5	8.04		40.0	6.05	
3324	Wo 9155	A	04 23 13	-57 11.0	G4 V	6.88	0.66	40.0	4.89	BS 1405 V (AB) = 6.29 d (m) = 0.35
3325	Wo 9155	B	04 23 13	-57 11.1	G6 V	7.30		40.0	5.30	sep 5.8"
3326	NN 3295		04 29 11	+64 31.7	G0	7.74		40.0	5.75	

3327	NN 3299	AB	04 31 29	+39 02.4	K5	9.30		40.0	7.30	ADS 3303 sep 0.3" d(m) = 0.5
3328	NN 3318		04 51 46	-20 37.4	M0 V	10.12	1.25	40.0	8.13	LTT 2117
3329	NN 3339		05 11 21	+07 57.1	DA8	15.89	0.42	40.0	13.90	LTT 17767
3330	GI 193		05 12 04	-15 52.8	G8 V	7.44	0.73	40.0	5.45	dG6 (Wilson)
3331	NN 3360	A	05 36 45	-46 07.6	G5 V	7.34	0.78	40.0	5.35	LTT 2342
3332	NN 3361	B	05 36 46	-46 07.6	K5 V	9.70		40.0	7.70	LTT 2343 sep 5.5" 67d
3333	NN 3376	AB	05 55 53	-04 39.1	G0	6.99		40.0	5.00	LTT 2421 ADS 4557 sep 4.1" 359d, d(m) = 6.8 , Mv = 5.01 Olsen
3334	NN 3377	C	05 55 49	-04 38.1	k-m	16.30		40.0	14.30	LP 659-4 sep (AB-C) 89" 312d (NLTT)
3335	GI 226.2		06 02 37	+67 59.1	dK8	9.75	1.25	40.0	7.76	AC+67:1894
3336	Wo 9201		06 03 15	-55 18.2	k	12.15	1.46	40.0	10.16	LTT 2452
3337	NN 3386		06 08 48	+63 24.7	dK8	9.69	1.21	40.0	7.70	
3338	NN 3402		06 38 36	+15 48.9	M3	13.77		40.0	11.78	LTT 11899 Wolf 289
3339	NN 3403		06 38 48	-55 34.0	K7 V	9.94	1.31	40.0	7.95	CP-55:1035 LTT 2621
3340	GI 243		06 42 52	-27 17.6	G2 V	6.45	0.54	40.0	4.46	
3341	NN 3411		06 46 16	+35 12.1	K5	10.17	1.32	40.0	8.18	LP 254-40
3342	NN 3424		07 01 46	+25 04.6	M1	11.62	1.48	40.0	9.63	LTT 11970 Ross 874
3343	NN 3428		07 04 54	+29 55.1	K3	8.32	0.93	40.0	6.33	LTT 11979
3344	NN 3443		07 27 00	-07 26.9	F8 V	5.86	0.48	40.0	3.87	

3345	GI 285.1		07 42 11	+70 19.9	dG5	7.09	0.66	40.0	5.10	
3346	NN 3465		07 49 53	+06 26.4	m	13.56		40.0	11.57	LTT 12080
3347	NN 3510	A	08 37 07	+09 06.8	m+	12.93	1.58	40.0	10.94	
3348	NN 3511	B	08 37 07	+09 06.8	m+	12.96		40.0	10.97	LP 485-38 sep 7" 85d
3349	GI 321.2		08 42 58	-42 26.9	G5 V	7.21	0.74	40.0	5.22	
3350	GI 340.2		09 16 54	+01 06.6	K0	8.16	0.87	40.0	6.17	
3351	Wo 9303		09 33 12	+37 45.2	K5	11.02	1.44	40.0	9.03	
3352	NN 3561		09 33 38	-05 53.3	m	14.00		40.0	12.00	
3353	NN 3581		09 59 14	-15 11.0	K3 V	8.64	1.02	40.0	6.65	LTT 3676
3354	NN 3620		10 44 13	-24 19.2	K5 V	9.39	1.16	40.0	7.40	CP-23: 5013
3355	NN 3627	A	10 47 42	+52 03.9	G5	8.33		40.0	6.34	LTT 12889
3356	NN 3628	B	10 47 40	+52 00.9	m	14.10		40.0	12.11	LP 128-32
3357	NN 3644		11 07 07	+02 43.6	G5	7.68	0.78	40.0	5.69	LTT 13000 Wolf 363
3358	GI 426	A	11 19 12	+18 27.9	K0	8.03	0.89	40.0	6.04	ADS 8140 V (AB) = 7.94 d (m) = 2.7
3359	GI 426	B	11 19 12	+18 27.9	K7	10.70		40.0	8.70	
3360	GI 433.2	A	11 36 07	+45 23.1	G0 V	6.45	0.57	40.0	4.46	
3361	GI 433.2	B	11 36 06	+45 23.1	K2 V	8.40	0.96	40.0	6.41	
3362	NN 3718		12 12 59	+39 27.9	m	11.89		40.0	9.90	
3363	NN 3755		12 48 09	+27 11.9	m	14.14		40.0	12.15	LTT 13677 LP 321-147 San 149
3364	GJ 1166	A	12 48 57	+22 22.5	dM4	12.97	1.60	40.0	10.98	LP 377-78 BPM 88513 San 151

3365	GJ 1166	wissenschaft in die schulen	B	12 49 02	+22 23.3	dM3-3.5	14.28	1.72	40.0	12.29	LP 377-79 BPM 88515 San 152 sep 85" 53d (NLTT)
3366	NN 3761			13 04 05	-77 02.5	K3 V	8.88	1.04	40.0	6.89	CP-76:747
3367	NN 3763			13 06 24	+16 38.2	m	12.99		40.0	11.00	LTT 13794 L 1264-69 LP 437-12
3368	NN 3831		AB	14 11 38	-15 07.3	K4 V	10.40	1.28	40.0	8.41	LTT 5580 L 836-121 Oo 587 sep 1.6" d(m) = 3.4 V (AB) = 10.35
3369	NN 3832		C	14 11 34	-15 07.1	m	13.96	1.60	40.0	11.97	LTT 5581 L 836-122 Oo 586 sep 65" 279d
3370	NN 3864		A	14 41 44	-22 02.3	K2/3 V	9.32	1.17	40.0	7.33	LTT 5855
3371	NN 3865		B	14 41 49	-22 01.8	k-m	16.30		40.0	14.30	LP 858-23 sep 69" 68d (NLTT)
3372	Gl 585.1			15 25 12	+02 46.3	dM0	10.21	1.34	40.0	8.22	
3373	Gl 587			15 25 44	-49 46.8	G5 V	7.69	0.77	40.0	5.70	
3374	Gl 588.1			15 32 03	+38 04.9	dM0	11.28	1.50	40.0	9.29	AC +38:34548
3375	NN 3914			15 40 15	-30 46.1	m	13.10		40.0	11.10	LTT 6278 L 552-4 LP 916-51
3376	NN 3932			15 57 34	+15 08.9	m	13.99	1.58	40.0	12.00	
3377	NN 3944			16 10 44	-21 16.4	G3 V	6.69	0.61	40.0	4.70	
3378	Gl 640			16 47 54	+18 59.2	dK5	8.90	1.02	40.0	6.91	
3379	NN 3982			16 57 44	-61 29.6	K3 V	8.84	1.04	40.0	6.85	CP-61: 5825
3380	NN 3985			16 59 09	-53 09.9	F6 V	5.29	0.50	40.0	3.30	

3381	NN 3994	S	17 12 41	+26 58.9	m	12.35	1.52	40.0	10.36	LTT 15104 L 1421-36 LP 332-9
3382	Wo 9599		17 39 45	+65 01.5	K0	8.37	0.93	40.0	6.38	
3383	GJ 1229		18 29 52	+13 41.8	G8 V	7.20	0.68	40.0	5.21	
3384	NN 4085	A	18 50 01	-54 25.1	K3 V	9.18	1.13	40.0	7.19	CP-54:9142 LTT 7488 L 273-102
3385	NN 4086	B	18 50 01	-54 25.1	m	12.30		40.0	10.30	LTT 7489 L 273-101 sep 11" 357d
3386	Wo 9637		18 52 06	-22 44.1	K3 IIIa:	4.99	1.33	40.0	3.00	
3387	NN 4094	AB	19 02 55	+63 55.0	M0	10.60	1.42	40.0	8.60	Steph 1676 sep 3" 70d d (R) = 3. Weis; V(AB) = 10.55 d(m) = 3.5 :
3388	G1 765.2		19 40 40	+76 18.2	dK0	8.08	0.88	40.0	6.09	
3389	Wo 9677	A	19 55 39	+59 01.7	dM0 p	9.96	1.22	40.0	7.97	
3390	Wo 9677	B	19 55 30	+59 01.3	m	13.50	1.48	40.0	11.51	
3391	G1 794.3		20 36 47	+38 27.7	G2 V	6.75	0.62	40.0	4.76	
3392	NN 4175		20 59 10	+20 32.1	m	14.10		40.0	12.10	
3393	NN 4192		21 21 52	+08 17.3	m	13.64		40.0	11.65	
3394	NN 4220		21 45 26	+05 35.7	M1.5	11.79	1.43	40.0	9.80	LTT 16371 Ross 779
3395	NN 4255		22 03 28	+78 02.1	m	15.87	1.80	40.0	13.90	LP 27-9
3396	NN 4280		22 24 52	+63 37.3	K7	9.51	1.18	40.0	7.52	
3397	Wo 9793		22 39 08	+18 33.7	M0	10.75	1.42	40.0	8.76	L 1293-93 pm (AC - BDX)
3398	GJ 1281		23 08 03	-19 28.7	M3	12.47	1.49	40.0	10.50	LP 822-31 L 791-76

3399	NN 4323	S	23 14 19	+05 25.4	dM0.5	10.52	1.41	40.0	8.53	
3400	NN 4343		23 32 57	+30 53.3	K0	7.91	0.84	40.0	5.92	LTT 16944
3401	NN 4364		23 47 04	+08 04.8	M1	11.39	1.45	40.0	9.40	Steph 2166
3402	GJ 1291	AB	23 47 39	-29 40.8	K1 V	7.94	0.84	40.0	5.95	BPM 68764 comp in 2.5", d(m) = 7
3403	NN 4376		23 52 50	-04 15.8	m	13.95		40.0	11.96	
3404	Wo 9177		05 09 13	-44 38.1	G8 IV/V	8.71	0.77	39.9	6.70	LTT 2195
3405	G1 579.2	A	15 07 28	-16 08.5	K0 VI	9.08	0.77	39.9	7.08	
3406	G1 579.2	B	15 07 28	-16 13.5	K2 VI	9.45	0.86	39.9	7.45	
3407	NN 3499		08 25 12	-65 58.2	K2 III	3.76	1.13	39.8	1.80	FK 319
3408	NN 3559		09 27 37	+63 16.9	F0 IV	3.67	0.33	39.8	1.67	
3409	NN 4095	AB	19 03 06	+13 47.5	A0 Vn	2.99	0.01	39.8	1.00	BS 7235 ADS 12026 sep 158.6" d (m) = 8.4
3410	G1 848.2		22 05 05	-47 12.2	B5 V	1.74	-0.13	39.8	-0.30	ALF Gru
3411	NN 3358		05 34 18	+51 24.9	K2 V	7.73	0.83	39.7	5.72	LTT 11689 LFT 420
3412	Wo 9238		07 34 49	+28 23.8	M3	13.85	1.47	39.7	11.84	LTT 12045 LFT 536 Ross 394
3413	NN 3751		12 47 04	+09 44.8	M3.5	13.07	1.56	39.7	11.10	LTT 13667 Wolf 439
3414	NN 3828	A	14 09 39	-00 21.2	M3.5	12.97	1.63	39.7	10.96	LTT 5558 LFT 1076 LP 619-49 L 980-2
3415	NN 3829	B	14 09 40	-00 21.4	m+	21.00		39.7	19.00	LP 619-50 sep 21" 125d (LHS)

3416	NN 3881	S	wissenschaft in die schulen	14 54 59	+00 02.0	K1 III	5.53	1.13	39.7	3.50	BS 5573 comp B: sep 86.3" d(m) = 2.9
3417	Wo 9723			21 07 01	+46 57.3	K3	10.78	0.95	39.7	8.80	LFT 1609
3418	NN 4259			22 07 21	+14 14.8	DA6	15.66	0.23	39.7	13.65	LTT 16482 PG
3419	Wo 9836	A		23 40 08	-14 49.3	B9 V	4.48	-0.04	39.7	2.50	
3420	Wo 9836	B		23 40 08	-14 49.3		11.00		39.7	9.00	
3421	G1 911			23 52 12	-22 03.3	dM0.5	10.87	1.47	39.7	8.86	
3422	G1 83			01 57 12	-61 48.8	F0 V	2.86	0.28	39.6	0.85	ALF Hyi
3423	Wo 9107			02 59 28	-28 16.9	G5 IV	5.88	0.79	39.5	3.86	LTT 1446 LFT 251
3424	NN 3347	A		05 26 03	+12 30.9	G0 V	6.75	0.58	39.5	4.70	LTT 11655
3425	NN 3348	B		05 26 08	+12 29.7	m	13.98	1.65	39.5	12.00	sep 94" 315d
3426	NN 3912			15 32 43	-14 37.5	G8.5 III	3.90	1.00	39.5	1.90	
3427	G1 371			09 49 37	+03 27.4	dM0 p	8.86	1.23	39.4	6.84	
3428	Wo 9510			15 03 58	+65 00.3	G8	9.47	0.82	39.4	7.40	LTT 14491
3429	GJ 1195			15 40 22	-10 46.3	F3 VI	7.22	0.49	39.4	5.20	CVS 101522
3430	Wo 9547			16 07 57	-52 47.0	g	10.50	1.16	39.4	8.48	CD-52:7263 LTT 6452
3431	Wo 9593	A		17 33 36	-49 22.6	G2 V	9.40	0.63	39.4	7.40	LTT 7002 V (AB) = 8.98 d (m) = 0.8
3432	Wo 9593	B		17 33 36	-49 22.5	G5	10.20		39.4	8.20	LTT 7003 sep 6.0" 336d (1903), d(R) = 0.8 d (pg) = 0.8 (NLTT)
3433	Wo 9605			17 45 16	+04 57.5	K1 V	8.92	0.84	39.4	6.90	LFT 1377

3434	NN 3544	S	09 14 06	+00 56.3	F6 III-IV	6.71	0.41	39.3	4.70	ADS 7276 sep 2" d(m) = 5.5
3435	NN 3995	AB	17 12 57	+24 53.5	A3 IV	3.14	0.08	39.3	1.11	BS 6410 ADS 10424 sep 8.5" d(m) = 5.6
3436	NN 3365		05 43 02	+44 06.4	M4	12.79	1.55	39.2	10.80	LTT 11721 Wolf 237
3437	NN 4298		22 47 36	+24 19.8	G8+ III	3.48	0.93	39.2	1.40	
3438	GI 330.1		08 55 44	+20 44.6	dK5	9.26	1.11	39.1	7.22	
3439	NN 3889		15 03 10	-07 03.1	DA7	15.90	0.39	39.1	13.86	GD 175
3440	NN 4107		19 18 46	-17 56.6	F0 IV	3.93	0.23	39.1	1.89	
3441	NN 4277	A	22 23 43	+02 45.3	dM	13.68	1.59	39.1	11.64	LTT 16570 LFT 1717 L 1077-19 LP 640-73 Rob 319
3442	NN 4278	B	22 23 43	+02 45.1	m	17.70		39.1	15.70	LP 640-72 sep 11" 201d (LHS)
3443	NN 3003		00 02 21	+22 59.5	G9 V	7.82	0.74	39.0	5.78	LTT 10010
3444	NN 3026		00 15 22	-18 11.4	m	13.20	1.58	39.0	11.16	LTT 146 L 722-46 LP 764-92
3445	GI 17.2		00 19 52	-27 18.3	K3 V	8.30	0.90	39.0	6.26	LTT 190
3446	NN 3046		00 36 40	+60 16.9	m	12.83		39.0	10.79	LTT 10222 Wolf 10
3447	GI 56.3	A	01 16 06	-01 07.6	K1 V	8.00	0.82	39.0	5.96	
3448	GI 56.3	B	01 16 05	-01 08.0	M0	10.70	1.41	39.0	8.66	
3449	NN 3116		01 47 44	+18 02.9	M0	10.79	1.38	39.0	8.70	LTT 10634
3450	NN 3156		02 21 54	+25 45.1	m	11.62		39.0	9.58	LTT 10808 LP 353-74
3451	NN 3165		02 31 01	+14 47.1	M3.5	13.76	1.63	39.0	11.70	LTT 10846

3452	NN 3185	S	02 49 23	+60 39.0	K5 V	9.16	1.07	39.0	7.12	AG+60:305
3453	Gl 135		03 16 30	-03 01.4	G1.5 V	7.03	0.66	39.0	4.99	
3454	NN 3280		04 21 36	+32 20.2	k-m	12.44	1.51	39.0	10.40	LTT 11417 L 1455-12 LP 302-22
3455	Gl 171		04 31 59	+55 18.9	K2 V	8.34	0.90	39.0	6.30	
3456	Gl 175	A	04 39 29	-59 02.5	G5 V J	7.19	0.68	39.0	5.15	BS 1504 V (AB) = 6.53 d (m) = 0.21
3457	Gl 175	B	04 39 29	-59 02.5		7.40		39.0	5.40	a = 1.902" P = 240.0 yr
3458	NN 3316		04 47 44	+26 02.4	m	12.84	1.54	39.0	10.80	LTT 11519
3459	Gl 187		05 01 30	-49 13.3	F2 V	5.37	0.43	39.0	3.33	ETA(1) Pic
3460	NN 3340		05 12 42	-07 23.8	m	11.55		39.0	9.51	S 3
3461	NN 3342	A	05 16 18	+58 45.0	m	13.44	1.62	39.0	11.40	
3462	NN 3343	B	05 16 17	+58 44.7	m	14.03	1.64	39.0	11.99	
3463	NN 3346		05 17 44	-15 53.5	K3 V	8.79	1.00	39.0	6.75	LTT 2240
3464	Gl 223		05 51 52	+02 08.6	K3 V	8.83	1.02	39.0	6.79	
3465	NN 3387		06 09 18	+06 47.9	G4 V	6.87	0.63	39.0	4.83	LTT 11802
3466	Wo 9220	A	06 51 49	+13 14.6	A9 V p	4.74	0.31	39.0	2.70	BS 2564 ADS 5559
3467	Wo 9220	B	06 51 49	+13 14.6	G6 V	7.68	0.72	39.0	5.64	sep 7.0" d(m) = 2.9
3468	Wo 9269		08 31 36	-23 11.1	K1(IV)+G	7.21	0.74	39.0	5.20	LTT 3170 possibly composite (Mich)
3469	NN 3536		09 06 46	+84 23.1	m	11.92		39.0	9.88	LP 5-140
3470	NN 3585		10 03 43	+41 57.8	M0	11.32	1.49	39.0	9.30	LTT 12699 FI-285
3471	NN 3591		10 12 57	-82 37.8	k	11.07	1.42	39.0	9.03	LTT 3760 L 17-47

3472	NN 3595	S	wissenschaft in die schulen!	10 17 33	+49 33.0	m	13.16		39.0	11.12	
3473	NN 3603			10 25 43	-06 20.5	K0 V	7.86	0.80	39.0	5.82	
3474	Wo 9376			11 51 54	-51 06.7	G5	10.97	0.92	39.0	8.93	LTT 4428
3475	NN 3724			12 22 31	+23 40.1	m	16.58	1.88	39.0	14.50	LP 376-62 San 71
3476	NN 3818			13 56 11	+00 10.1	m	14.05		39.0	12.01	LTT 14085 L 1051-35 LP 619-9
3477	Gl 542.1	A		14 16 10	-25 35.4	F5 V	5.87	0.50	39.0	3.83	
3478	Gl 542.1	B		14 16 10	-25 35.4		13.30		39.0	11.30	
3479	Gl 558.1			14 33 32	-67 42.7	F8 V	6.04	0.50	39.0	4.00	
3480	NN 3870			14 49 58	+00 22.6	M2	12.58	1.58	39.0	10.50	LTT 14407 Wolf 555
3481	Gl 569.1			14 53 46	+53 52.5	K1 V	7.78	0.78	39.0	5.74	
3482	Gl 606.1	A		15 58 21	-84 05.8	K0 V	7.68	0.78	39.0	5.64	V(AB) = 7.66 d(m) = 3.35
3483	Gl 606.1	B		15 58 21	-84 05.8	k-m	11.03	1.36	39.0	8.99	L 20-30 sep 22" 29d (NLTT)
3484	NN 3983			16 58 18	+25 25.3	m	13.22		39.0	11.18	LP 587-31
3485	NN 4014			17 35 25	-43 06.9	G5 V	7.24	0.72	39.0	5.20	LTT 7019 CP-43: 8186
3486	NN 4058			18 23 51	+38 20.1	M1	11.27	1.48	39.0	9.23	
3487	NN 4097			19 05 19	-31 03.1	K0 V	7.82		39.0	5.78	\$ mod = 2.03 Olsen
3488	NN 4112			19 30 06	-52 32.0	M4	12.80	1.55	39.0	10.76	LTT 7723 L 275-26 BPM 26201 Sm 39
3489	NN 4123			19 47 13	+08 04.9	k	15.21	1.72	39.0	13.20	
3490	NN 4139			20 09 39	-12 45.9	F7 V	5.85	0.48	39.0	3.81	LTT 7995
3491	Gl 791.3			20 29 33	+33 36.3	dK8	9.23	1.13	39.0	7.19	

3492	NN 4147	S	wissenschaft in die schulen	20 31 25	-13 53.7	F6 V	6.13	0.54	39.0	4.09	BS 7855
3493	GJ 2149			20 39 36	-68 16.0	DA3	13.40	0.10	39.0	11.40	LTT 8190 L 116-79 BPM 13491
3494	NN 4183			21 09 24	+45 15.3	K2	7.83	0.78	39.0	5.79	LTT 16209
3495	Wo 9754			21 44 55	-40 29.0	K3 V	8.62	0.97	39.0	6.58	LTT 8701
3496	Wo 9757			21 47 06	-11 54.9	K5	10.83	1.41	39.0	8.79	LTT 8720
3497	NN 4232			21 49 55	+27 11.5	m	14.06		39.0	12.02	
3498	GJ 871.2			22 44 11	+49 56.8	K0	7.86	0.80	39.0	5.82	
3499	NN 4313			23 06 34	-02 31.8	K3 V	8.59	1.01	39.0	6.55	LTT 9378
3500	NN 4330			23 15 25	-41 05.8	F5 V	5.53	0.44	39.0	3.49	
3501	NN 4339			23 27 45	+31 25.9	K0	8.31	0.93	39.0	6.27	LTT 16910
3502	Wo 9829			23 28 56	-04 21.6	F8 V	6.49	0.54	39.0	4.45	LTT 9578 Viln 82 no 70
3503	NN 4372			23 51 28	-41 49.4	M4	13.30		39.0	11.30	LFT 1834 LTT 9766 L 433-62
3504	GJ 1293			23 58 51	-17 13.4	dM1.5	10.80	1.40	39.0	8.76	
3505	Wo 9141			03 57 20	+51 15.4	M3.5	13.65		38.9	11.60	LTT 11315 LFT 324
3506	GJ 558			14 32 55	+33 57.7	dM0.5	9.58	1.28	38.8	7.52	
3507	NN 3921			15 48 19	+04 37.6	A2 m	3.71	0.15	38.4	1.63	
3508	GJ 697.1			17 52 56	+03 45.7	dM0 e	10.13	1.34	38.4	8.05	AC+03:2518- 200
3509	GJ 708			18 13 07	+18 28.9	dM1	10.07	1.33	38.4	7.99	
3510	GJ 769			19 50 22	-47 55.6	M3	12.53	1.56	38.4	10.50	L 349-068
3511	NN 3415	A		06 52 59	+40 08.8	K5 V	9.12	1.12	38.1	7.02	LTT 11946

3512	NN 3416	S	06 52 59	+40 08.8	M1	11.10	1.43	38.1	9.00	LTT 11947
3513	NN 4227		21 48 49	+12 36.4	m	13.42	1.50	38.1	11.32	
3514	NN 3187		02 50 14	-33 39.3	K1 V	8.09	0.84	38.0	5.99	LTT 1376
3515	Gl 186.1	A	05 01 20	-56 09.7	G5 V	7.02	0.63	38.0	4.92	
3516	Gl 186.1	B	05 01 28	-56 10.5	m	10.60	1.36	38.0	8.50	LTT 2159 L 179-10 sep 78" 124d (LHS)
3517	NN 3338		05 11 19	+19 49.7	K4	9.47	1.17	38.0	7.37	LTT 11613 comp B: K3: opt.
3518	Wo 9185		05 35 24	-62 50.2	K5 V	9.33	1.13	38.0	7.23	LTT 2337 L 132-46
3519	Gl 378.1		09 59 23	+44 49.3	dK8	9.04	1.07	38.0	6.94	
3520	Gl 383.1		10 10 44	+52 45.9	dM0	9.53	1.10	38.0	7.43	
3521	Wo 9367		11 31 48	+03 20.3	F6 V	5.77	0.46	38.0	3.67	LTT 13159
3522	Gl 521.2	A	13 38 24	+50 46.3	F7 V	6.33	0.54	38.0	4.23	
3523	Gl 521.2	B	13 38 26	+50 46.1		10.46	1.36	38.0	8.36	
3524	Gl 612		16 04 42	+38 46.4	K3 V	8.61	0.96	38.0	6.51	
3525	Gl 773.2		19 55 13	+29 41.1	K0 Ve	7.90	0.80	38.0	5.80	
3526	Gl 826.2		21 20 52	-46 55.2	M2	12.46	1.56	38.0	10.36	L 353-143 Sm 78
3527	Gl 895.1		23 22 55	-45 53.1	M0	11.26	1.42	38.0	9.20	L 359-33 Sm 135
3528	Wo 9216		06 38 53	+71 56.8	K7	10.95	1.48	37.8	8.80	LTT 11898 LFT 480 AC +72:3338 GJ 2050
3529	NN 3825		14 04 49	+38 51.7	m	14.54	1.70	37.4	12.40	
3530	GJ 1213		17 11 26	+42 23.7	dM1	10.10	1.27	37.2	7.95	
3531	NN 3701		12 01 04	-42 08.7	F6 V	5.15	0.41	37.1	3.00	LTT 4497 FK 449
3532	NN 3066		00 53 42	+68 46.6	K4 V	9.10	1.03	37.0	6.94	LTT 10329

3533	GI 77	A	01 46 12	-41 44.7	G4 V	7.14	0.65	37.0	4.98	
3534	GI 83.4	A	02 01 55	-45 39.2	G3 V	7.31	0.69	37.0	5.15	
3535	GI 83.4	B	02 01 55	-45 39.2		11.50		37.0	9.30	sep 1.0" 178d (1932)
3536	GI 165.2		04 11 53	+02 53.6	K3 V	8.79	0.97	37.0	6.63	
3537	Wo 9158		04 31 11	+05 17.1	K1	7.93	0.79	37.0	5.77	LTT 11456
3538	Wo 9206		06 10 51	-65 10.8	k	11.35	1.46	37.0	9.19	LTT 2486 LFT 461
3539	GI 296.2		08 05 11	+69 52.2	F8 V	6.57	0.58	37.0	4.41	
3540	Wo 9336		10 50 39	-20 21.5	G3/5 V	7.05	0.64	37.0	4.89	LTT 3991
3541	GI 485		12 44 54	+31 29.4	K4 V	9.84	1.29	37.0	7.68	
3542	Wo 9474	A	14 14 24	+51 35.8	A7 V	4.75	0.20	37.0	2.59	
3543	Wo 9474	B	14 14 26	+51 36.4	K1 V	8.23	0.82	37.0	6.07	
3544	NN 3977		16 48 59	+47 48.9	dK8	9.42	1.19	37.0	7.26	
3545	NN 4234		21 50 16	+28 33.5	F5 VI-V	5.53	0.42	37.0	3.37	
3546	NN 3792		13 32 10	-00 20.4	A3 V	3.37	0.11	36.9	1.21	LTT 5252
3547	NN 3025		00 15 07	-08 57.7	dM0	11.00	1.42	36.6	8.82	LTT 141 L 866-22
3548	GI 611.3		16 04 18	+08 31.2	dM3 e	11.55	1.46	36.6	9.37	LTT 14795 L 1130-30
3549	GI 62		01 34 49	-29 38.8	K0 V	8.14	0.86	36.0	5.92	
3550	Wo 9082		02 23 23	+05 33.2	G9	7.95	0.81	36.0	5.73	LTT 10810
3551	NN 3267		04 08 37	+76 09.9	G5	8.19	0.84	36.0	5.97	LTT 11362
3552	NN 3460		07 38 01	+49 20.4	dK8	9.73	1.19	36.0	7.51	
3553	GI 389.1		10 21 45	-10 08.9	dK8	10.00	1.24	36.0	7.78	
3554	NN 3715		12 10 24	+10 19.2	G8 V	7.92	0.79	36.0	5.70	LTT 13397

3555	NN 3721	S	wissenschaft in die schulen	12 19 53	+25 27.0	M0	11.38	1.34	36.0	9.16	LTT 13466 Wolf 409
3556	Wo 9417			12 46 29	+60 35.5	F6 V	5.85	0.46	36.0	3.63	
3557	Wo 9421			12 50 37	-03 16.9	F5 V	6.11	0.50	36.0	3.89	LTT 4922
3558	Gl 503.2			13 11 34	+56 58.4	G1 V	6.83	0.60	36.0	4.61	
3559	Gl 654.4			17 04 50	+88 41.8	K0	8.32	0.87	36.0	6.10	
3560	Wo 9664	A		19 38 18	-59 07.5	G5 V	7.48	0.71	36.0	5.26	LTT 7783
3561	Wo 9664	B		19 38 18	-59 07.5		8.70		36.0	6.50	
3562	Gl 781.2			20 06 48	-14 26.0	K3/4 V	9.76	1.15	36.0	7.54	
3563	Wo 9726			21 09 01	-40 28.3	F7 V	5.83	0.45	36.0	3.61	LTT 8410
3564	Gl 827.1			21 23 18	-56 20.7	K3 V	8.66	0.92	36.0	6.44	
3565	Gl 838.3	A		21 49 52	+42 06.8	G8	7.86	0.78	36.0	5.64	
3566	Gl 838.3	B		21 49 52	+42 06.8	M1	11.45	1.43	36.0	9.23	
3567	NN 4384	AB		23 56 56	+33 26.8	F8 V	6.47	0.55	36.0	4.25	BS 9074 ADS 17149 V(AB) = 5.81 d(m) = 0.2 ; sep 1.5"
3568	Gl 16			00 15 42	+09 55.5	dM0	10.90	1.50	35.9	8.68	AC+09:2-34
3569	Gl 292.1			07 51 59	+19 22.5	dK6	7.78	0.95	35.5	5.53	
3570	NN 3234			03 31 53	+28 05.7	m	16.67	1.94	35.3	14.41	
3571	Wo 9036			01 01 59	-25 52.1	K5 V	9.80	1.19	35.0	7.52	LTT 606
3572	Wo 9212	A		06 25 10	-25 49.3	F9 V	6.07	0.53	35.0	3.79	LTT 2558
3573	Wo 9212	B		06 25 10	-25 49.3	K7	11.57	1.04	35.0	9.29	LTT 2559
3574	GJ 1139			10 50 40	+76 19.9	K4	9.65	1.10	35.0	7.37	
3575	Wo 9397			12 10 50	+16 58.7	M1.5	11.96	1.45	35.0	9.68	LFT 885 LTT 13403 Wolf 1438 Ross 127

3576	Wo 9450	S	wissenschaft in die schulen	13 31 36	-38 38.8	G4 V	7.29	0.67	35.0	5.01	LFT 1020
3577	Wo 9452			13 31 52	+75 15.7	K7	10.27	1.29	35.0	7.99	LTT 13949
3578	GI 667.1			17 15 40	-75 17.7	G2 V	7.00	0.60	35.0	4.72	
3579	Wo 9639			18 56 55	+30 06.5	G2 V	6.79	0.58	35.0	4.51	LTT 15573
3580	Wo 9798			22 48 56	+13 42.1	dK4	8.30	0.84	35.0	6.02	LTT 16716
3581	NN 3385			06 07 40	+25 57.1	M1.5	11.55	1.46	34.7	9.25	LTT 11796 Wolf 1058
3582	GI 786.1			20 14 11	+42 49.5	dM0 p	9.97	1.34	34.6	7.67	AC+42:849- 367
3583	NN 3038			00 29 56	-63 21.9	K7	9.61	1.35	34.3	7.29	CD-63:9 LTT 288 LFT 49
3584	NN 3349			05 26 38	+32 03.2	M3	12.15	1.48	34.1	9.81	LTT 11657 LFT 414 Ross 406
3585	GI 87.1	A		02 10 14	-02 37.6	F8 V	5.67	0.56	34.0	3.33	ADS 1703
3586	GI 87.1	B		02 10 13	-02 37.8	G5 V	7.74	0.68	34.0	5.40	sep 16.2" 232d (1958)
3587	GI 308	A		08 25 15	+35 11.2	M0 V	11.48	1.55	34.0	9.14	AC +36:28826 Wor 19 V (AB) = 10.73 d(m) = 0.1
3588	GI 308	B		08 25 15	+35 11.2		11.56		34.0	9.22	a = 0.56" P = 32.7 yr
3589	Wo 9287	A		09 06 26	-25 38.2	G1 V	6.77	0.57	34.0	4.43	LTT 3365
3590	Wo 9287	B		09 06 26	-25 38.2		13.00		34.0	11.00	
3591	NN 3596			10 20 03	+15 35.9	dG2	7.28	0.65	34.0	4.94	LTT 12778 ADS 7744 sep. 1.1" rapid
3592	GI 479.1			12 35 44	+79 29.4	dG2 e	6.96	0.59	34.0	4.62	
3593	NN 3806	A		13 46 02	-35 27.2	G3 IV-V	6.57	0.55	34.0	4.23	LTT 5358

3594	NN 3807	S	wissenschaft in die schulen	B	13 46 02	-35 27.2	K4 :	10.14	1.23	34.0	7.80	LTT 5359 sep 12" 354d (NLTT)
3595	Gl 536.1	A			13 59 34	+15 44.1	dM0.5 J	11.25	1.45	34.0	8.90	AC+16:799- 62 V(AB) = 10.60 d(m) = 0.2
3596	Gl 536.1	B			13 59 34	+15 44.1		11.45		34.0	9.10	sep 1.1" 214d - 1.5" 195d (1946- 1965)
3597	GJ 1189				15 06 54	+24 12.2	dK8	9.31	1.06	34.0	6.97	LTT 14505 LFT 1175
3598	Gl 632				16 34 28	+79 53.7	dG3	7.06	0.62	34.0	4.72	
3599	Wo 9577				16 43 35	-30 31.6	K5	10.59	1.41	34.0	8.20	
3600	Wo 9827				23 24 30	-01 33.9	dM0.5	10.39	1.28	34.0	8.05	LTT 9542
3601	NN 4375				23 52 29	+28 21.3	K1 V	7.38	1.01	34.0	5.00	LTT 17045 LFT 1838
3602	NN 3938				16 02 57	-45 02.4	A m	4.72	0.23	33.3	2.30	BS 5980 may be composite (Mich)
3603	NN 3931				15 57 31	-16 23.3	F8 V	5.47	0.52	33.2	3.08	LTT 6378
3604	Gl 24	A			00 34 14	-49 24.3	G3 V	6.79	0.64	33.0	4.38	
3605	Gl 24	B			00 33 40	-49 24.1	K0 V	8.37	0.78	33.0	5.96	
3606	Wo 9056				01 22 10	+18 14.6	K2	8.49	0.89	33.0	6.08	LFT 132
3607	Gl 81.1	A			01 54 43	-10 29.0	G5 IV	6.42	0.82	33.0	4.00	LTT 1036
3608	Gl 81.1	B			01 54 45	-10 29.4	m	11.21	1.38	33.0	8.80	LTT 1039 LP 709-81 L 799-3
3609	NN 3217				03 18 17	+52 09.4	K3	9.07	0.99	33.0	6.66	LTT 11103
3610	Wo 9242				07 48 31	-59 15.0	G5 V	7.50	0.68	33.0	5.09	LTT 2959
3611	NN 3535				09 06 26	-10 33.2	G4	7.15	0.61	33.0	4.74	LTT 3364

3612	Gl 452.5	A	11 52 29	-55 48.9	G5 V	7.29	0.64	33.0	4.88	V(AB) = 6.72 d(m) = 0.40
3613	Gl 452.5	B	11 52 29	-55 48.9		7.70		33.0	5.30	sep 1.8" 207d - 3.2" 180d (1887- 1956)
3614	Wo 9403		12 15 21	+46 54.1	dM1.5e	11.50	1.44	33.0	9.09	LTT 13429 LFT 894
3615	Gl 511		13 23 56	-24 02.0	K3 V	8.72	0.89	33.0	6.31	
3616	GJ 1190		15 11 25	-03 36.9	K5 V	9.84	1.13	33.0	7.43	U370 Wolf 561
3617	NN 4051		18 16 40	-05 47.6	M2.5	12.57	1.45	33.0	10.16	LTT 7282 LP 689-1 L 920-7
3618	NN 4101		19 08 14	+79 40.4	dK8	9.72	1.10	33.0	7.31	
3619	Wo 9659		19 28 12	-06 37.1	G0	7.29	0.64	33.0	4.88	LTT 7713
3620	NN 4142		20 14 28	+06 46.0	dK8	9.72	1.14	33.0	7.31	
3621	Gl 847.1		22 03 38	-45 38.0	K2 V	8.43	0.85	33.0	6.02	
3622	Wo 9797		22 47 20	-41 45.1	G5 V	7.77	0.74	33.0	5.36	LTT 9216
3623	Gl 99	A	02 25 46	+32 02.1	dM0 pJ	10.20	1.36	32.2	7.74	V(AB) = 9.59 d(m) = 0.3
3624	Gl 99	B	02 25 46	+32 02.1		10.50		32.2	8.00	sep 0.26" 105d - 0.15" 115d (1959- 60)
3625	NN 4270		22 14 31	-48 54.0	K3 V	8.42		32.1	6.00	LTT 8937 CP-49:11578
3626	Gl 42.1		00 52 19	+23 49.9	G5	7.38	0.65	32.0	4.91	
3627	Wo 9073	A	02 05 02	-00 51.0	G2 V	6.90	0.61	32.0	4.43	LTT 1107
3628	Wo 9073	B	02 05 00	-00 49.8	K4	10.52	1.24	32.0	8.05	LTT 1106
3629	Wo 9079		02 19 11	-31 09.8	K3 V	8.81	0.93	32.0	6.34	LTT 1194 LFT 211

3630	GI 141.2	wissenschaft in die schulen!	03 24 07	-30 47.7	G8 V	7.88	0.71	32.0	5.41	
3631	GI 217.2		05 45 06	-70 10.8	K0 V	8.08	0.76	32.0	5.61	
3632	GI 374		09 54 09	-40 32.9	K4 V	9.00	0.96	32.0	6.53	
3633	Wo 9356		11 14 42	-01 42.5	dK6	9.78	1.17	32.0	7.31	LFT 788
3634	Wo 9572		16 37 22	+05 36.5	K2	8.67	0.89	32.0	6.20	LTT 14942
3635	GI 650		16 58 22	-13 29.4	G2 V	7.12	0.58	32.0	4.65	G3 Kui, SBO (A&A 195,129)
3636	GI 722.1		18 36 28	+42 37.2	dK0 e	8.34	0.82	32.0	5.87	
3637	NN 4181		21 05 49	+24 58.5	dK8	9.88	1.16	32.0	7.41	LTT 16183
3638	GI 836.4		21 39 25	-12 23.0	M1.5:	12.80	1.48	32.0	10.33	Ross 206
3639	GI 863.3		22 32 57	-54 52.0	G5 V	7.58	0.66	32.0	5.11	
3640	GI 99.1		02 25 52	+29 42.5	G0 V	5.88	0.58	31.7	3.39	
3641	NN 3680		11 38 39	-28 55.3	G0 V	6.44	0.66	31.7	3.95	CP-28:4330 LTT 4332
3642	GI 53.2		01 06 01	+16 59.1	dK6	10.55	1.27	31.0	8.01	
3643	Wo 9059		01 37 52	+66 39.7	G5 V	7.68	0.68	31.0	5.14	LTT 10587 LFT 148
3644	Wo 9089		02 35 31	+30 36.4	G1 V	7.34	0.60	31.0	4.80	LFT 219
3645	Wo 9202		06 05 25	-59 31.5	K0 V	8.46	0.85	31.0	5.92	LTT 2459 LFT 453 CD- 59:1224
3646	GI 295.1		07 57 28	+13 56.2	K5 e	10.36	1.26	31.0	7.82	
3647	Wo 9420		12 50 26	+34 00.5	K1 V	9.42	1.08	31.0	6.88	LTT 13690
3648	Wo 9453	A	13 34 01	+74 45.3	dK5	9.79	1.12	31.0	7.25	LTT 13958
3649	Wo 9453	B	13 34 01	+74 45.3	k	13.47	1.44	31.0	10.93	LP 21-568 sep 15" 324d (NLTT)
3650	GI 561.1	A	14 43 06	-25 13.9	F2 III-IV	5.10	0.34	31.0	2.56	BS 5497 ADS 9375 V (AB) = 4.94 d (m) = 1.98

3651	Gl 561.1	B	14 43 07	-25 14.0	dF9	7.14		31.0	4.60	sep 8.65" (1954)
3652	Gl 563.3		14 47 55	+07 01.3	K2 V	9.08	0.96	31.0	6.54	
3653	Gl 570.2		14 55 30	+31 36.7	dM2	11.11	1.33	31.0	8.57	AC +31:32985
3654	Wo 9808		23 03 08	+68 08.7	G6 V	7.48	0.65	31.0	4.94	LFT 1759
3655	Wo 9830		23 30 57	+42 34.1	G0	7.14	0.58	31.0	4.60	LTT 16929
3656	Gl 909.1		23 50 05	-06 16.3	K4	9.53	1.08	31.0	6.99	
3657	Gl 56.2		01 15 49	-48 24.9	M1	11.55	1.44	30.0	8.94	L 293-094 Sm 185
3658	Gl 306.1		08 23 46	-29 45.7	G4 V	7.81	0.67	30.0	5.20	
3659	Gl 388.2		10 18 25	-15 13.9	F8 V	7.18	0.55	30.0	4.57	
3660	Gl 550		14 24 10	-51 42.6	G5 V	7.83	0.70	30.0	5.22	
3661	Gl 596	A	15 40 55	+26 26.2	K7	10.70	1.29	30.0	8.10	Steph 21187
3662	Gl 596	B	15 40 57	+26 25.5	m	13.50		30.0	10.90	LP 384-43 sep 45" 148d (NLTT)
3663	Wo 9672		19 52 33	+03 56.0	K3	9.40	0.99	30.0	6.79	LTT 15820
3664	Gl 828.4		21 25 45	+10 23.5	K2	8.73	0.86	30.0	6.12	
3665	Gl 838.2		21 49 05	+00 36.9	K1	8.60	0.83	30.0	5.99	
3666	NN 3901		15 18 39	-47 44.8	F8 V	5.00	0.50	29.9	2.38	LTT 6126
3667	Gl 7		00 06 29	-27 24.1	m	11.72	1.50	29.0	9.03	
3668	Gl 50		00 59 27	-10 08.9	K5 V	10.50	1.25	29.0	7.81	
3669	Wo 9169	A	04 53 17	+04 35.5	F8	7.02	0.55	29.0	4.33	LTT 11546
3670	Wo 9169	B	04 53 15	+04 35.7	k	14.60		29.0	11.90	sep 22" 278d
3671	GJ 1076		05 19 13	+54 45.5	K3 p	9.46	1.04	29.0	6.77	
3672	Gl 251.1		06 52 10	+12 13.7	dM1.5	10.55	1.24	29.0	7.86	
3673	Gl 384	A	10 10 56	-47 13.8	G8 V	8.27	0.80	29.0	5.58	V(AB) = 8.19 d(m) = 2.6

3674	GI 384	B	10 10 56	-47 13.8		10.90		29.0	8.20	sep 4.6" 135d - 5.3" 127d (1901-59)
3675	GI 478		12 33 45	-76 40.7	m	11.00	1.30	29.0	8.31	L 038-015
3676	GI 508.3		13 21 07	-13 46.8	K7	11.79	1.40	29.0	9.10	AC-13:2264-197
3677	Wo 9486		14 30 54	-09 42.5	K4	10.54	1.25	29.0	7.85	LTT 5754 LFT 1117
3678	Wo 9566		16 30 23	+03 21.2	K1	8.85	0.88	29.0	6.16	LTT 14916
3679	GI 630		16 33 17	+33 24.3	dM0	11.06	1.34	29.0	8.37	AC +33:45152
3680	GI 632.2	A	16 35 48	+76 04.9	K7	10.02	1.15	29.0	7.33	V(AB) = 9.95 d(m) = 3.
3681	GI 632.2	B	16 35 47	+76 04.9	DA	13.00		29.0	10.00	AC+76:5655 sep 3.7" 285d (1895)
3682	NN 4028		17 46 45	-56 33.4	M2	12.13	1.46	29.0	9.44	LTT 7100 LFT 1378 L 205-83
3683	NN 4033		17 51 22	-65 42.6	F8 V	6.36	0.45	29.0	3.67	CD-65:2389 LTT 7126
3684	NN 4233		21 50 14	+39 34.0	K2	8.23	0.73	29.0	5.54	LTT 16388
3685	GI 847	A	21 59 55	-70 09.9	m	10.97	1.38	29.0	8.28	AC-71:462-64
3686	GI 847	B	21 59 55	-70 09.9	m	13.70	1.61	29.0	11.01	L 118-272
3687	GJ 1272	A	22 42 58	+10 55.9	dK6	9.98	1.13	29.0	7.29	ADS 16242A V (AB) = 9.82 d (m) = 2.
3688	GJ 1272	B	22 42 58	+10 55.9		12.00		29.0	9.00	ADS 16242B sep 0.7" 80d - 1.9" 359d (1878-1971)
3689	Wo 9819		23 15 41	-58 34.7	G2 V	7.52	0.65	29.0	4.83	LTT 9472
3690	NN 4315	AB	23 07 39	+47 41.2	G5	7.91	0.90	28.7	5.20	ADS 16557

3691	Wo 9697	A	20 28 04	+26 40.6	dM1	10.28	1.34	28.4	7.55	LTT 15985 V (AB) = 9.71 d (m) = 0.4 , Sp T.: K7 (Kui)
3692	Wo 9697	B	20 28 04	+26 40.6		10.70		28.4	8.00	sep 1.3" 335d
3693	NN 4209		21 37 19	-16 53.4	F0 p	3.68	0.32	28.2	0.90	A7MF3 (III)P (SR) Mich
3694	Wo 9024		00 41 58	-26 47.5	G5 V	7.79	0.67	28.0	5.03	LTT 410
3695	Gl 210		05 36 30	-42 59.7	G0 V	7.44	0.60	28.0	4.68	
3696	Wo 9237		07 33 32	-03 02.5	G0	7.16	0.57	28.0	4.40	LTT 2893
3697	Gl 340.1	A	09 16 36	-68 28.7	F4 V	6.13	0.42	28.0	3.37	BS 3712 V (AB) = 5.39 d (m) = 0.0
3698	Gl 340.1	B	09 16 36	-68 28.7		6.13		28.0	3.37	a = 0.124" P = 3.20 yr, sep (AC) 18.1" 132d (1901)
3699	Gl 452.2	A	11 51 55	-37 28.3	F7 V	6.75	0.52	28.0	3.99	BS 4557 V (AB) = 6.47 d (m) = 1.3
3700	Gl 452.2	B	11 51 55	-37 28.3		8.10		28.0	5.30	sep 1.1"
3701	Gl 743		19 03 00	+22 59.8	G9	8.55	0.81	28.0	5.79	
3702	Wo 9725		21 08 34	+80 35.3	K5	10.84	1.26	28.0	8.08	LTT 18514 AC+80:5262
3703	Gl 618.1		16 17 48	-04 08.9	dM2	10.70	1.40	27.2	7.87	AC-04:2788- 82
3704	GJ 2018		00 57 51	-25 53.0	K2	9.95	1.11	27.0	7.11	LTT 565
3705	Wo 9135		03 48 04	+23 45.2	dK6	10.23	1.16	27.0	7.39	vB 170 Hyades
3706	Gl 181.1		04 55 14	-61 13.9	m	12.06	1.48	27.0	9.22	L 131-006
3707	Wo 9181		05 27 06	-75 43.7	F8 V	7.17	0.54	27.0	4.33	LTT 17817
3708	Wo 9204		06 09 55	-41 33.7	K2 V	9.29	0.95	27.0	6.45	LTT 2482

3709	Wo 9251	A	08 04 28	+07 31.8	dK8	10.45	1.24	27.0	7.61	ADS 6597 V (AB) = 9.69 d (m) = 0.5
3710	Wo 9251	B	08 04 28	+07 31.8	K8	10.86		27.0	8.02	sep 5.7"
3711	G1 454.2	A	11 59 13	-34 22.3	G0 V J	7.35	0.59	27.0	4.51	V(AB) = 6.90 d(m) = 0.7
3712	G1 454.2	B	11 59 13	-34 22.3		8.10		27.0	5.30	sep 0.6" 121d (1960)
3713	G1 488.2	A	12 52 22	-06 03.9	K5	10.42	1.18	27.0	7.58	LTT 4937 Ross 970
3714	G1 488.2	B	12 52 21	-06 03.7	m	17.00		27.0	14.20	LP 674-34 sep. 20" 318d
3715	G1 518.1		13 34 29	+08 01.6	K4	10.02	1.09	27.0	7.18	
3716	GJ 1188		15 00 57	+03 58.1	m	12.10	1.46	27.0	9.26	Ross 1044
3717	G1 848.1	A	22 04 55	-51 27.7	K7	10.51	1.21	27.0	7.67	LTT 8866 L 283-8 Sm 101
3718	G1 848.1	B	22 04 34	-51 21.7	m	12.51	1.51	27.0	9.67	L 283-009 sep (A-BC) 408" 331d (NLTT)
3719	G1 848.1	C	22 04 33	-51 21.9	m	13.42	1.49	27.0	10.58	L 283-010 sep (B-C) 11" 214d (NLTT)
3720	G1 867.1	A	22 36 55	-12 52.4	G8/K0 V J	8.51	0.78	27.0	5.67	ADS 16145 dG9e Wil, V (AB) = 7.80 d (m) = 0.08
3721	G1 867.1	B	22 36 55	-12 52.4	dG9 e	8.60		27.0	5.80	sep 3.6" 118d (1960)
3722	G1 867.1	C	22 37 02	-12 50.9	k-m	14.65	1.61	27.0	11.81	sep(AC) 139"
3723	Wo 9822		23 17 28	+28 35.7	K1 V	8.89	0.81	27.0	6.05	LFT 1783
3724	NN 3457	A	07 36 22	+33 34.9	m	11.83	1.46	26.4	8.94	LTT 17998

3725	NN 3458	S B	wissenschaft in die schulen 07 36 23	+33 35.0	m+	18.00		26.4	15.00	LP 256-44 sep 13" 56d
3726	Gl 647			+13 22.0	dM0	10.66	1.36	26.2	7.75	AC+13:804- 98
3727	Wo 9003			-24 05.9	K0 V	8.70	0.80	26.0	5.77	LTT 47
3728	Gl 56			-15 45.6	K3 V	9.77	1.00	26.0	6.84	
3729	Wo 9067	A		+03 42.1	K4	10.62	1.22	26.0	7.69	LTT 10689 Wolf 109
3730	Wo 9067	B		+03 42.3	M1.5	12.40		26.0	9.50	LTT 10690 sep 17" 16d (NLTT)
3731	Wo 9134			-64 59.4	G5 V	7.85	0.66	26.0	4.92	LTT 1791
3732	Wo 9156			-64 11.8	G5 V	7.91	0.65	26.0	4.98	LTT 1986
3733	Wo 9322			+03 24.3	G1 V	7.76	0.60	26.0	4.83	LTT 12747
3734	Gl 421.1	A		+53 02.7	F6 V	6.50	0.43	26.0	3.57	
3735	Gl 421.1	B		+53 02.9	F9 V	8.03	0.60	26.0	5.10	
3736	Gl 452.3	A		+19 41.4	dG6	8.22	0.71	26.0	5.29	
3737	Gl 452.3	B		+19 42.4	dG7	8.43	0.76	26.0	5.50	
3738	NN 3752			+01 28.3	G8 V	8.16	0.69	26.0	5.23	LTT 13668
3739	Gl 559.1			+64 30.4	dG0 e	7.54	0.61	26.0	4.61	
3740	Wo 9512	A		-51 54.6	G8 III	3.41	0.92	26.0	0.48	
3741	Wo 9512	B		-51 55.1	F9 V	6.69	0.50	26.0	3.76	
3742	Wo 9535			+65 32.4	dG5	9.04	0.86	26.0	6.11	LTT 14752
3743	Wo 9758			+74 45.9	K0	8.99	0.86	26.0	6.06	
3744	Gl 900.1			-47 13.1	G8 V	8.54	0.79	26.0	5.61	
3745	Gl 901			+00 53.4	M3.5:	13.08	1.56	26.0	10.20	Wolf 1040
3746	GJ 1040			+44 20.1	dK8	10.84	1.20	25.0	7.83	AC+44:66- 318

3747	NN 3278	S	wissenschaft in die schulen	04 21 07	+16 36.2	dM0	12.55	1.49	25.0	9.54	VA 297
3748	NN 3290			04 24 24	+17 07.6	dM1	13.06	1.49	25.0	10.05	VA420 GH7- 221
3749	NN 3498			08 22 03	+32 46.9	K3	10.05	1.06	25.0	7.04	LFT 583 LTT 12198
3750	GI 550.1			14 25 31	+24 03.8	dM0	10.92	1.26	25.0	7.91	
3751	Wo 9551			16 15 10	+71 03.4	dG5	7.90	0.63	25.0	4.89	LTT 14856
3752	NN 4366			23 47 31	+02 35.8	G7 V	8.36	0.74	25.0	5.35	LTT 17022
3753	NN 3086	A		01 17 10	+38 43.5	dM0	11.39	1.31	24.0	8.29	
3754	NN 3087	B		01 17 11	+38 43.7	k-m	14.35		24.0	11.25	sep 11" 41d
3755	NN 3089			01 17 42	+38 04.3	dK8	10.64	1.14	24.0	7.54	
3756	Wo 9203			06 05 57	+26 34.0	M3	13.34	1.50	24.0	10.20	LTT 11788 LFT 454 Ross 62
3757	Wo 9224			07 04 48	-47 30.6	k	10.54	1.17	24.0	7.44	LTT 2738
3758	GI 534.3			13 55 43	-33 45.2	G5 V	8.17	0.68	24.0	5.07	
3759	Wo 9843			23 49 32	+77 19.4	F5 V	6.56	0.43	24.0	3.46	LTT 17037
3760	GI 76			01 45 20	-26 59.7	K1 V	8.98	0.81	23.0	5.79	
3761	Wo 9106			02 53 27	+13 42.8	K0	9.05	0.81	23.0	5.86	
3762	NN 3269			04 12 43	+15 34.9	M2	11.01	1.24	23.0	7.82	VA 75 GH7- 140
3763	GI 223.1			05 52 11	-09 24.3	dM0	10.71	1.17	23.0	7.52	
3764	GI 308.3			08 30 27	-50 01.3	m	10.80	1.21	23.0	7.61	
3765	GI 343			09 22 49	+18 53.5	M2	13.43	1.61	23.0	10.24	Ross 83
3766	Wo 9395			12 09 52	-06 04.7	K3	9.96	1.00	23.0	6.77	LTT 4574

3767	NN 3854	S AB	wissenschaft in die schulen! 14 28 34	-15 24.8	G5 V J	8.38	0.71	23.0	5.19	LTT 5735 ADS 9291 V (AB) = 7.99, sep 2.3" 90d d(m) = 0.9 G6 Kui	
3768	Gl 599.1			15 47 22	-50 32.2	k	10.72	1.19	23.0	7.53	
3769	Wo 9553			16 16 02	-28 10.2	G0 V	7.67	0.61	23.0	4.48	LTT 6500
3770	Gl 698.1			17 54 59	-51 37.1	K3 V	9.64	0.92	23.0	6.45	
3771	Gl 776.1			20 00 41	-45 47.7	K4 :	12.15	1.40	23.0	8.96	L 349-18
3772	Gl 138.1	A		03 17 54	+08 51.3	dG2	8.45	0.68	22.0	5.16	
3773	Gl 138.1	B		03 17 59	+08 51.4	k-m	15.13		22.0	11.84	
3774	Gl 379.2			10 07 40	-36 30.8	G3 V-VI	8.08	0.60	22.0	4.79	
3775	Gl 577			15 04 57	+64 14.2	dG5 e	8.42	0.68	22.0	5.13	
3776	Wo 9624			18 16 00	-45 43.1	F7 V	6.85	0.54	22.0	3.56	
3777	Wo 9228			07 13 59	-15 29.7	A3 V	5.44	0.08	21.2	2.10	
3778	GJ 2015			00 48 56	-27 39.5	K0	10.41	1.08	21.0	7.02	
3779	Wo 9043			01 06 35	-31 11.7	G8/K0 V	9.10	0.79	21.0	5.71	LTT 646
3780	Wo 9094			02 38 28	-30 21.0	G0 V	8.02	0.56	21.0	4.63	LTT 1310 LFT 222
3781	Wo 9532			15 55 44	+63 57.4	G5	9.54	0.89	21.0	6.15	LTT 14744
3782	Wo 9657	A		19 26 47	-27 05.4	K3 III	5.52	1.12	21.0	2.10	
3783	Wo 9657	B		19 26 47	-27 05.4		8.69	0.86	21.0	5.30	
3784	Wo 9812	A		23 07 15	-22 43.7	G2 V	5.11	0.65	21.0	1.72	BS 8817 V (AB) = 4.69 d (m) = 0.8 , G6/8 III Mich
3785	Wo 9812	B		23 07 15	-22 43.7	A3 (IV)	5.90		21.0	2.50	sep 0.4" 7d (1959)
3786	Gl 10.1			00 09 03	-59 11.3	G4 V	8.35	0.62	20.0	4.86	

3787	Wo 9016		00 31 43	+47 38.4	F8	7.37	0.54	20.0	3.88	LTT 10192
3788	NN 3062		00 47 54	-27 42.6	A3	9.60	0.89	20.0	6.11	
3789	Wo 9222		06 54 41	-74 39.8	F8 V +A/F	7.65	0.53	20.0	4.16	composite spectra (Michigan)
3790	Wo 9407		12 26 39	-30 33.6	K0 V	9.06	0.79	20.0	5.57	LTT 4731
3791	Wo 9418		12 48 05	+71 27.6	K8	10.08	0.97	20.0	6.59	LTT 13673
3792	Gl 579.3		15 10 14	-00 58.5	K0	9.29	0.78	20.0	5.80	
3793	Gl 743.2		19 03 18	+25 50.7	dK2	7.22	1.03	20.0	3.73	
3794	Gl 161.2		04 05 21	-40 53.4	k	10.98	1.13	19.0	7.37	L 374-20
3795	NN 3281		04 22 08	+16 52.3	M2	10.31	1.04	19.0	6.70	VA342
3796	Gl 268.5		07 15 11	-13 54.6	K5	12.11	1.43	19.0	8.50	AC-13:1069- 363
3797	Gl 506.2		13 16 45	+85 00.9	dF7	7.28	0.50	19.0	3.67	
3798	Gl 632.3		16 36 13	+05 31.4	G	10.22	0.99	19.0	6.61	AC+05:125- 28
3799	Wo 9608		17 55 40	-30 09.6	K0 V	9.37	0.79	19.0	5.76	LTT 7146 LFT 1386
3800	Gl 886.1	A	23 00 18	+42 29.3	A3 Vn	5.14	0.09	18.5	1.50	BS 8766 ADS 16467 V(AB) = 5.10 d(m) = 3.7
3801	Gl 886.1	B	23 00 18	+42 29.3		8.80		18.5	5.10	sep 0.5" 25d (1958)
3802	Wo 9321		10 11 15	-07 08.2	dF6	7.21	0.49	16.0	3.23	

Available Visualisations:

- [Plot the results with the VOPlot utility](#)